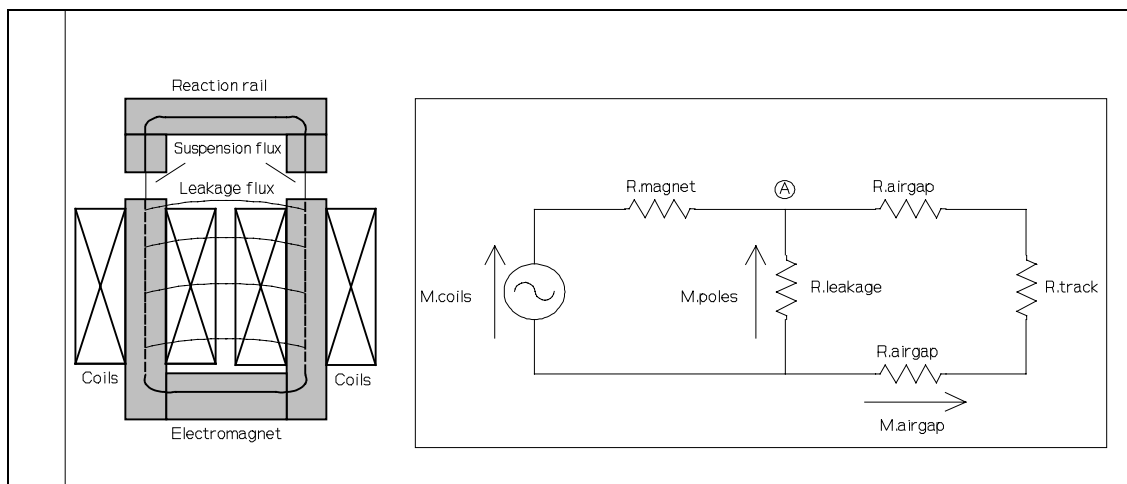


# Appendix A

## Electromagnet analysis

### A.1 Electromagnet steady-state flux circuit analysis

In order to determine the static lift force characteristic of the electromagnet, it is necessary to determine the relationship between applied coil mmf and the resultant mmf across each suspension air gap. This can be achieved by analysing a model of the electromagnet flux circuit. Figure A.1 shows a model of the electromagnet flux circuit which incorporates three flux quantities, namely air gap flux, leakage flux and electromagnet core flux.



**Figure A.1** Electromagnet flux paths and flux model circuit diagram

Network analysis and the application of Kirchhoff's Current Law is now used to determine the relationship between the applied coil mmf,  $M_{coils}$ , and the resulting air gap mmf,  $M_{airgap}$ . First, the currents into node A (see Figure 1) must be summed to zero, giving:

$$\frac{(M_{coils} - M_{poles})}{R_{magnet}} + \frac{(0 - M_{poles})}{R_{leakage}} + \frac{(0 - M_{poles})}{(R_{track} + 2R_{airgap})} = 0 \quad \mathbf{A.1}$$

This can be simplified by multiplying by the electromagnet and leakage reluctances,

$$(M_{coils} - M_{poles})R_{leakage} - M_{poles}R_{magnet} - \frac{M_{poles}R_{magnet}R_{leakage}}{(R_{track} + 2R_{airgap})} = 0 \quad \mathbf{A.2}$$

and collecting terms and rearranging thus,

$$M_{coils}R_{leakage} = M_{poles} \left( R_{leakage} + R_{magnet} + \frac{R_{magnet}R_{leakage}}{(R_{track} + 2R_{airgap})} \right) \quad \mathbf{A.3}$$

The mmf across each gap is given by the simple potential divider,

$$M_{airgap} = M_{poles} \left( \frac{R_{airgap}}{R_{track} + 2R_{airgap}} \right) \quad \mathbf{A.4}$$

and hence the pole piece mmf, in terms of the air gap mmf is given by:

$$M_{poles} = M_{airgap} \left( \frac{R_{track} + 2R_{airgap}}{R_{airgap}} \right) \quad \mathbf{A.5}$$

The expression for  $M_{poles}$  can now be substituted into Equation 3, giving:

$$M_{coils}R_{leakage} = M_{airgap} \left( \frac{R_{track} + 2R_{airgap}}{R_{airgap}} \right) \left( R_{leakage} + R_{magnet} + \frac{R_{magnet}R_{leakage}}{(R_{track} + 2R_{airgap})} \right) \quad \mathbf{A.6}$$

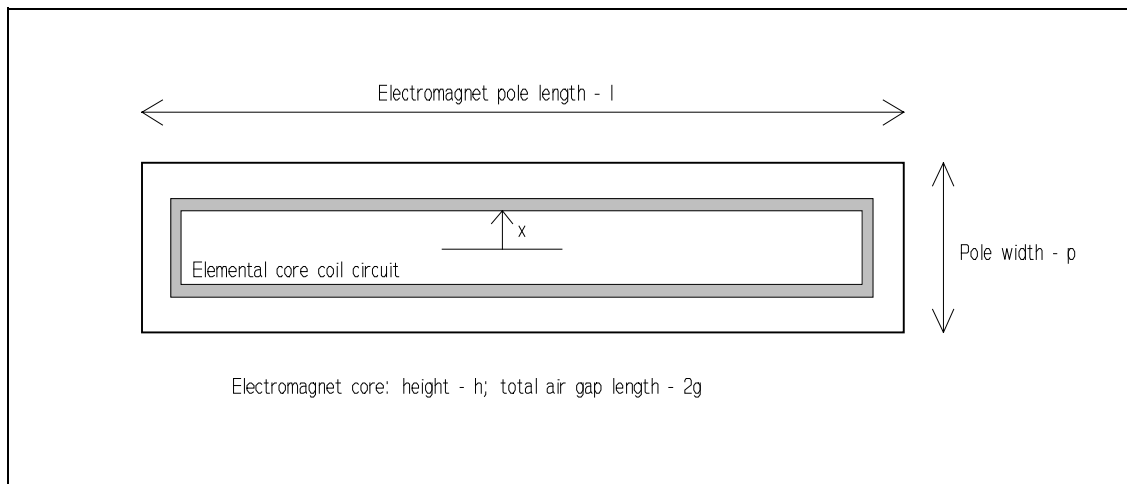
This can be rearranged to give the required relationship between coil mmf and airgap mmf,

$$\frac{M_{airgap}}{M_{coils}} = \frac{R_{leakage}R_{airgap}}{(R_{track} + 2R_{airgap})(R_{leakage} + R_{magnet}) + R_{magnet}R_{leakage}} \quad \mathbf{A.7}$$

### A.2 Eddy current time constant analysis

The flux lag time constant due to eddy-currents circulating within the electromagnet and track cores must be determined before control system synthesis can be performed. A novel time domain analysis is proposed which considers elemental circuits within the core as depicted in Figure A.2. To simplify the analysis, the ferromagnetic core is assumed to have infinite permeability. The analysis is performed in 5 stages, involving the calculation of the following:

- inductance of the elemental circuit within the core.
- inductance of an external coil (ie. outside the core) with a flux coupling equivalent to the internal elemental circuit.
- resistance of the elemental coil.
- time constant of the equivalent external coil circuit.
- total flux lag time constant is obtained by integrating the elemental time constants.



**Figure A.2** Eddy current elemental coil circuit analysis

By assuming infinite core permeability, the self inductance of a cored coil of cross sectional area  $A$ , with  $N$  turns, and a core air gap  $g$ , is given by:

$$L_{coil} = \frac{\mu_o A N^2}{g} \tag{A.8}$$

where  $\mu_o$  is the permeability of free space.

The self inductance of the elemental coil circuit within the electromagnet core (with two air gaps) as depicted in Figure A.2 can therefore be approximated by:

$$L_{elem} = \frac{\mu_o 2x (l-p+2x)}{2g} \approx \frac{\mu_o x l}{g} \quad \text{for } l \gg p, x \quad \mathbf{A.9}$$

The elemental coil inductance must now be translated to the inductance of an external coil coupled to the entire core flux, this is given by:

$$L'_{elem} = L_{elem} \left( \frac{2x}{p} \right) = \frac{2\mu_o x^2 l}{pg} \quad \mathbf{A.10}$$

The resistance of the elemental coil circuit is given by:

$$R_{elem} = \frac{\rho (2l-2p+8x)}{h\delta x} \approx \frac{2\rho l}{h\delta x} \quad \text{for } l \gg p, x \quad \mathbf{A.11}$$

where  $\rho$  is the resistivity of the core material, and  $\delta x$  is the width of the elemental coil.

The time constant for the equivalent external coil circuit is thus given by,

$$T'_{elem} = \frac{L'_{elem}}{R_{elem}} = \frac{2\mu_o x^2 l h \delta x}{2\rho l p g} = \frac{\mu_o h x^2 \delta x}{\rho p g} \quad \mathbf{A.12}$$

Since the equivalent external coil circuit is effectively coupled to the full core flux, the total time flux lag time constant due to eddy currents for all elemental coils is given by summing the time constant for each coil (see next section),

$$T_{eddy} = \sum T'_{elem} = \sum_x \frac{\mu_o h x^2 \delta x}{\rho p g} \quad \mathbf{A.13}$$

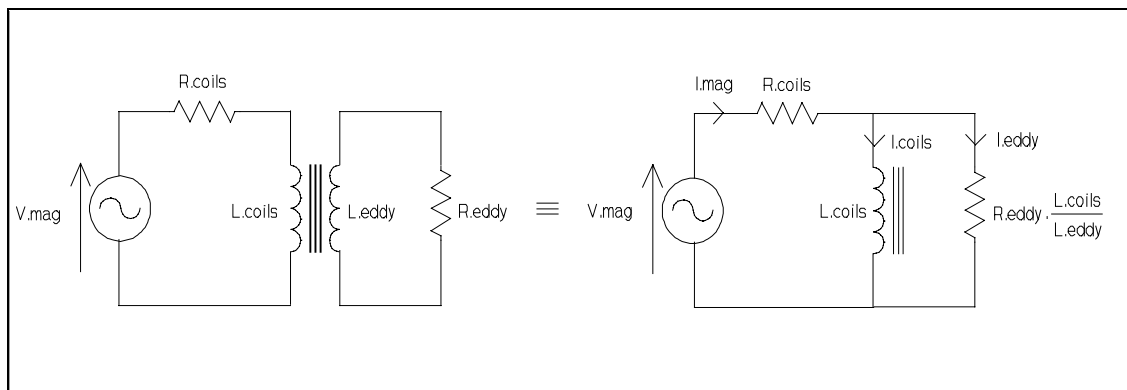
This summation can be most accurately and conveniently achieved by integrating the time constant of elemental eddy current coil circuits, giving,

$$T_{eddy} = \int_0^{p/2} \frac{\mu_o h x^2}{\rho p g} dx = \frac{\mu_o h}{\rho p g} \left[ \frac{x^3}{3} \right]_0^{p/2} = \frac{\mu_o h p^2}{24 \rho g} \quad \mathbf{A.14}$$

### A.3 Summation of coil and eddy current time constants

The eddy current circuits analysed in the previous section give rise to a flux lag characteristic which augments the flux lag due to the electromagnet coil circuit.

The eddy current effect has been modelled using equivalent external coils. The electromagnet, therefore, can be modelled as a transformer with two windings consisting of the excitation coil turns and equivalent eddy current circuit turns. By neglecting any leakage inductance, the two windings can be assumed to be perfectly coupled and hence modelled by the first circuit shown in Figure A.3. The second circuit in Figure A.3 has a secondary winding circuit which has been referred with respect to the primary and is therefore equivalent to the first circuit. The second circuit is now used to analyse the combined behaviour of the coil and eddy current circuits.



**Figure A.3** Schematic models for the coil and eddy current circuits

For convenience the referred eddy current circuit resistance can be expressed more simply by:

$$R'_{eddy} = \frac{L_{coils}}{T_{eddy}} \quad \text{where} \quad T_{eddy} = \frac{L_{eddy}}{R_{eddy}} \quad \text{A.15}$$

The parallel impedance of the coil inductance and the normalised eddy current circuit resistance is then given by:

$$Z(L_{coils}) \parallel Z(R'_{eddy}) = \frac{sL_{coils} \frac{L_{coils}}{T_{eddy}}}{sL_{coils} + \frac{L_{coils}}{T_{eddy}}} = \frac{sL_{coils}}{(1 + sT_{eddy})} \quad \text{A.16}$$

where  $Z(x)$  represents the impedance of  $x$ , and  $s$  is the Laplace operator.

The voltage across the coil inductance is given by the potential divider:

$$\frac{V_{coils}}{V_{mag}} = \frac{\frac{sL_{coils}}{(1 + sT_{eddy})}}{R_{coils} + \frac{sL_{coils}}{(1 + sT_{eddy})}} = \frac{s \frac{L_{coils}}{R_{coils}}}{\left(1 + sT_{eddy} + s \frac{L_{coils}}{R_{coils}}\right)} \quad \text{A.17}$$

Finally, this can be rearranged to express the coil current,  $I_{coils}$ , in terms of the applied electromagnet voltage, this gives:

$$I_{coils} = \frac{V_{coils}}{sL_{coils}} = \frac{1}{1 + s(T_{coils} + T_{eddy})} \frac{V_{mag}}{R_{coils}} \quad \text{where } T_{coils} = \frac{L_{coils}}{R_{coils}} \quad \text{A.18}$$

The overall flux actuation characteristic is therefore a first-order lag with a time constant equal to the sum of the coil and eddy current time constants.

This result can be expanded in an iterative fashion to prove that any number of perfectly coupled shorted windings will give rise to a first-order flux lag with a time constant equal to the sum of the winding time constants. This fact is used in the previous section to combine the effect of elemental eddy current circuits.

Finally, the transfer function for the referred eddy current, and the total electromagnet current, in terms of the applied electromagnet voltage, are given by the following:

$$I_{eddy} = \frac{V_{coils}}{L_{coils}/T_{eddy}} = \frac{sT_{eddy}}{1 + s(T_{coils} + T_{eddy})} \frac{V_{mag}}{R_{coils}} \quad \text{A.19}$$

$$I_{mag} = I_{coils} + I_{eddy} = \frac{1 + sT_{eddy}}{1 + s(T_{coils} + T_{eddy})} \frac{V_{mag}}{R_{coils}} \quad \text{A.20}$$

## A.4 Computer program to calculate electromagnet model parameter values

```

Program Magnet_Model ();

{ Calculates parameter values and forces for the electromagnet model developed in Chapter 2 }
{ Pascal Program; Author: N. S. McLagan; 1-9-90; all variables in elementary units }

{ Electromagnet dimensions }
Const
  length = 0.200;
  pole = 0.0095;
  offset = 0.0015;
  height = 0.063;
  width = 0.033;
  num_turns = 274;

  mu_o = 1.2566e-6; { 4e-7.pi }

Function Gap_area( z : Real ) : Real;
Begin {Air gap normal plus fringe flux area - from Equation 2.11}
  Gap_area := length * (pole + (2*z / pi))
End;

Function Lift_force_ratio( z : Real ) : Real;
Begin {Electromagnet lift/gross force ratio - Equation 2.20}
  Lift_force_ratio := 1 - (offset/z)*arctan(offset/z) / (1+(pi*pole)/(2*z))
End;

Function R_mag( mu_m : real ) : Real;
Begin {Electromagnet core reluctance - Equation 2.13}
  R_mag := (2*height + width + 2*pole) / (mu_m * mu_o * length * pole)
End;

Function Mu_mag( core_flux, mu_max, mu_break, mu_span : real ) : Real;

  { mu_max: Plateau value for mu before roll-off. /1 }
  { mu_break: Flux density break point for mu roll-off. /Tesla }
  { mu_span: Span of fall from break point to zero. /Tesla }

  Var
    core_flux_density, mu : Real;
  Begin {Electromagnet core permeability - Table 2.2}
    mu := mu_max;
    core_flux_density := core_flux / (pole * length);
    IF (core_flux_density > mu_break) Then
      mu := mu * (1 - (core_flux_density - mu_break)/mu_span);
    If (mu < 1) Then
      mu := 1;
    Mu_mag := mu
  End; { of Mu_mag }

Function R_track( mu_t : Real ) : Real;
Begin {Track reluctance - Equation 2.12}
  R_track := (width + 4*pole) / (mu_t * mu_o * length * pole )
End;

Function Mu_track : Real;
Begin {Relative track permeability}
  Mu_track := 2000;
End;

Function R_leak : Real;
Begin {Leakage reluctance - Equation 2.15}
  R_leak := 2*width / ( mu_o * (length + 2*width/pi) * (height + 2*width/pi) )
End;

```

```

Function R_gap( z : real ) : Real;
Begin {Air gap reluctance - from Equation 2.11}
  R_gap := z / ( mu_o * Gap_area(z) )
End;

Function L_mag( z, mu_m, mu_t : Real ) : Real;
Begin {Electromagnet inductance - Equation 2.32}
  L_mag := num_turns * num_turns * (R_track(mu_t) + 2*R_gap(z) + R_leak) /
    ((R_track(mu_t)+2*R_gap(z))*(R_leak+R_mag(mu_m))+(R_mag(mu_m)*R_leak))
End;

Procedure Calculate( Var current, airgap_flux, leakage_flux, core_flux : Real;
  { Using } airgap, force, mu, mu_break, mu_span : Real );
Var
  gross_force_per_pole : Real;
  pole_mmf, iron_mmf, coil_mmf : Real;

Begin
  gross_force_per_pole := force / (2 * Lift_force_ratio(airgap));
  airgap_flux := SQRT( 2*gross_force_per_pole * Gap_area(airgap) * mu_o );
  pole_mmf := airgap_flux * (2 * R_gap(airgap) + R_track( Mu_track ) );
  leakage_flux := pole_mmf / R_leak;
  core_flux := airgap_flux + leakage_flux;
  iron_mmf := core_flux * R_mag( Mu_mag( core_flux, mu, mu_break, mu_span ) );
  coil_mmf := pole_mmf + iron_mmf;
  current := coil_mmf / num_turns;
End; { of Calculate }

Procedure Force;

Var
  airgap_index : Integer;
  force, airgap : Real;
  airgap_flux, leakage_flux, core_flux : Real;
  current, k : Real;

Begin
  writeln;
  write( 'Enter required lift force in Newtons: ' );
  readln( force );
  writeln;
  For airgap_index := 1 To 9 Do
    Begin
      airgap := airgap_index / 1000;
      Calculate( current, airgap_flux, leakage_flux, core_flux,
        { Using } airgap, force, 2000, 1.0, 0.6 );
      k := force * airgap * airgap * 1E6 / (current * current);
      write( 'Airgap =', airgap_index:2 );
      write( ' I =', current:7:2 );
      write( ' k =', k:6:2 );
      write( ' track B =', airgap_flux/pole/length:5:2 );
      write( ' mag B =', core_flux/pole/length:5:2 );
      write( ' mu_m =', Mu_mag( core_flux, 2000, 1.0, 0.6 ):5:0 );
      writeln
    End; { of gap loop }
  End; { of Force }

Procedure Parameters;
Var
  airgap_index, mu : Integer;
  gap : Real;

Begin
  mu := 2000;
  writeln; writeln('All reluctances are kA/Wb, Inductances are in mH' );
  For airgap_index := 0 To 9 Do
    Begin
      gap := airgap_index / 1000;
      writeln; write( 'Gap = ', airgap_index );
      write( ' R_mag = ', R_mag(mu)/1000:1:0 );
      write( ' R_track = ', R_track(mu)/1000:1:0 );
      write( ' R_leak = ', R_leak/1000:1:0 );
      write( ' 2*R_gap = ', 2*R_gap(gap)/1000:4:0 );
      write( ' L_mag = ', 1000*L_mag(gap,mu,mu):5:1 );
      write( ' A_gap = ', Gap_area(gap):3:3 );
      End
    End; { of Parameters }

```



```

Procedure Spreadsheet_plots;
Var
  datafile : Text;
  airgap_index, force_index : Integer;
  airgap, force : Real;
  current_fo, current_imu, current_fm, current_vmu : Real;
  airgap_flux, leakage_flux, core_flux : Real;

Begin
writeln;
writeln( 'Writing spreadsheet data to file: magmodel.dat ' );
write( 'Airgaps: ' );
Assign( datafile, 'magmodel.dat' );
Rewrite( datafile );
For airgap_index := 1 To 7 Do
  Begin
  write( airgap_index, ',' );
  For force_index := 0 To 100 Do
    Begin
      airgap := airgap_index / 1000;
      force := force_index * 20;
      current_fo := SQRT(4*force/(mu_o*pole*length))*airgap/num_turns;
      Calculate( current_imu, airgap_flux, leakage_flux, core_flux,
        { Using } airgap, force, 1E6, 1E6, 1E6 );
      Calculate( current_fm, airgap_flux, leakage_flux, core_flux,
        { Using } airgap, force, 2000, 1E6, 1E6 );
      Calculate( current_vmu, airgap_flux, leakage_flux, core_flux,
        { Using } airgap, force, 2000, 1.0, 0.6 );
      writeln( datafile, force:10:1, current_fo:8:2, current_imu:8:2,
        current_fm:8:2, current_vmu:8:2 );

      End; { of force loop }
      writeln( datafile )
    End; { of airgap loop }
  Close( datafile )
End; { of Spreadsheet_plots }

```

```

Procedure Menu;
Var
  response : Char;
Begin
Repeat
  writeln;
  writeln;
  writeln('Force and flux characteristic');
  writeln('Parameters');
  writeln('Spreadsheet plot file');
  writeln('Quit');
  readln(response);
  Case response Of
    'f','F': Force;
    'p','P': Parameters;
    's','S': Spreadsheet_plots;
  End; { of Case }
Until (response = 'Q') Or (response = 'q')
End; { of Menu }

```

```

Begin
Menu
End.

```

## A.5 Electromagnet and rail design parameters

The analysis of the experimental electromagnet described in Chapter 2 provides a good grounding in the fundamental electromagnetic principles and practical issues that are central to the operation of a suspension electromagnet. This section first examines the impact of electromagnet and rail design parameters on the steady-state force and the force dynamics, and then two distinct electromagnet configurations that have evolved are discussed.

### A.5.1 Steady-state force

The air gap flux coupling the electromagnet and its reaction rail generates a force of attraction between the electromagnet and rail. To assist in the understanding of the concepts involved, it is helpful to make two simplifying assumptions. The first assumption is that the electromagnet and rail cores have negligible reluctance relative to the air gaps, and the second is that the air gap flux is uniformly distributed over an area equal to the electromagnet pole face area. Using these approximations, the lift force is proportional to the square power of the air gap flux density multiplied by the total air gap flux area. To get a satisfactory core lift/weight ratio, the core must be operated with a high flux density. Unit magnetic flux density produces a lift force per unit area of about  $4 \times 10^5 \text{ N/m}^2$ . This is a 'magnetic pressure' of 4 bar (60 lb/in<sup>2</sup>) which is comparable with a typical truck tyre pressure. The flux density used and hence the magnetic pressure determines the pole face area required to support a given load. For example, a 1 t lift capacity requires a total electromagnet pole face area of about 250 cm<sup>2</sup> at unit flux density.

At the required high operational flux levels, the reluctance of the cores is not negligible relative to the air gap reluctance. Also, for air gap dimensions comparable to the pole width, significant flux fringing occurs giving an effective air gap flux area larger than the pole face area. For accurate modelling, the simplifying assumptions used above are untenable and a more detailed analysis is required.

The coil excitation required to produce unit flux density in the air gap is dominantly determined by the permeability of free space. Thus, approximately 1600 ampere-turns are required per mm of electromagnet air gap (this figure allows for both air gaps). The desired operating air gap range and lift force range thus determine the required coil excitation range. The coil must be able to dissipate the waste heat generated at the

required excitation and also provide an acceptable power/lift ratio so that excessive power controller weight is avoided. Two critical factors are the conductor resistivity and the method of cooling the coils. These factors dictate a nominal operational current density for the windings based on thermal considerations. The coil cross-section and hence the slot area between the pole pieces can be calculated directly from the current density and the ampere-turns. Coils are usually made from copper or aluminium wire or foil. Aluminium is less dense than copper, but it has a higher resistivity, thus requiring a lower current density than copper for a given power dissipation. The lower current density for aluminium is achieved at the expense of a larger coil cross-sectional area which also needs a longer and hence heavier core. A detailed optimisation analysis is therefore required to design for best power/lift and lift/weight ratios.

In addition to the air gap flux linking the electromagnet and rail, flux also flows across the slot between the pole pieces, increasing the flux through the cores. If the slot is too narrow, this leakage flux requires a larger, heavier core, whereas if it is too wide, the extra yoke length also increases the core weight. The amount of leakage flux is also affected by the location of the coils which can be wound either around the pole pieces or around the yoke. With the coils on the pole pieces, the m.m.f. rises up the pole pieces from 0% at the yoke to 100% at the pole faces. However, with a yoke wound coil, the full m.m.f. is present all the way up the pole pieces. The first arrangement benefits from a smaller leakage flux, thus requiring a smaller and lighter core, whilst the latter arrangement allows a modest increase in the pole face length and area without increasing the yoke and coil size and weight. The optimum slot width/height ratio and the coil location clearly depends on the detailed electromagnet configuration and dimensions.

The partitioning of the coil cross-section into a particular number of turns depends largely on a practical consideration of available power semiconductor technology. From a heat transfer viewpoint, a solid coil consisting of one turn would be ideal. However, such a high current and low voltage coil would obviously require rather a heavy and inefficient power controller and interconnecting cables ! To enable the use of light and economical power controllers, the voltage and current rating of the coil must be matched for use with available power semiconductor technology. The slot space occupied by insulation, and the thermal insulation attendant with electrical insulation must be factored into the allowable coil current density discussed above.

The lift force characteristic outlined above assumes the electromagnet and its rail are vertically aligned. If the electromagnet is displaced laterally so that there is some

overlap of the poles, then the shear flux near the pole edges produces a lateral force component in addition to a reduced lift force component. By using an inverted U-shaped rail core, shear flux occurs at both electromagnet pole faces when the electromagnet and rail are laterally displaced. This rail core shape gives approximately double the lateral force, but at the expense of a reduced lift force because of the increased air gap reluctance. For small lateral displacements (relative to the pole width), the lateral force is approximately proportional to the displacement, thus giving a reasonably constant lateral stiffness. The lateral force and hence stiffness do however decrease as the air gap increases. Accurate modelling of the lateral force for a given pole face geometry, lateral displacement and electromagnet air gap requires a detailed analysis of the air gap flux distribution.

Having considered the design parameters which affect the steady-state force characteristics of suspension electromagnets, the parameters affecting the rate of change of flux must now be considered to determine the dynamic force characteristics.

### A.5.2 Force dynamics

Electromagnet flux changes from one steady-state value to a new steady-state value whenever the air gap or the applied coil terminal voltage changes. The variation in the electromagnet core flux generates an e.m.f. across any conducting circuits that enclose the flux. For a suspension electromagnet, there are two such circuits. The first is the excitation coil circuit, whilst the second circuit occurs within the core material in which circulating eddy currents are distributed. The coil inductance and resistance impose a first order lag characteristic on the core flux with the time constant given by the inductance / resistance ratio. The flux lag due to eddy currents in the core can be approximated by integrating the effect of elemental circuits within the core. This produces a first order flux lag with a time constant proportional to the square power of the smallest pole face dimension divided by the resistivity of the core material. The combined effect of the flux coupled circuits is a first order flux lag characteristic, with a time constant equal to the sum of the coil and core lag time constants. Both the coil inductance and the effective eddy current circuit inductance are a function of the magnetic reluctance of the flux path and hence the air gap length. The flux lag time constant is therefore inversely proportional the air gap length.

The dynamic requirements and structure of the closed-loop suspension controller determine acceptable flux lag time constants for the electromagnet coil and core. There

is little design flexibility with the coil time constant since the coil inductance is fundamentally determined by the air gap reluctance and the coil resistance is generally designed on the basis of coil weight and steady-state power dissipation. The number of coil turns offers no help since doubling the number of turns doubles both the inductance and resistance (assuming a constant coil cross section) leaving the time constant unchanged.

The flux lag time constant due to eddy currents in electromagnet/rail cores depends critically on the shape and size of the pole faces. The time constant can be reduced using a suitable feedback strategy, but if necessary, it is usually more cost effective to modify the core. This can be achieved through the use of high silicon steel (which has a larger resistivity than mild steel) or by using a laminated core construction to reduce the dimensions of the eddy current circuits within the core.

Eddy currents also affect the motion of an electromagnet along its rail. This is because eddy currents in the rail cause a lag in the magnetisation and subsequent demagnetisation of the rail as an electromagnet progresses along the guideway. These spatial flux lags reduce the lift force and generate a drag force. The time a moving electromagnet takes to pass a point on its rail is given by the electromagnet length divided by its speed. As this passing time decreases towards the flux lag time constant of the rail core, the problem becomes more severe. This problem thus increases with higher speeds, shorter magnets and longer rail core time constants. It can therefore be alleviated by using longer electromagnets, higher resistivity steel or a laminated track core. Rather than use a very long electromagnet, a series of shorter electromagnets that maintain the rail magnetism over a number of electromagnets often carries practical advantages.

In addition to controlled d.c. excitation of the electromagnet coil, controlled a.c. excitation provides a similar characteristic lift force behaviour. However, by suitably configuring a number of multi-phase a.c. windings, a moving magnetic field can be produced which generates a propulsion force component in addition to the lift force component. Unfortunately, a.c. excitation produces a lower lift force compared with d.c. excitation. This is because the mean amplitude of a sinusoidal flux is  $1/\sqrt{2}$  of the d.c. flux level. Since the force is proportional to the square power of the flux, a 50% loss of force results from the use of a.c. rather than d.c. excitation, assuming a given maximum core flux level. A.c. excited cores also suffer from higher leakage flux due to the larger number of narrower slots which are required to accommodate the multi-phase windings. The overall effect is that a.c. excitation requires approximately

double the core size and weight compared with d.c. excitation. The coil must also be larger and heavier since it must encircle the larger core. The rapid cycling of flux associated with typical a.c. excitation means that laminated magnetic steel or iron cores are mandatory. The merits of using an a.c. excited suspension/propulsion electromagnet/motor clearly depend on whether the additional weight and complexity of the combined scheme is less than that required for a separate linear induction/synchronous motor.

The last dynamic effect to be considered is that due to the magnetic hysteresis of the core materials. Hysteresis can be viewed as an effect which modifies the permeability of the core material. It is very difficult to model accurately because it is a nonlinear function of the flux history of the core. Fortunately, the impact of the core hysteresis on the total flux path reluctance can be largely neglected due to the dominance of the air gap reluctance. However, at small air gaps the effect of hysteresis on the lift force is significant and a qualitative consideration must be made when designing the electromagnet suspension control system.

A detailed analysis of an electromagnetic suspension system in terms of the required closed loop bandwidth, vehicle speed and electromagnet deployment is required to determine suitable pole face dimensions, mode of excitation (a.c. or d.c.), and electromagnet and rail core constructions.

### A.5.3 Practical suspension electromagnets

The overview given above of the influence of electromagnet design parameters on both the steady-state and dynamic performance shows the highly interactive nature of suspension electromagnet design. A successful design clearly requires a constrained optimisation, involving all of the critical design factors, and the use of a structured design procedure<sup>1</sup> is a prerequisite. Out of the multitude of possible electromagnet designs, practical and economic considerations have led to the emergence of two distinct configurations. The base configurations both use U-shaped electromagnets with a flat rail to provide a balance between the critical electromagnet parameters listed in Table A.1.

The two configurations which have emerged are characterised by the orientation with which the magnetic flux passes through the rail. This being either perpendicular (transverse flux) or in-line (axial flux) to the rail direction of travel.

**Table A.1** Critical performance parameters for an electromagnetic suspension

---

• Lift force range	• Weight
• Operational air gap range	• Power consumption
• Lateral force stiffness	• Electromagnet cost
• Track velocity range	• Track cost
• Flux time constant	

---

Achieving an acceptable rail core size for transverse flux electromagnets requires the use of long, narrow electromagnet poles (with a typical pole length/width ratio of about 100). Such pole faces are sufficiently narrow to permit the use of solid steel cores for the electromagnet and rail with an acceptable eddy current flux lag, even at high speeds. The alternative axial flux electromagnet configuration can use a relatively square pole face without incurring a rail size penalty. However, the square pole cross-section causes a large flux lag time constant due to eddy currents circulating within the cores. This necessitates the use of either a high resistivity or laminated core for the axial flux electromagnet and a laminated core for its rail,<sup>2</sup> thus incurring a significant additional cost over a solid steel rail core.

There are two main performance advantages that accrue from the use of relatively square pole faces rather than long, narrow pole faces. Firstly, they have a much smaller perimeter which results in shorter, lighter coils, with the additional benefit of lower power consumption. A shorter pole length also leads to significantly reduced leakage flux between the pole pieces. This enables the electromagnet core size and weight to be reduced. An additional refinement is possible when two or more adjacent axial flux electromagnets are required, since they can be combined to share common inner pole coils. This configuration (referred to as an E-core when two U-cores are combined) reduces the coil weight relative to independent electromagnets.

The axial flux configuration is thus capable of providing a performance improvement over the transverse flux configuration in terms of the electromagnet lift/weight and power/lift ratios. This performance improvement is achieved at the expense of the requirement for a laminated rail core and either a high resistivity or laminated electromagnet core.

In order to provide a feel for practical electromagnet configurations, the parameters of the axial flux electromagnets used on the PMG vehicle<sup>3</sup> at Birmingham, and the transverse flux electromagnets used on the University of Sussex experimental vehicle<sup>4</sup>

are listed in Table A.2. Both vehicles use electromagnets with anodised aluminium foil coils wound around the pole pieces. The superior performance of the axial flux electromagnet is illustrated by its lift/weight ratio which is almost double that of the transverse flux electromagnet.

**Table A.2** Parameters of typical axial flux and transverse flux electromagnets

<b>Electromagnet Parameters</b>	<b>Axial Flux</b>	<b>Transverse Flux</b>
<b>Vehicle</b>	PMG Birmingham 8t	Sussex University 1t
<b>Lift capacity</b>	1 t	¼ t
<b>Nominal air gap</b>	15 mm	10 mm
<b>Pole face (length × width)</b>	100 × 50 mm	1000 × 12 mm
<b>Number of flux circuits</b>	2	1
<b>Slot width</b>	100 mm	100 mm
<b>Electromagnet core</b>	E-shaped Magnetic steel	U-shaped Mild steel
<b>Rail core</b>	Laminated Magnetic steel	U-shaped Mild steel
<b>Lift / Weight ratio</b>	11	6
<b>Power / Lift ratio</b>	3 kW/t	2.8 kW/t

The final configuration to be considered is the a.c. excited axial flux electromagnet/motor employed by the combined suspension/propulsion schemes. The induction motor design uses a slotted, laminated electromagnet/motor core excited by multi-phase a.c. windings. The laminated rail incorporates shorted conduction bar coils as found in conventional induction motor rotors. The active track synchronous motor based scheme uses a slotted, laminated rail core, with powered multi-phase a.c. stator coils to provide propulsion and suspension excitation. The matching ‘rotor’ cores also carry coils which are used to control the suspension lift force. These combined systems have the obvious advantage of not requiring a separate and heavy propulsion motor and aluminium guideway reaction rail. However, a.c. excitation requires double the electromagnet and rail core size and weight plus a much heavier coil compared to d.c. excitation. An additional drawback for the linear induction motor scheme is that the rail cost is higher than a normal laminated rail due to the conduction bars. The extreme expense of the rail core and coils and the associated power controllers for the active



track linear synchronous motor scheme are justified only for very high speed systems. The active track overcomes the problem of trying to supply many megawatts of propulsion power in a non-contacting fashion to a vehicle travelling at speeds of up to 500 km/h. It is interesting to note that the force of attraction between the stator and 'rotor' of the linear synchronous motor would in most other applications probably be regarded as an undesirable parasitic effect.

## A.6 References

- 1 Sinha, P. K.: 'Electromagnetic suspension: Dynamics & control', Peter Peregrinus, London, Chapter 6, 1987.
- 2 Yamamura, S. and Yamaguchi, H.: 'Electromagnetic Levitation System by means of salient pole type magnets coupled with laminated slotless rails', *IEEE Trans. on Veh. Tech.*, **VT-39**, 1990, pp 83-7.
- 3 Nenadovic, V. and Riches, E.E.: 'Maglev at Birmingham Airport: from system concept to successful operation', *GEC Review*, **1**, 1985, pp 3-17.
- 4 Jayawant, B.V., Sinha, P.K., Wheeler, A.R., Whorlow, R.J. and Willsher, J.: 'Development of a 1-ton magnetically suspended vehicle using controlled d.c. electromagnets', *Proc. IEE, Pt. A*, **123**, 1976, pp 941-8.

# Appendix B

---

## Electromagnet force control

### B.1 Open-loop electromagnet force/voltage transfer function

The air gap flux,  $\Phi$ , of the electromagnet is approximately proportional to the coil current,  $I$ , divided by the air gap,  $C$ , (see Equation 2.27). This nonlinear flux behaviour can be linearised for small perturbations and represented in the frequency domain by the Laplace transfer function given by:

$$\Delta\Phi(s) = k_{\phi i} \Delta I(s) - k_{\phi c} \Delta C(s) \quad \text{where} \quad k_{\phi i} = \frac{\partial\phi(i_o, c_o)}{\partial i}, \quad k_{\phi c} = -\frac{\partial\phi(i_o, c_o)}{\partial c} \quad \mathbf{B.1}$$

The same treatment applied to the electromagnet force,  $F$ , (see Equation 2.25), which is approximately proportional to the square power of the air gap flux, gives:

$$\Delta F(s) = k_{f\phi} \Delta\Phi(s) \quad \text{where} \quad k_{f\phi} = \frac{\partial f(i_o, c_o)}{\partial \phi} \quad \mathbf{B.2}$$

The dynamic relationship between electromagnet coil voltage,  $V$ , coil current, and air gap flux, (see Equation 2.26), is given by:

$$\Delta V(s) = sN \Delta\Phi(s) + R_{coils} \Delta I(s) \quad \mathbf{B.3}$$

where  $N$  is the number of coil turns, and  $R_{coils}$  is the coil resistance. Finally, the acceleration of the suspended load due to the electromagnet force is given by:

$$s^2 \Delta C(s) = -\frac{\Delta F(s)}{m} \quad \mathbf{B.4}$$

where  $m$  is the total load mass. Equation B.1 is now rearranged to form an expression for the current in terms of the flux and air gap, this gives:

$$\Delta I(s) = \frac{1}{k_{\phi i}} \Delta \Phi(s) + \frac{k_{\phi c}}{k_{\phi i}} \Delta C(s) \quad \text{B.5}$$

This current expression is substituted into Equation B.3, giving:

$$\Delta V(s) = sN \Delta \Phi(s) + \frac{R_{coils}}{k_{\phi i}} \Delta \Phi(s) + \frac{R_{coils} k_{\phi c}}{k_{\phi i}} \Delta C(s) \quad \text{B.6}$$

Equation B.2 is now rearranged to form an expression for flux in terms of force, this gives:

$$\Delta \Phi(s) = \frac{\Delta F(s)}{k_{f\phi}} \quad \text{B.7}$$

This flux expression is substituted into Equation B.6, giving:

$$\Delta V(s) = \frac{\Delta F(s)}{k_{f\phi}} \left( sN + \frac{R_{coils}}{k_{\phi i}} \right) + \frac{k_{\phi c} R_{coils}}{k_{\phi i}} \Delta C(s) \quad \text{B.8}$$

Equation B.4 is now rearranged to give an expression for air gap in terms of forces by:

$$\Delta C(s) = - \frac{\Delta F(s)}{ms^2} \quad \text{B.9}$$

This air gap expression is substituted into Equation B.8, giving:

$$\Delta V(s) = \frac{\Delta F(s)}{k_{f\phi}} \left( sN + \frac{R_{coils}}{k_{\phi i}} - \frac{k_{f\phi} k_{\phi c} R_{coils}}{k_{\phi i} ms^2} \right) \quad \text{B.10}$$

This can now be rearranged to give the electromagnet force/voltage transfer function:

$$\frac{\Delta F(s)}{\Delta V(s)} = \frac{k_{f\phi} k_{\phi i}}{R_{coils}} \frac{s^2}{\left( s^3 N k_{\phi i} / R_{coils} + s^2 - k_{f\phi} k_{\phi c} / m \right)} \quad \text{B.11}$$

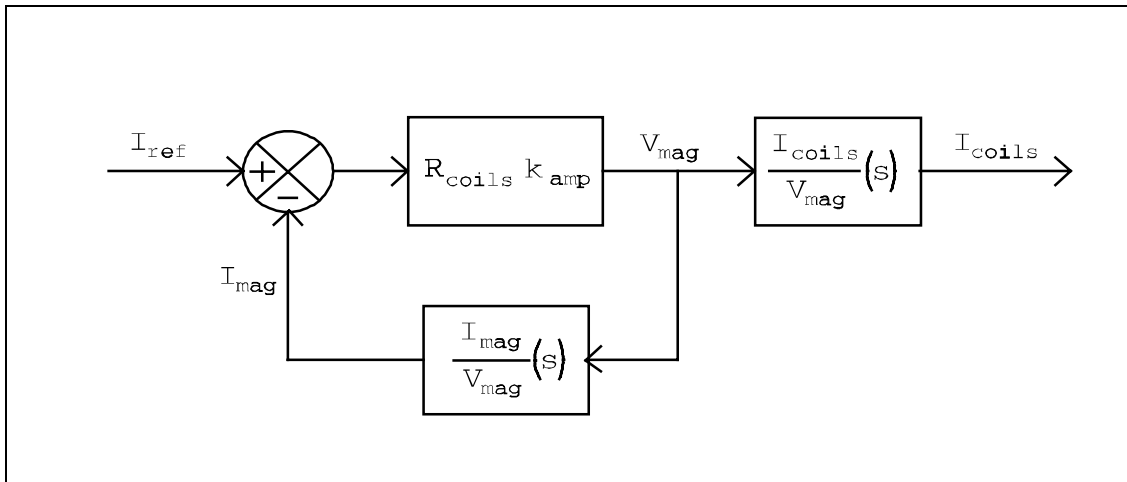
For convenience, it is noted that (see Equations 2.27 and 2.29):

$$k_{\phi i} = \frac{\partial \phi}{\partial i} = \frac{\partial}{\partial i} \left( \frac{L_{coils} i}{N} \right) = \frac{L_{coils}}{N}, \quad \text{B.12}$$

$$\therefore L_{coils} = N k_{\phi i}, \quad T_{coil} = \frac{L_{coils}}{R} = \frac{N k_{\phi i}}{R}$$

## B.2 Closed-loop current feedback transfer function

The transfer function for the electromagnet current feedback loop is now analysed. Figure B.1 shows the configuration of the current feedback controller, where  $k_{amp}$  is the current loop gain,  $V_{mag}$  is the applied electromagnet coil voltage,  $I_{mag}$  is the electromagnet current, and  $I_{coils}$  is the component of the electromagnet current which produces the suspension force. The open-loop electromagnet transfer functions  $I_{coils}/V_{mag}(s)$  and  $I_{mag}/V_{mag}(s)$  are derived in Appendix A, Section 3.



**Figure B.1** Configuration of the closed-loop current feedback control

The closed-loop transfer function in terms of the Laplace operator  $s$ , is given by:

$$\frac{I_{coils}(s)}{I_{ref}(s)} = \frac{R_{coils} k_{amp} \frac{I_{coils}(s)}{V_{mag}}}{1 + R_{coils} k_{amp} \frac{I_{mag}(s)}{V_{mag}}} \quad \text{B.13}$$

Expanding the two open-loop transfers functions gives:

$$\frac{I_{coils}(s)}{I_{ref}(s)} = \frac{R_{coils} k_{amp} \left( \frac{1}{R_{coils}} \frac{1}{1 + s(T_{coils} + T_{eddy})} \right)}{1 + R_{coils} k_{amp} \left( \frac{1}{R_{coils}} \frac{1 + sT_{eddy}}{1 + s(T_{coils} + T_{eddy})} \right)} \quad \text{B.14}$$

This can be simplified to give:

$$\frac{I_{coils}(s)}{I_{ref}(s)} = \frac{k_{amp}}{1 + s(T_{coils} + T_{eddy}) + k_{amp}(1 + sT_{eddy})} \quad \text{B.15}$$

For large values of feedback gain  $k_{amp}$ , this can be approximated by:

$$\frac{I_{coils}(s)}{I_{ref}(s)} \approx \frac{1}{1 + s\left(\frac{T_{coils}}{k_{amp}} + T_{eddy}\right)} \quad \text{where } k_{amp} \gg 1 \quad \text{B.16}$$

Equation B.16 shows that the use of current feedback reduces the time constant due to the electromagnet coil, but not the time constant due to the eddy currents circulating within the cores.

### B.3 Matlab models for root loci generation

```
% MatLab Script f_locus.m
%
% This script produces a root locus plot for force feedback
%
% Author: N. S. McLagan
% Last modified: 11th December, 1990
%
% Electromagnet/amplifier parameters
Tflux = 0.116
kc = 950000
mass = 15
% Gain factor range
kmax = 120
k = [ 0:0.005:0.135, 0.1409811442, 0.141, 1 ];
% H(s) numerator & denominator
num = [ kmax, 0, 0 ]
den = [ Tflux, 1, 0, -kc/mass ]
p = rlocus( num, den, [0] )
r = rlocus( num, den, k );
a = rlocus( num, den, [1] );
axis([-200, +100, -100, +100])
plot( real(r), imag(r), '-' )
text( real(p)-1.5, imag(p)-2.4, 'X' )
text( real(a(2))-1.5, imag(a(2))-2.4, '>' )
text( real(a(3))-1.5, imag(a(3))-2.4, '<' )
grid
!del f_locus.met
meta f_locus.met % Put current plot into temporary metafile
!gpp f_locus /dhpgl % Invoke GPP to convert to HPGL
```

```
% MatLab Script c_locus.m
%
% This script produces a root locus plot for air gap feedback
%
%       Author:  N. S. McLagan
% Last modified: 12th December, 1990
%

% Electromagnet/amplifier parameters
Tflux = 0.0057
kc = 950000
mass = 15

% Gain factor range
kmin = 0
kmax = 2
k = [ kmin:0.05:0.9, 0.92800303825, 1.000001, 1.05:0.05:kmax ];

% H(s) numerator & denominator
num = [ 0 0 kc/mass ]
den = [ Tflux 1 0 -kc/mass ]

p = rlocus( num, den, [kmin] )
r = rlocus( num, den, k );
a = rlocus( num, den, [kmax] );
axis([-400, +200, -200, +200])
plot( real(r), imag(r), '-' )
text( real(p)-3, imag(p)-4.8, 'X' )
text( real(a(1))-3, imag(a(1))-4.8, '<' )
grid

!del c_locus.met
meta c_locus.met           % Put current plot into temporary metafile
!gpp c_locus /dhpgl       % Invoke GPP to convert to HPGL
```

# Appendix C

---

## Suspension mode control

### C.1 Position control system transfer function

This section details the derivation of the Laplace transfer function of the suspension position control system illustrated in Figure 4.4. The Laplace transform of the control law for the position controller is given by:

$$F_{demand}(s) = - \left( k_{pos} + \frac{k_{pos}}{sT_{err}} \right) \left( \frac{s^2 Z(s)}{(s + \omega_{int})^2} - Z_{ref}(s) \right) - k_{vel} \frac{s^2 Z(s)}{(s + \omega_{int})} - k_{acc} s^2 Z(s) \quad \text{C.1}$$

where  $Z$  is the position,  $Z_{ref}$  is the position reference, and the feedback gains are denoted by:  $k_{pos}$  - position error (stiffness),  $T_{err}$  - error integral (time constant),  $k_{vel}$  - velocity (damping),  $k_{acc}$  - acceleration (virtual mass), and  $\omega_{int}$  is the low frequency cutoff point for the state integrators. This equation is rearranged for later convenience, giving:

$$F_{demand}(s) = - \frac{Z(s)}{(s + \omega_{int})^2} \left[ s \frac{k_{pos}}{T_{err}} + s^2 k_{pos} + s^2 (s + \omega_{int}) k_{vel} + s^2 (s + \omega_{int})^2 k_{acc} \right] + \frac{Z_{ref}(s)}{s} \left[ \frac{k_{pos}}{T_{err}} + s k_{pos} \right] \quad \text{C.2}$$

The acceleration of the suspended load due to the control force demand and a disturbance force is given by:

$$s^2 Z(s) = \frac{F_{demand}(s)}{m(1 + sT_{force})} + \frac{F_{disturb}(s)}{m} \quad \text{C.3}$$

where  $F_{disturb}$  is the disturbance force,  $T_{force}$  is the force actuation time constant, and  $m$  is the suspended mass. This is also rearranged for convenience, giving:

$$F_{demand}(s) = s^2(1+sT_{force})m Z(s) - (1+sT_{force}) F_{disturb}(s) \quad \text{C.4}$$

The Laplace transform of the closed-loop position/disturbance force transfer function can now be determined by equating the control force demand of Equation C.2 and Equation C.4, this gives:

$$\begin{aligned} \frac{Z(s)}{(s+\omega_{int})^2} & \left[ s \frac{k_{pos}}{T_{err}} + s^2 k_{pos} + s^2(s+\omega_{int})k_{vel} + s^2(s+\omega_{int})^2 k_{acc} + s^2(1+sT_{force})(s+\omega_{int})^2 m \right] \\ & = \frac{Z_{ref}(s)}{s} \left[ \frac{k_{pos}}{T_{err}} + s k_{pos} \right] + F_{disturb}(s) (1+sT_{force}) \end{aligned} \quad \text{C.5}$$

As an intermediate step, it is useful to expand the terms which comprise the characteristic polynomial of the closed-loop transfer function. The characteristic polynomial is thus given by:

$$\begin{aligned} CharPoly(s) & = s \frac{k_{pos}}{T_{err}} + s^2 k_{pos} + s^3 k_{vel} + s^2 \omega_{int} k_{vel} + s^4 k_{acc} + 2s^3 \omega_{int} k_{acc} + s^2 \omega_{int}^2 k_{acc} \\ & + s^4 m + 2s^3 \omega_{int} m + s^2 \omega_{int}^2 m + s^5 m T_{force} + 2s^4 \omega_{int} m T_{force} + s^3 \omega_{int}^2 m T_{force} \end{aligned} \quad \text{C.6}$$

Equation C.5 can now be rearranged with the help of Equation C.6 to obtain the closed-loop transfer function of the position control system in terms of the position reference input and the disturbance force input. This yields:

$$\frac{Z(s)}{Z_{ref}(s)} = \frac{k_{pos} (s+1/T_{err}) (s+\omega_{int})^2}{s^6(mT_{force}) + s^5(k_{acc} + m + 2\omega_{int}mT_{force}) + s^4(k_{vel} + 2\omega_{int}(k_{acc} + m) + \omega_{int}^2mT_{force}) + s^3(k_{pos} + \omega_{int}^2(k_{acc} + m) + \omega_{int}k_{vel}) + s^2(k_{pos}/T_{err})} \quad \text{C.7}$$

$$\frac{Z(s)}{F_{disturb}(s)} = \frac{(1+sT_{force})(s+\omega_{int})^2}{s^5(mT_{force}) + s^4(k_{acc} + m + 2\omega_{int}mT_{force}) + s^3(k_{vel} + 2\omega_{int}(k_{acc} + m) + \omega_{int}^2mT_{force}) + s^2(k_{pos} + \omega_{int}^2(k_{acc} + m) + \omega_{int}k_{vel}) + s(k_{pos}/T_{err})} \quad \text{C.8}$$



## C.2 ACSL model of electromagnet suspension control system

```

Program Maglev
"---- Single Electromagnet Suspension System Simulation"

"---- Features: - Nonlinear electromagnet model"
"----           - Nonlinear force controller"
"----           - Absolute position controller (P+I+D+DD)"
"----           - Guideway following filter (2 pole)"

"---- Author: Neil McLagan"
"---- Last modified: 4-2-91"

"---- All variables are in elementary units (eg. secs, metres, newtons)"
"---- unless the variable name suggests otherwise, eg. gap.mm"

Initial
  "---- Electromagnet characteristics"
  Constant Rcoil = 0.79
  Table Lcoil, 1, 3 / 0.001, 0.003, 0.005, 0.088, 0.067, 0.059 /
  Table Teddy, 1, 3 / 0.001, 0.003, 0.005, 0.005, 0.003, 0.002 /
  "---- Electromagnet force = kForce * I^2 / G^2"
  Constant kForce = 44.8E-6
  Constant Fmin = 1.0, Fmax = 1000.0
  Constant Mass = 15.0

  "---- Current Amplifier characteristics"
  Constant kIerr = 100.0 $ "Closed-loop gain"
  Constant Vmax = 30.0 $ "Supply voltage"
  Constant Imin = 0.0, Imax = 20.0
  Constant DeltaI = 0.005 $ "DAC resolution"

  "---- Disturbance characteristics"
  Constant Ride = 1.5E-3, Tstart = 0.1, Ts = 0.0
  Constant StpSiz = 1.0E-3, StpWid = 2.5
  Constant MinGap = 0.5E-3, MaxGap = 10.0E-3

  "---- Feedback sensor time constants and quantization"
  Constant TgapS = 0.80E-3, deltaG = 5.0E-6
  Constant TaccS = 0.45E-3, deltaA = 5.0E-3

  "---- Acceleration signal high-pass filter (H/W) time constant"
  Constant TaccF = 1.5

  "---- Absolute position controller feedback gains"
  Constant Steady = 1.0 $ "-- s"
  Constant Stiff = 250000.0 $ "-- N/m"
  Constant Damp = 6500.0 $ "-- N/(m/s)"
  Constant Vmass = 15.0 $ "-- kg (virtual mass)"

  "---- Other time constants"
  Constant Tfollo = 0.04 $ "Guideway following cutoff freq: 4 Hz"
  Constant Tinteg = 1.6 $ "State integration cutoff freq: 0.1 Hz"
  Constant Tforce = 0.0015 $ "Required force actuation time constant"

  "---- Initialise feedback signals"
  Idem = 0.0
  Gap = MinGap
  Gapmm = Gap * 1000.0
  Pi = 3.1415926

```

```

"---- Simulation control"
Constant Tstop = 8.0
Tdisp = Tstop - 2.0 * StpWid

End $ " of Initial"

Dynamic
Termt( t .ge. Tstop)
Td = t - Ts
Tdisp = Tstop - 2.0 * StpWid

Cinterval Tcomm = 10.0E-3 $ "Communication interval"
Algorithm Ialg=3 $ "Euler integration"

Derivative Magnet $ "Electromagnet and Current Amplifier"

Maxterval Tmagss = 0.1E-3 $ "Integration step size"
Nsteps Msteps = 1

Procedural

"---- Closed loop magnet current controller"
Vmag = Bound( -Vmax, Vmax, KIerr * (Idem - Imag) )

"---- Apply coil flux lag to electromagnet "
Imag = RealPl( Lcoil(Gap)/Rcoil, Vmag/(Rcoil*Gap) ) * Gap

"---- Apply eddy current flux lag to electromagnet"
Flux = RealPl( Teddy(Gap), Imag/Gap )

"---- Limits for magnet movement (clamped initially)"
LowLim = FcnSw( t-Tstart, ride, MinGap, MinGap)
UprLim = FcnSw( t-Tstart, ride, MaxGap, MaxGap)

"---- Static electromagnet force characteristic"
Fmag = Bound(Fmin, Fmax, kForce * (Flux*Flux) )

"---- Magnet acceleration, velocity & position"
Acc = 9.81 - (Fmag / Mass)
DblInt(Pos, Vel = 0.0, Acc, 0.0, LowLim, UprLim)
Gap = Bound( MinGap, MaxGap, Pos )
Gapmm = Gap * 1000.0

"---- Air gap and acceleration feedback sensors"
GapFB = RealPl( TgapS, Gap, MinGap )
AccFB2 = RealPl( TaccS, Acc )
AccFB1 = RealPl( TaccS, AccFB2 )

"---- Acceleration high-pass filter (analogue)"
AccFB = AccFB1 - RealPl( TaccF, AccFB1 )

End $ " of Procedural"
End $ " of Derivative Electromagnet & Current Amplifier Model"

```

```

Discrete Contro $ "Discrete time digital controller"

Interval Tsampl = 0.8E-3 $ "Controller sampling interval"
Procedural

"---- Position step input reference"
GapRef = Ride + Bound(0.0, StpSiz, -1.0E6 * SIN(Pi*t/StpWid) )

"---- Feedback sensor Quantization"
AccQ = Bound( -9.81, +9.81, Qntzr(deltaA, AccFB) )
GapQ = Bound( 0.0, 10.0E-3, Qntzr(deltaG, GapFB) )

"---- Calculate Magnet acc, vel, pos & Track pos"
AccHP = AccQ - RealPl( Tinteg, AccQ )
VelHP = RealPl( Tinteg, AccHP * Tinteg )
PosHP = RealPl( Tinteg, VelHP * Tinteg )
TrkHP = (GapRef + PosHP) - GapQ

"---- Apply Guideway following filter"
TrkFl = RealPl( Tfollo, TrkHP )
PosRef = RealPl( Tfollo, TrkFl )

"---- Absolute position controller"
PosErr = PosHP - PosRef
AccDem = Vmass * AccHP
VelDem = Damp * VelHP
PosDem = Stiff * PosErr
SseDem = (Stiff/Steady) * LimInt(PosErr,0.0,-0.02,+0.02)

"---- Steady-state, position, velocity, acceleration demand"
Fdem = (9.81 * Mass) + AccDem + VelDem + PosDem + SseDem

"---- Determine required magnet current"
Fsqrt = SQRT( Bound( Fmin, Fmax, Fdem ) / kForce )
Idem = Qntzr( deltaI, LedLag(Teddy(0.001), Tforce, Fsqrt*gapQ) )

End $ " of Procedural"
End $ " of Discrete Controller"
End $ " of Dynamic "
End $ " of Maglev Simulation "

```

# Appendix D

---

## Control system hardware

This Appendix lists the specifications of the industrial accelerometer and air gap sensor, and the schematic diagrams for all of the control system hardware. The various system components are listed below:

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## D.1 Accelerometer

The Model 3110 is a general purpose, solid-state, piezo-resistive accelerometer with built-in amplification and temperature compensation. The module consists of a silicon micro-machined accelerometer.

### ICSensors, accelerometer, model 3110-002, specifications.

(Supply voltage = 10 Vdc, Ambient temperature = 25 °C)

PARAMETERS	Min	Typ	Max	Units	Notes
Range		±2		g	
Frequency Response		0-350		Hz	
Mounted Resonant Frequency		600		Hz	
Full Scale Output (- Acc)		0.5		Volts	1
Full Scale Output (+ Acc)		4.5		Volts	1
Full Scale Output Span	3.96	4.00	4.04	Volts	1
Zero Acceleration Output	2.48	2.5	2.52	Volts	1
Damping Factor		0.7			2
Accuracy		0.2	1.0	±%Span	3
Transverse Sensitivity		1.0	3.0	±%Span	
Temperature Coefficient - Span		1.0	2.0	±%Span	4
Temperature Coefficient - Zero		1.0	2.0	±%Span	4
Supply Voltage	8.0	10.0	30.0	Volts	
Supply Current		5.0		mA	
Output Resistance		0.1		Ω	
Output Noise		0.5		mV p-p	
Output Load Resistance	2			kΩ	
Acceleration Limits		20x		Rated	
Operating Temperature	-20		+85	°C	
Storage Temperature	-40		+125	°C	
Weight (Excluding Cable)		23		Grams	

**Notes**

1. The output voltage increases from the Zero Acceleration Output for positive acceleration and decreases for negative acceleration. The sensitivity is then 2V/Range.
2. The 0.7 damping factor represents critical damping. The damping factor is controlled to within  $\pm 10\%$  over the entire operating temperature range. Alternate damping factors are available on a special order basis.
3. Includes repeatability, hysteresis and linearity (best straight line fit).
4. Compensated temperature range: 0 to 50 °C in reference to 25 °C.
5. See Model 3021 for an accelerometer without amplification and compensation.
6. Pin 2 provides an optional 2.5 V reference which may be used, if desired, to provide a stable zero-g reference. Thus, the full scale differential output between Pin 2 and Pin 4 would be  $\pm 2$  Vdc. If a single-ended output signal is preferred (0.5-4.5 Vdc), make no connection to Pin 2.

**ICSensors, Model 3110, Pin connections.**

<b>Pin:</b>	1	2	3	4	5
<b>Function:</b>	Ground	Zero-g ref.	Supply (+)	Output	Test point

## D.2 Air gap sensor

The non-contacting air gap sensor used is a general purpose device, which uses the power loss due to eddy currents in the target to determine the air gap or material properties. For accurate measurement of air gap, the resistivity of the target must remain constant, ie. known material and constant temperature.

### Pepperl+Fuchs, Inductive displacement sensor, model IA8-M1K-I3, specifications.

PARAMETERS	VALUES
Sensing Range	3mm - 8 mm
<b>Nominal Values:</b>	
Damping plate, 1mm St 37	35 mm x 35 mm
Linearity (rel. to FSD)	$\pm 3\%$
Zero Tolerance	$\pm 2\%$
Working Voltage	15 to 30 V dc
Cut-off Frequency (3 dB)	$\approx 190$ Hz
Repeatability Accuracy	$\leq 15$ $\mu\text{m}$
Hysteresis Error	$\leq 30$ $\mu\text{m}$
<b>Electrical Data:</b>	
Output Signal	0 - 20 mA
Load Resistance $R_L$	0..500 $\Omega$
Quiescent Current Consumption	< 8 mA
Ripple Current (measured @ $R_L=100\Omega$ )	$\approx \pm 1.5\%$ FSD
Temperature Drift (target & transducer at same temperature)	$\approx \pm 1$ %/K FSD
Current Consumption max.	$\leq 35$ mA
<b>Mechanical Data:</b>	
Ambient Temperature	-10 to +70 °C
Protection class to DIN 40 050	IP 67
Permissible shock and vibration stresses	b $\leq 30$ g, T $\leq 11$ ms f $\leq 55$ Hz, a $\leq 1$ mm
Type of connection	Wire, $\phi \leq 2.5\text{mm}^2$

The useable sensing range with the MAGLEV track as target is about 3 mm - 10 mm, with distances above 8 mm being outside the rated specification (see full data sheet).



### D.3 Equipment chassis configurations

All equipment chassis are 3U high and 84E wide, ie. for single height, short eurocards (160 x 100 mm). The single electromagnet suspension contains all cards and modules in one chassis, whilst the multi-magnet vehicle uses 2 chassis: one with the DAC and the power controllers, and the other with the ADCs, processors and PSUs.

#### D.3.1 Single electromagnet suspension system

##### Logic & Power Control Chassis

<b>Card:</b>	E M C A	P S U	-	D A C	-	T M B	T M B	I P I F	A D C	S A P	C O N N
<b>Width:</b>	20	10	4	4	4	10	10	4	4	4	10

#### D.3.2 Vehicle suspension system

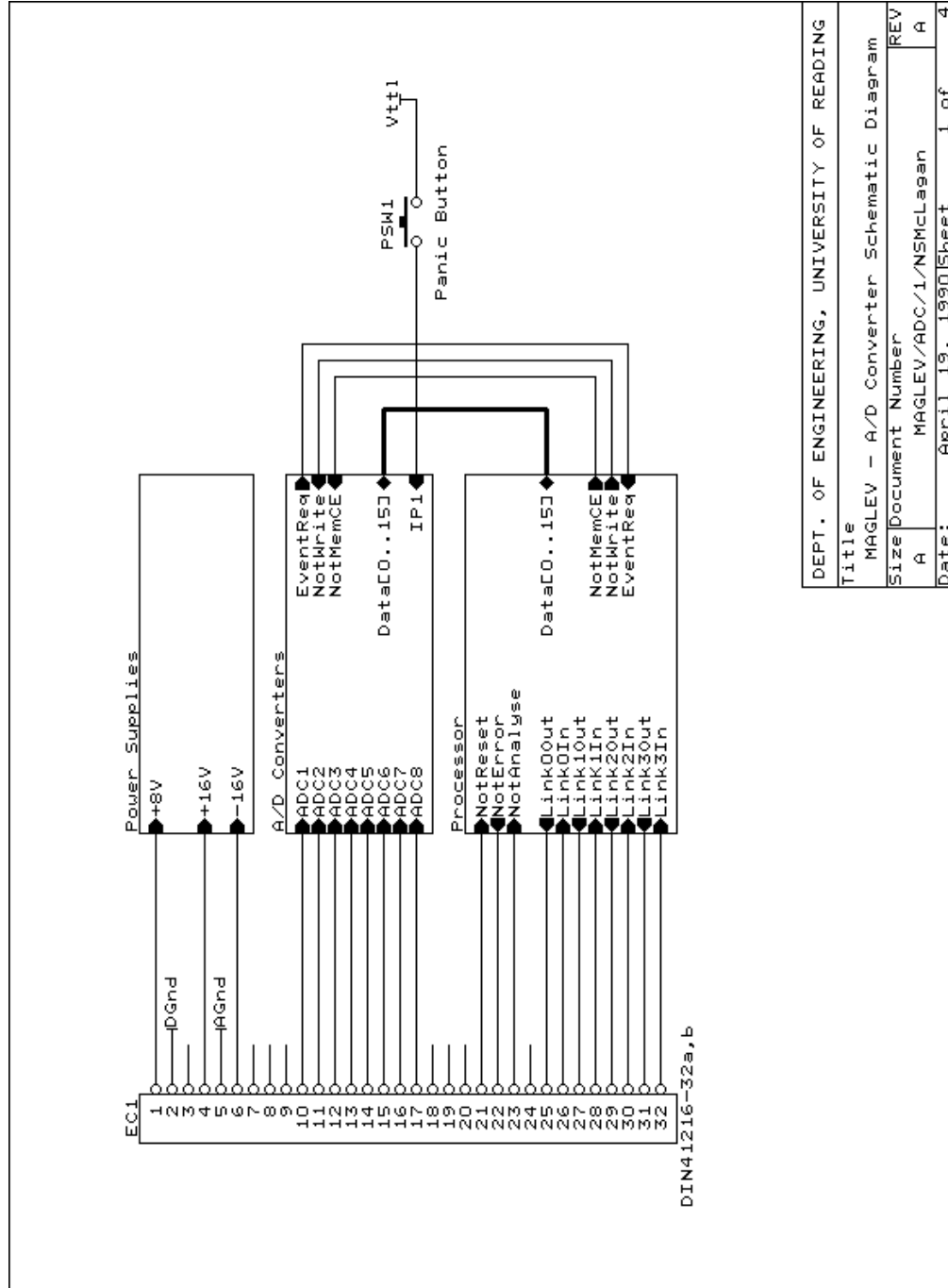
##### Logic Control Chassis

<b>Card:</b>	P S U	P S U	-	O P I F	T M B	T M B	T M B	I P I F	-	A D C	S A P	C O N N
<b>Width:</b>	10	10	4	4	10	10	10	4	4	4	4	10

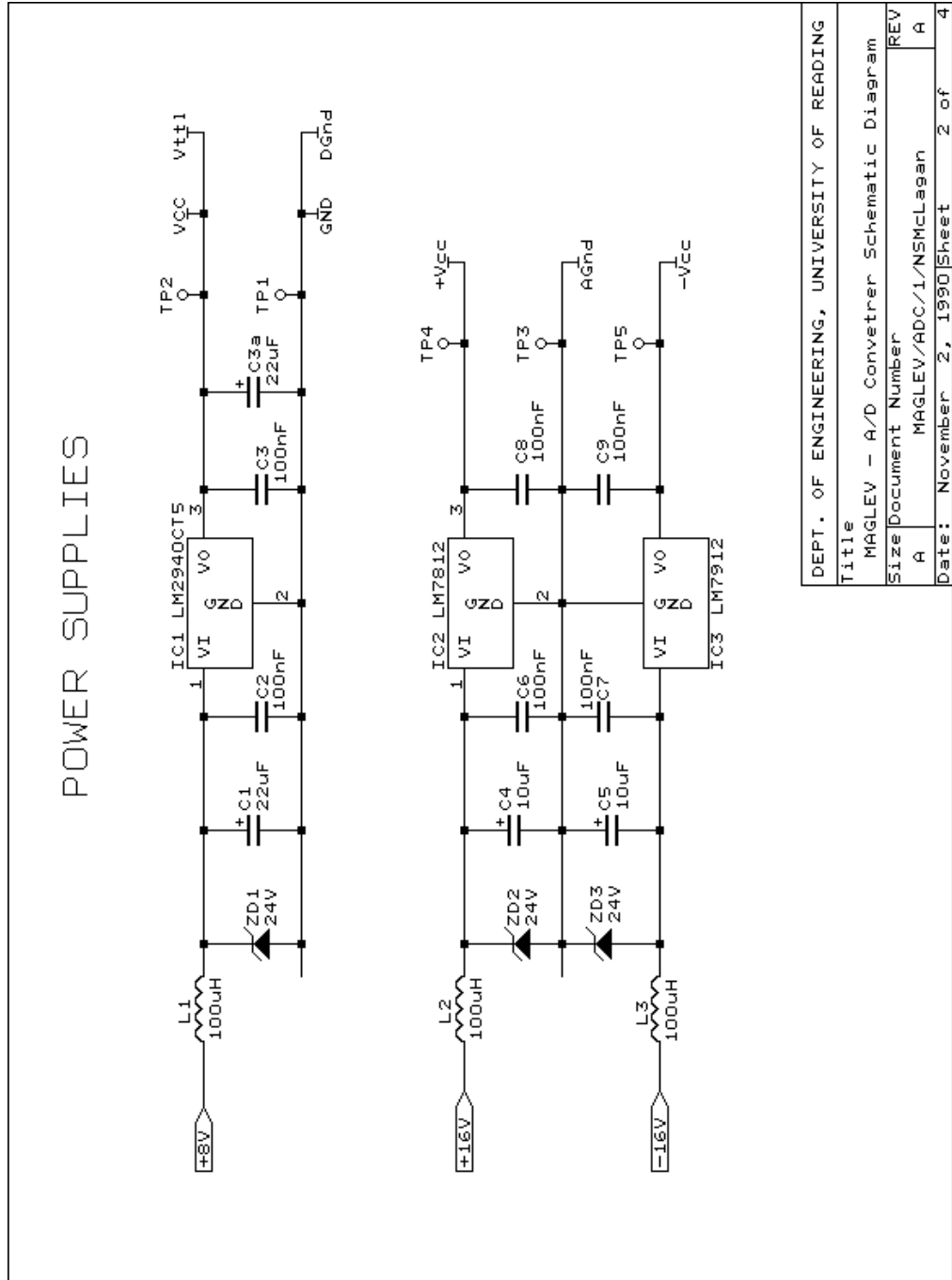
##### Power Control Chassis

<b>Card:</b>	E M C A	E M C A	E M C A	E M C A	D A C
<b>Width:</b>	20	20	20	20	4

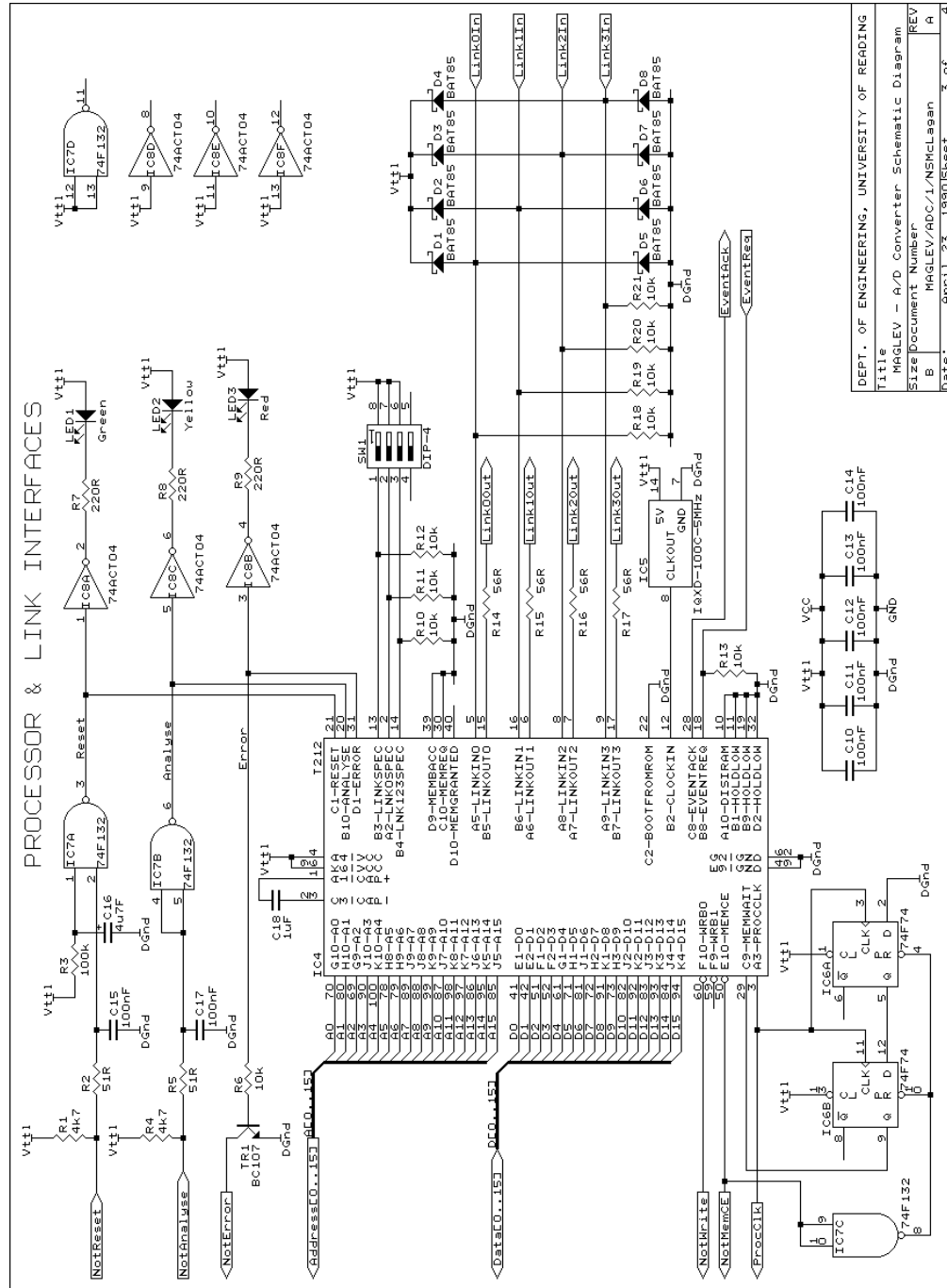
D.4 Analogue-to-digital converter (8 channel) card



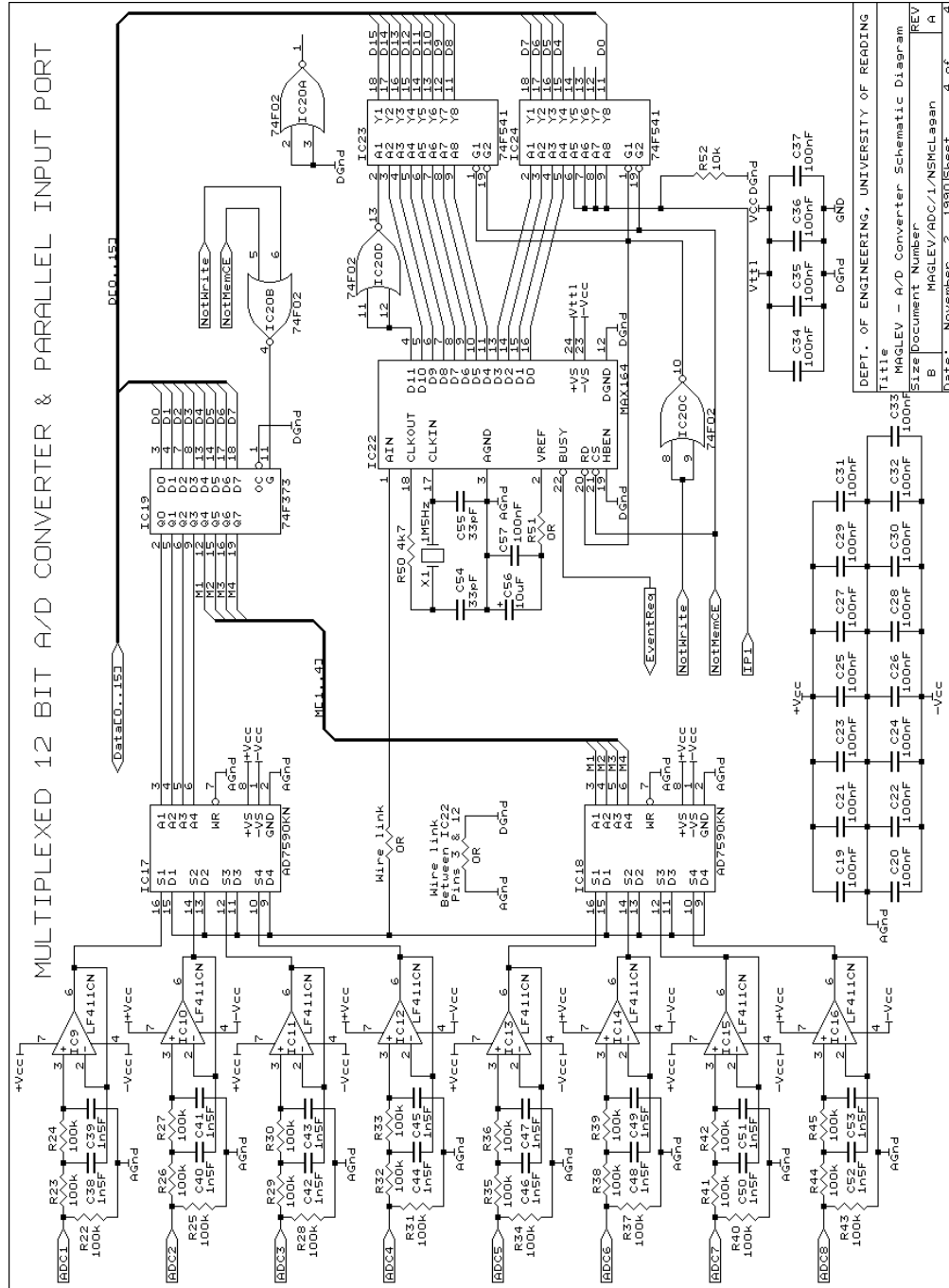
D.4.1 ADC card power supplies



D.4.2 ADC processor & link interfaces



D.4.3 ADC anti-alias filters, multiplexer & converter



## D.4.4 ADC card component parts list

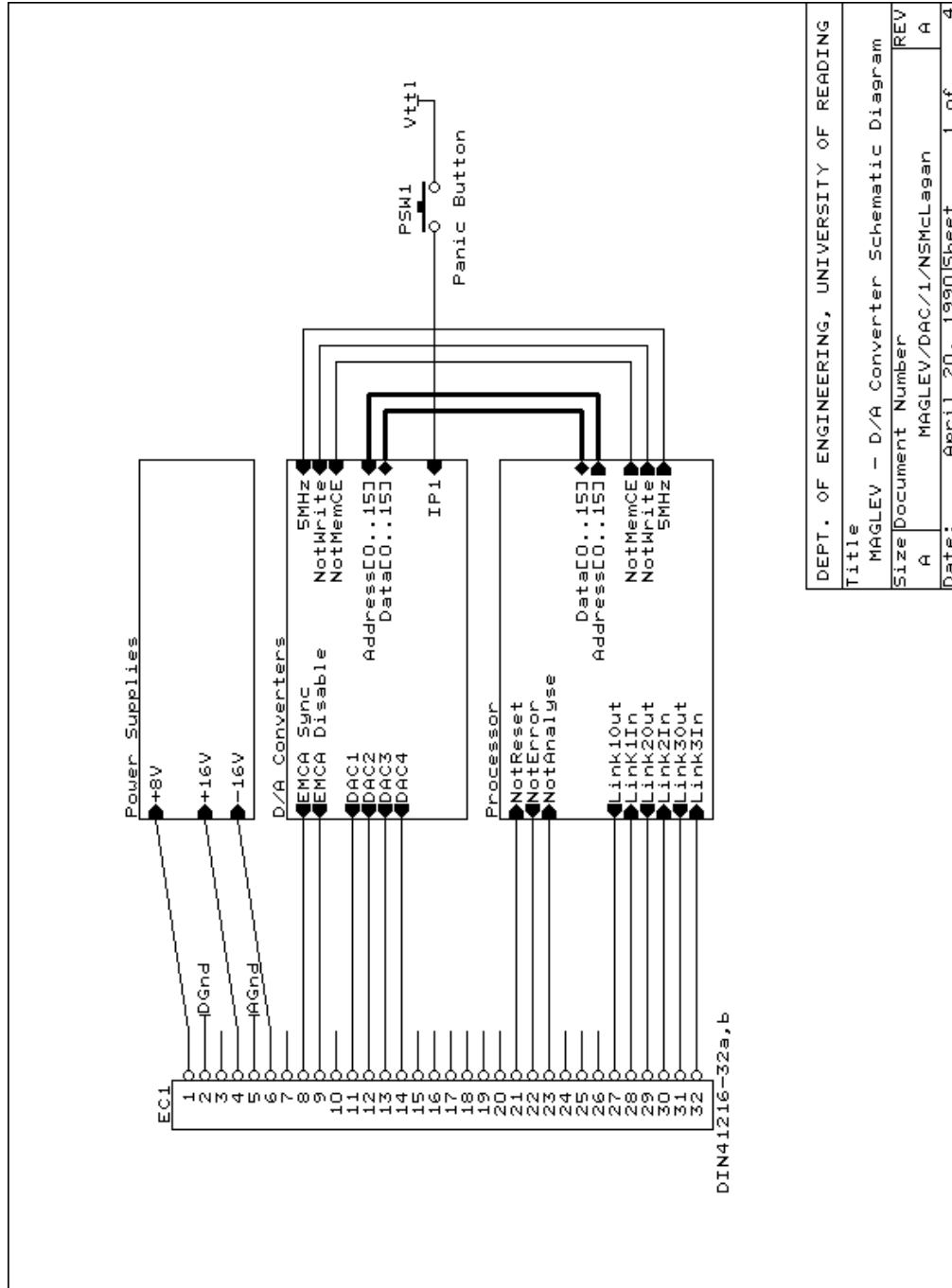
MAGLEV - A/D Converter Schematic Diagram  
MAGLEV/ADC/1/N.S.McLagan

Revised: November 2, 1990  
Revision: A

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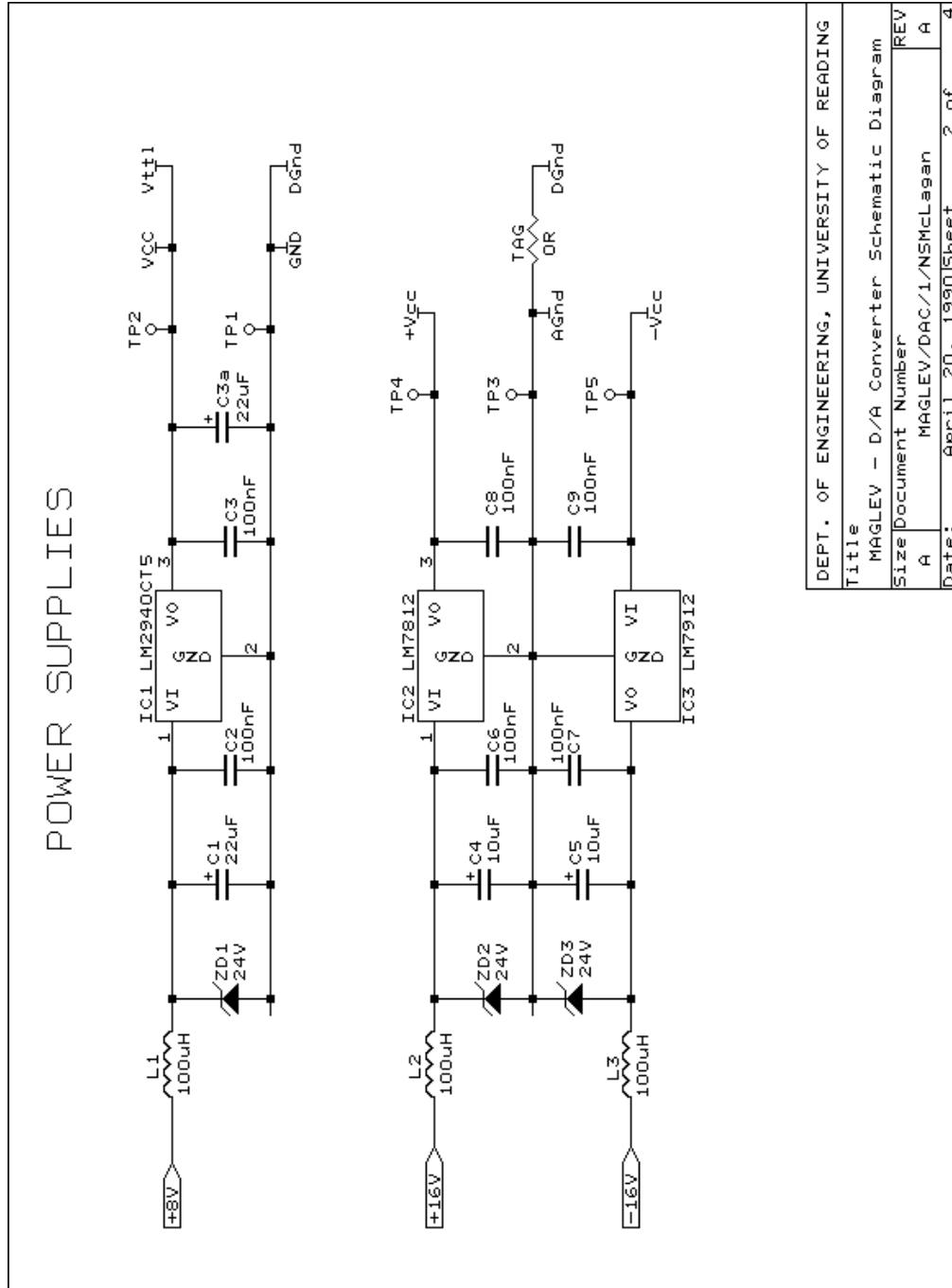
<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
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1	C16	4u7F
1	C18	1uF
34	C2, C3, C6, C7, C8, C9, C10, C11, C12, C13, C14, C15, C17, C19, C20, C21, C22, C23, C24, C25, C26, C27, C28, C29, C30, C31, C32, C33, C34, C35, C36, C37, C57, C58	100nF
16	C38, C39, C40, C41, C42, C43, C44, C45, C46, C47, C48, C49, C50, C51, C52, C53	1n5F
3	C4, C5, C56	10uF
2	C54, C55	33pF
8	D5, D1, D2, D3, D4, D6, D7, D8	BAT85
1	EC1	DIN41216-32a, b
1	IC1	LM2940CT5
8	IC16, IC9, IC10, IC11, IC12, IC13, IC14, IC15	LF411CN
2	IC17, IC18	AD7590KN
1	IC19	74F373
1	IC2	LM7812
1	IC20	74F02
1	IC22	MAX164BCNG
2	IC23, IC24	74F541
1	IC3	LM7912
1	IC4	T212
1	IC5	IQXD-100C-5MHz
1	IC6	74F74
1	IC7	74F132
1	IC8	74ACT04
3	L2, L1, L3	100uH
1	LED1	Green
1	LED2	Yellow
1	LED3	Red
1	PSW1	Push Switch
3	R1, R4, R50	4k7
4	R15, R14, R16, R17	56R
2	R2, R5	51R
25	R3, R22, R23, R24, R25, R26, R27, R28, R29, R30, R31, R32, R33, R34, R35, R36, R37, R38, R39, R40, R41, R42, R43, R44, R45	100k
1	R51	Wire link
10	R6, R10, R11, R12, R13, R18, R19, R20, R21, R52	10k
3	R7, R8, R9	220R
1	SW1	DIP-4 way SPST
5	TP2, TP1, TP3, TP4, TP5	Test pins
1	TR1	BC107
1	X1	1.5 MHz crystal
3	ZD1, ZD2, ZD3	24V

D.5 Digital-to-analogue converter (4 channel) card



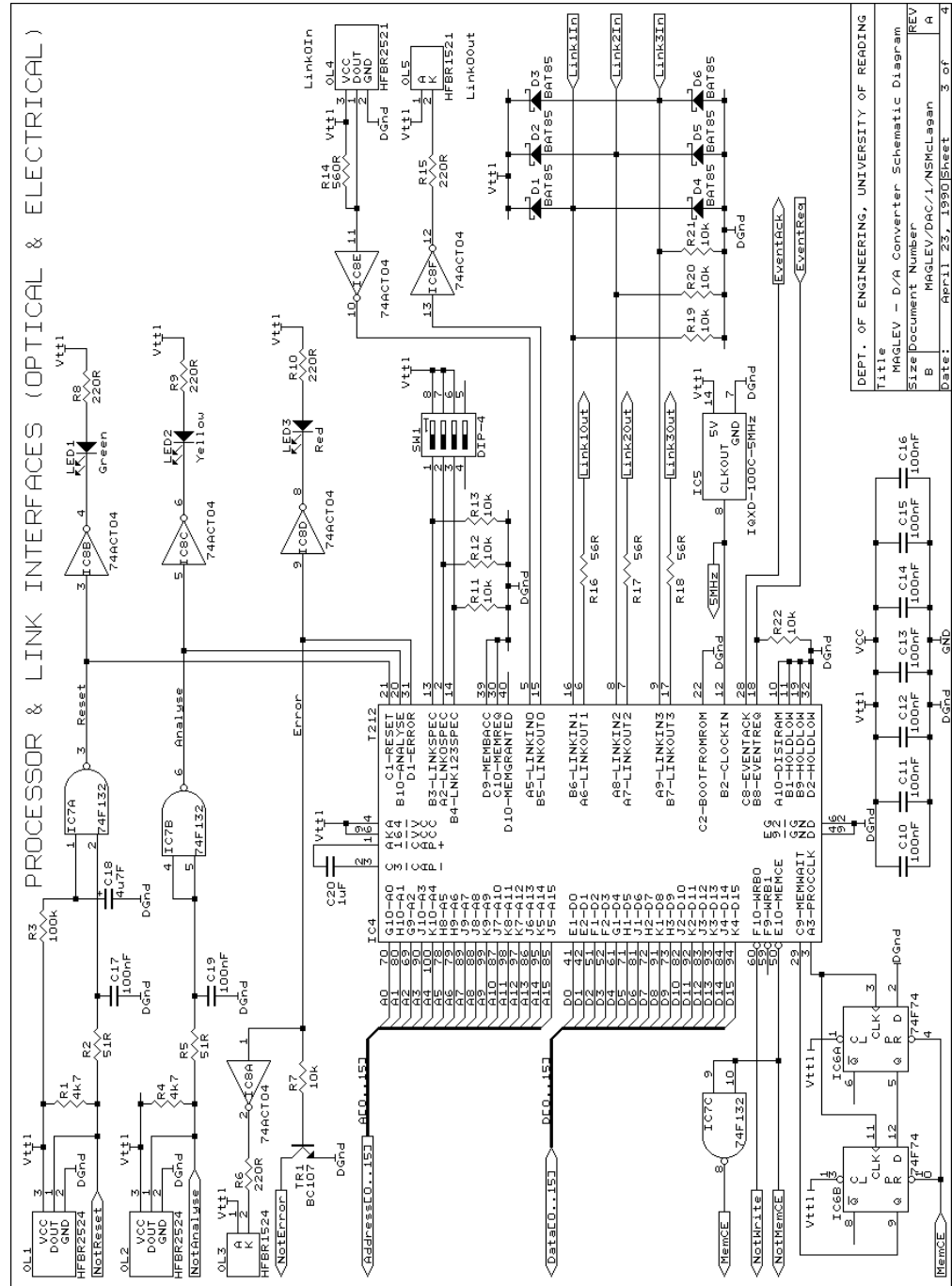
DEPT. OF ENGINEERING, UNIVERSITY OF READING	
Title	MAGLEV - D/A Converter Schematic Diagram
Size	Document Number
A	MAGLEV/DAC/1/NSMcLagan
Date:	April 20, 1990
Sheet	1 of 4

D.5.1 DAC card power supplies

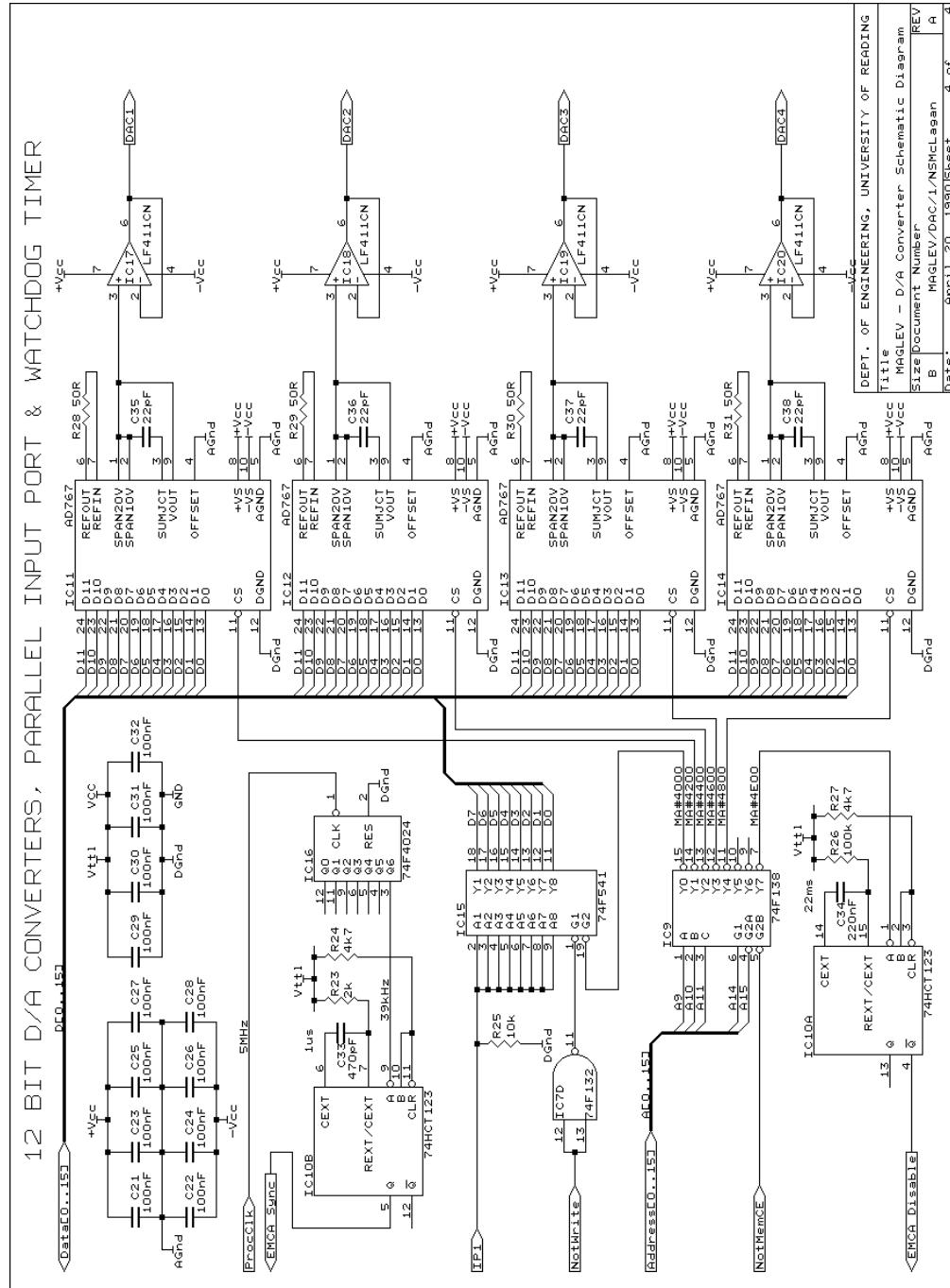




D.5.2 DAC processor & link interfaces (optical & electrical)



D.5.3 DAC converters & watchdog timer



## D.5.4 DAC card component parts list

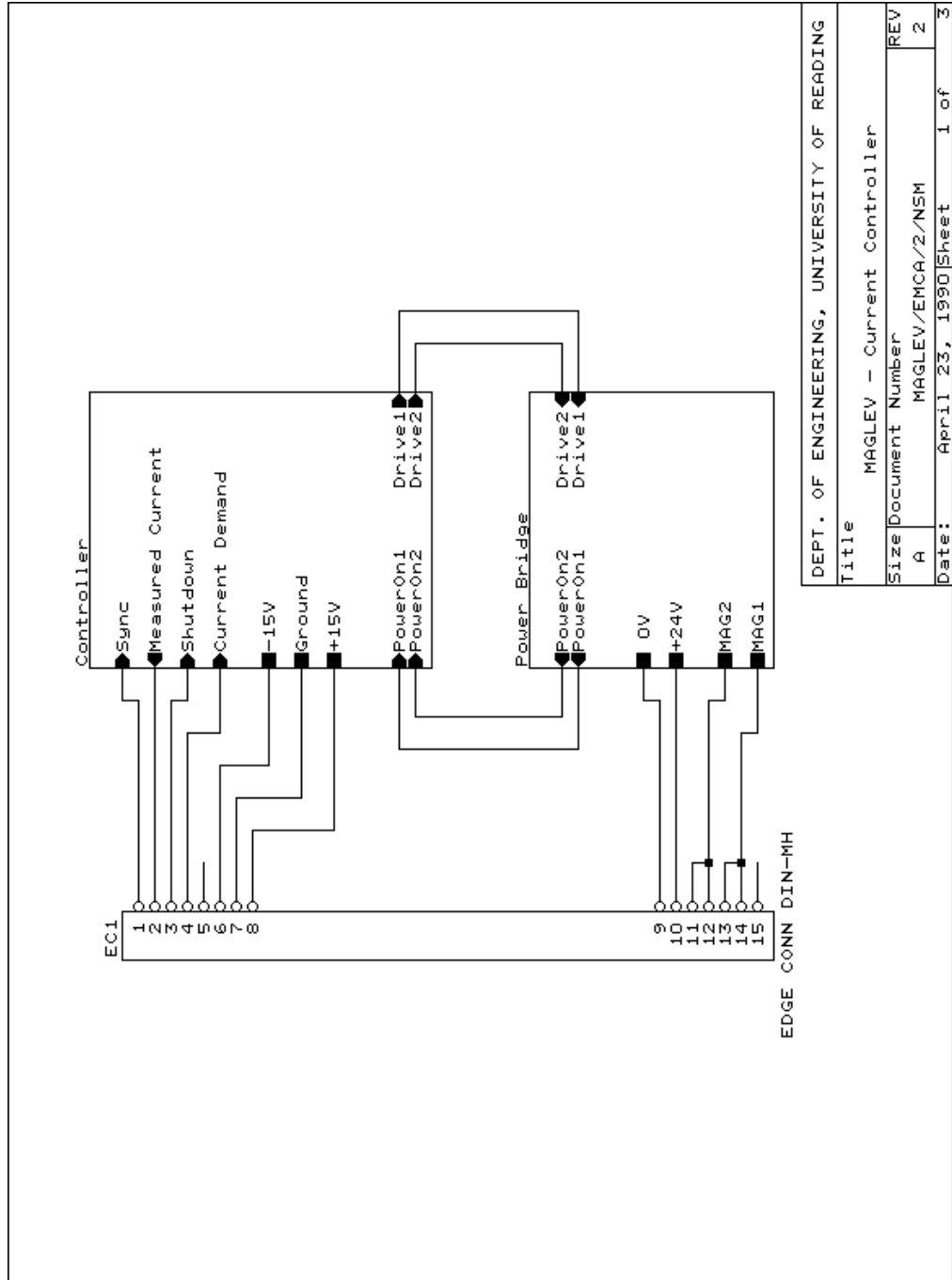
MAGLEV - D/A Converter Schematic Diagram  
MAGLEV/DAC/1/N.S.McLagan

Revised: January 24, 1990  
Revision: A

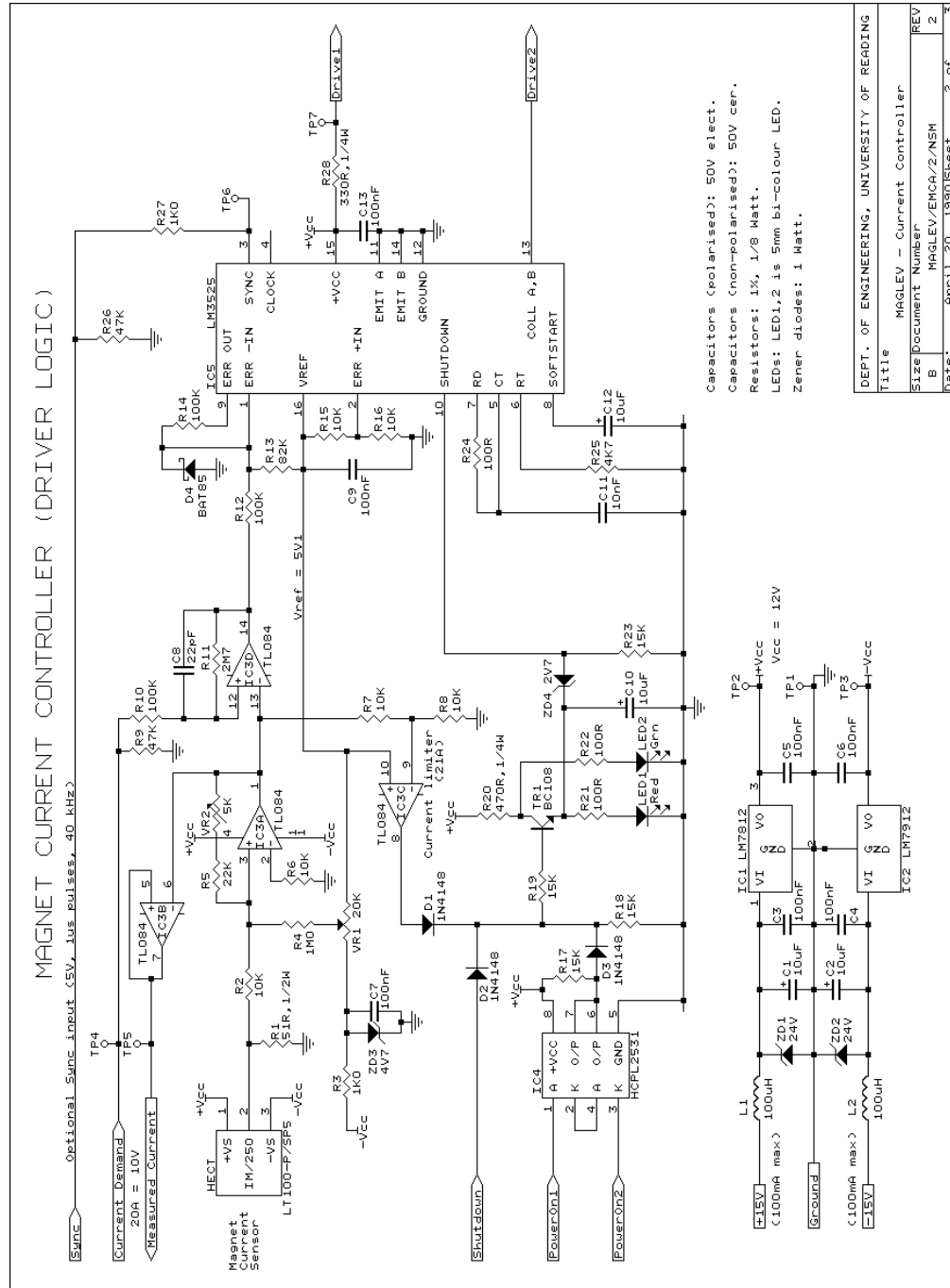
Bill Of Materials January 25, 1990 16:09:15 Page 1

<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
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1	C18	4u7F
27	C2, C3, C6, C7, C8, C9, C10, C11, C12, C13, C14, C15, C16, C17, C19, C21, C22, C23, C24, C25, C26, C27, C28, C29, C30, C31, C32	100nF
1	C20	1uF
1	C33	470pF
1	C34	220nF
4	C35, C36, C37, C38	22pF
2	C4, C5	10uF
6	D6, D2, D3, D4, D7, D8	BAT85
1	EC1	DIN41216-32a, b
1	IC1	LM2940CT5
1	IC10	74HCT123
4	IC11, IC12, IC13, IC14	AD767
1	IC15	74F541
1	IC16	74ACT4024
4	IC17, IC18, IC19, IC20	LF411CN
1	IC2	LM7812
1	IC3	LM7912
1	IC4	T212
1	IC5	IQXD-100C-5MHz crystal
1	IC6	74F74
1	IC7	74F132
1	IC8	74ACT04
1	IC9	74F138
3	L2, L1, L3	100uH
1	LED1	Green
1	LED2	Yellow
1	LED3	Red
2	OL1, OL2	HFBR2524
1	OL3	HFBR1524
1	OL4	HFBR2521
1	OL5	HFBR1521
1	PSW1	Push switch
4	R1, R4, R24, R27	4k7
2	R15, R6	100R
3	R16, R17, R18	56R
2	R2, R5	51R
1	R23	2k
4	R28, R29, R30, R31	50R
2	R3, R26	100k
1	R14	560R
9	R7, R11, R12, R13, R19, R20, R21, R22, R25	10k
3	R8, R9, R10	220R
1	SW1	DIP-4 way SPST
1	TAG	Earth tag
5	TP2, TP1, TP3, TP4, TP5	Test pins
1	TR1	BC107
3	ZD1, ZD2, ZD3	24V

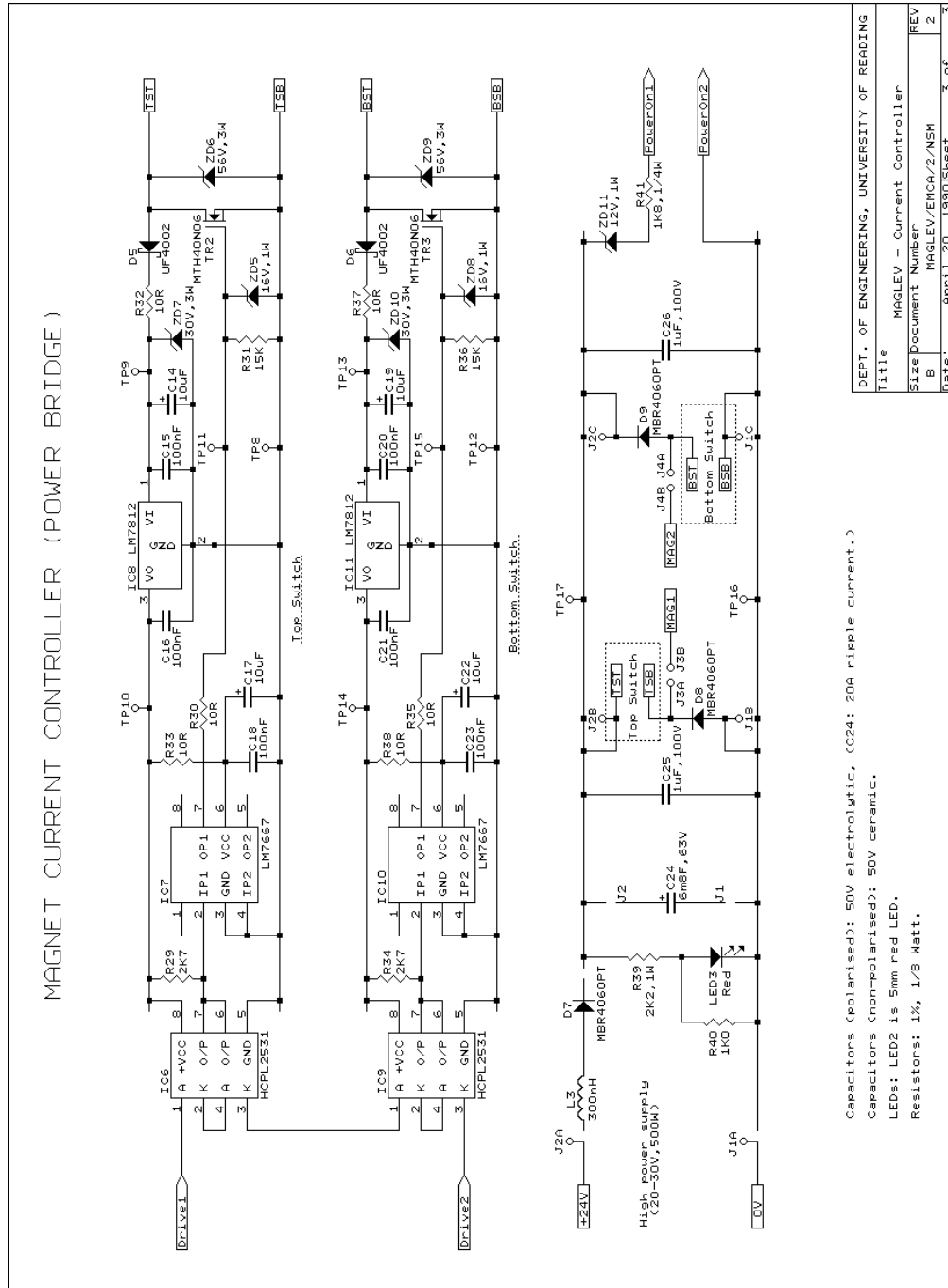
D.6 Electromagnet current controller module



D.6.1 EMCA controller logic



D.6.2 EMCA power switching bridge



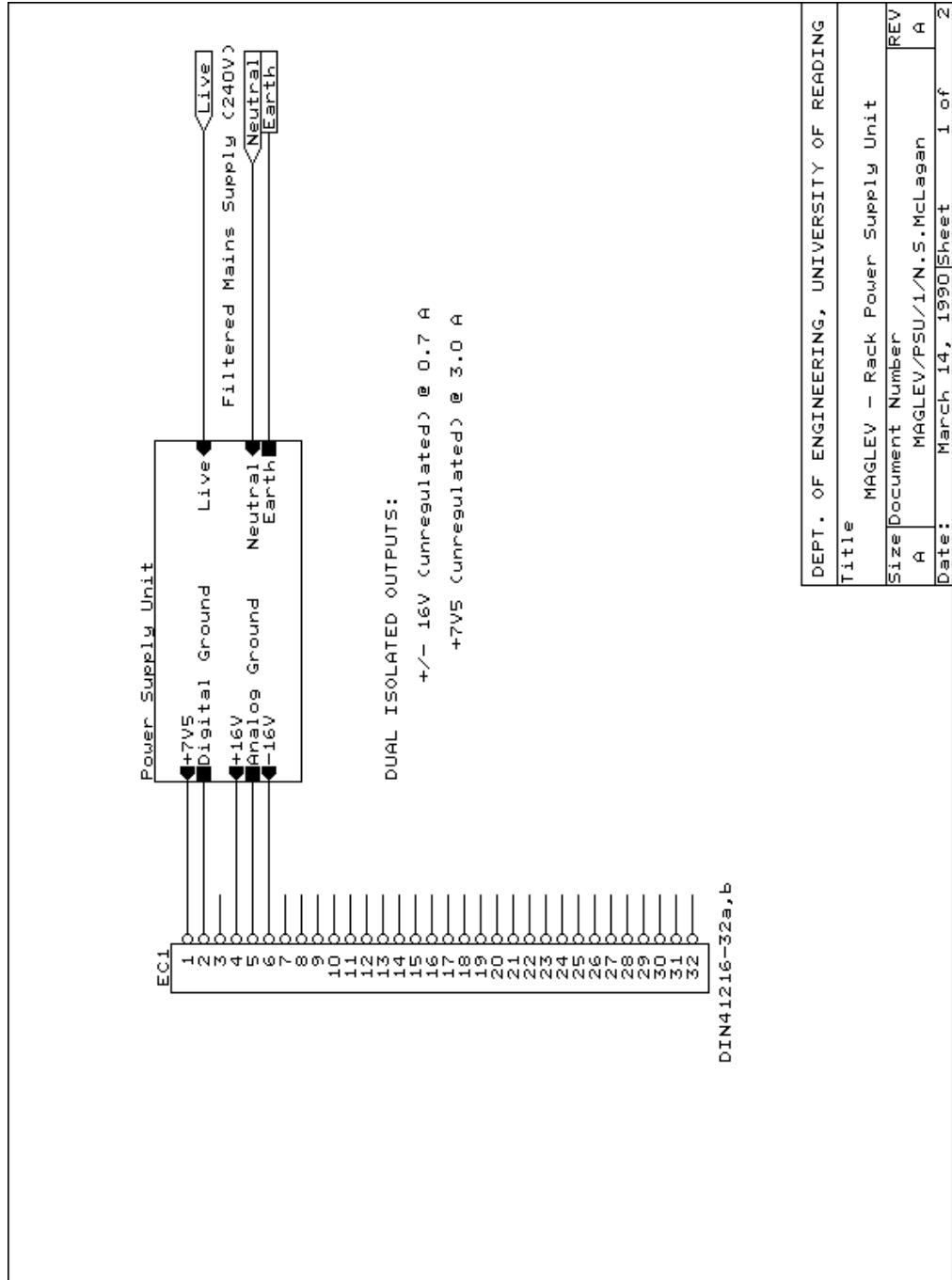
## D.6.3 EMCA card component parts list

ELECTROMAGNET CURRENT AMPLIFIER  
MAGLEV/EMCA/2/N.S.McLagan

Revised: November 8, 1989  
Revision: A

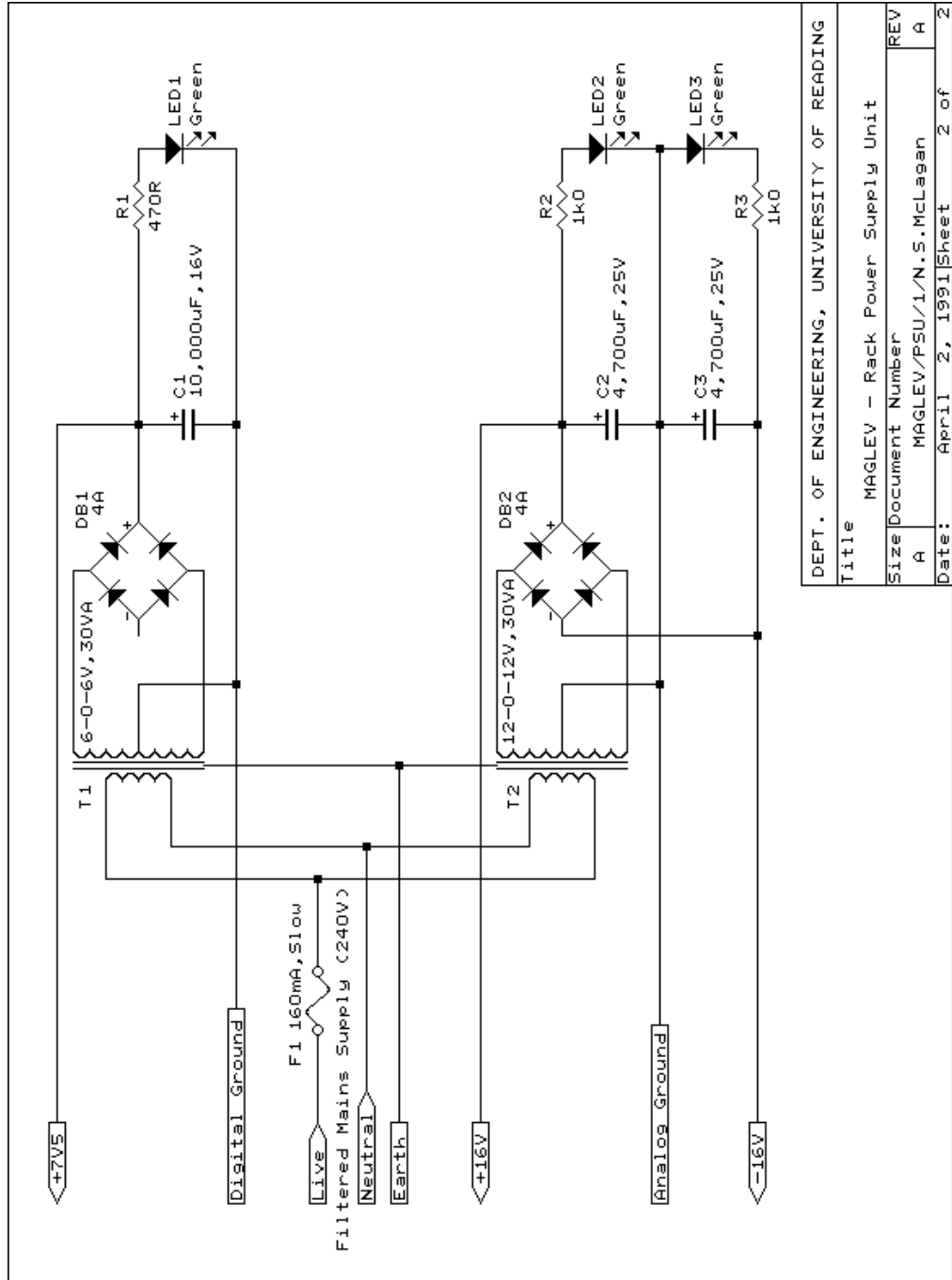
<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
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13	C15, C3, C4, C5, C6, C7, C9, C13, C16, C18, C20, C21, C23	100nF
1	C24	6m8F, 63V
2	C25, C26	1uF, 63V
1	C8	22pF
3	D2, D1, D3	1N4148
1	D4	BAT85
2	D5, D6	UF4002
3	D7, D8, D9	MBR4060PT
1	EC1	DIN41216 'MH'
1	HECT	LT100-P/SP5
1	IC2	LM7912
1	IC3	TL084
1	IC5	LM3525
3	IC6, IC4, IC9	HCPL2531
2	IC7, IC10	LM7667
3	IC8, IC1, IC11	LM7812
10	J1A, J1B, J1C, J2A, J2B, J2C, J3A, J3B, J4A, J4B	20A Jumpers
2	L1, L2	100uH
1	L3	300nH
1	LED2	Green LED
2	LED3, LED1	Red LED
1	R1	51R, 1/2W
3	R10, R12, R14	100K
1	R11	2M7
1	R13	82K
6	R2, R6, R7, R8, R15, R16	10K
1	R20	470R, 1/4W
3	R21, R22, R24	100R
1	R25	4K7
1	R28	330R, 1/4W
2	R29, R34	2K7
6	R31, R17, R18, R19, R23, R36	15K
6	R33, R30, R32, R35, R37, R38	10R
1	R39	2K2, 1W
1	R4	1M0
3	R40, R3, R27	1K0
1	R41	1K8, 1/4W
1	R5	22K
2	R9, R26	47K
17	TP8, TP1, TP2, TP3, TP4, TP5, TP6, TP7, TP9, TP10, TP11, TP12, TP13, TP14, TP15, TP16, TP17	Test pins
1	TR1	BC108
2	TR2, TR3	MTH40N06
1	VR1	20K
1	VR2	5K
2	ZD1, ZD2	24V
1	ZD11	12V, 1W
1	ZD3	4V7
1	ZD4	2V7
2	ZD6, ZD9	56V, 3W
2	ZD7, ZD10	30V, 3W
2	ZD8, ZD5	16V, 1W

D.7 Chassis power supply module





D.7.1 PSU supply conditioning



## D.7.2 PSU card component parts list

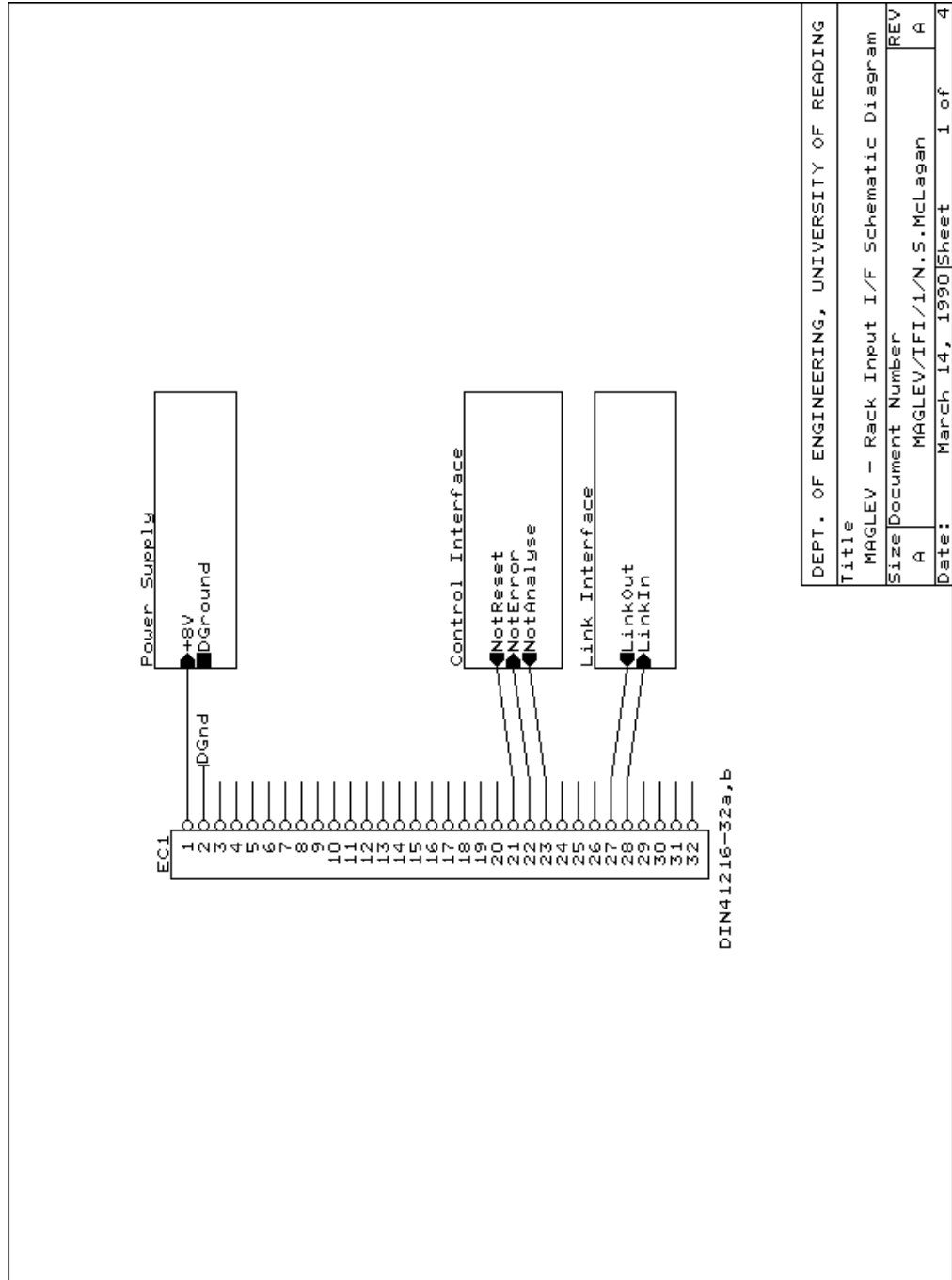
MAGLEV - Rack Power Supply Unit  
MAGLEV/PSU/1/N.S.McLagan

Revised: March 14, 1990  
Revision: A

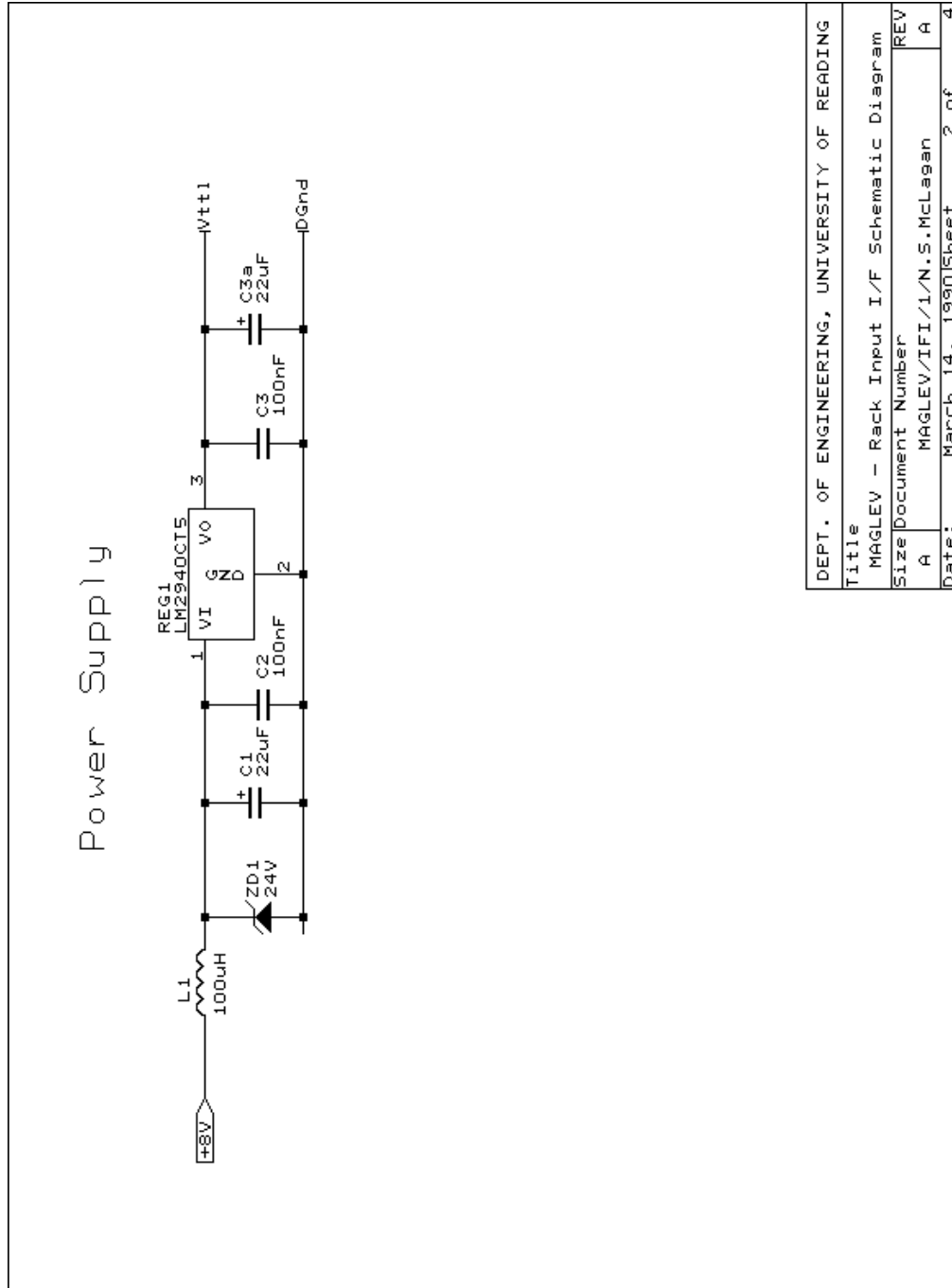
Bill Of Materials                      April 2, 1991                      17:45:25                      Page 1

<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
1	C1	10,000uF,16V
2	C2,C3	4,700uF,25V
2	DB1,DB2	4A
1	EC1	DIN41216-32a,b
1	F1	160mA, Slow
3	LED1,LED2,LED3	Green
1	R1	470R
2	R2,R3	1k0
1	T1	6-0-6V, 30VA
1	T2	12-0-12V, 30VA

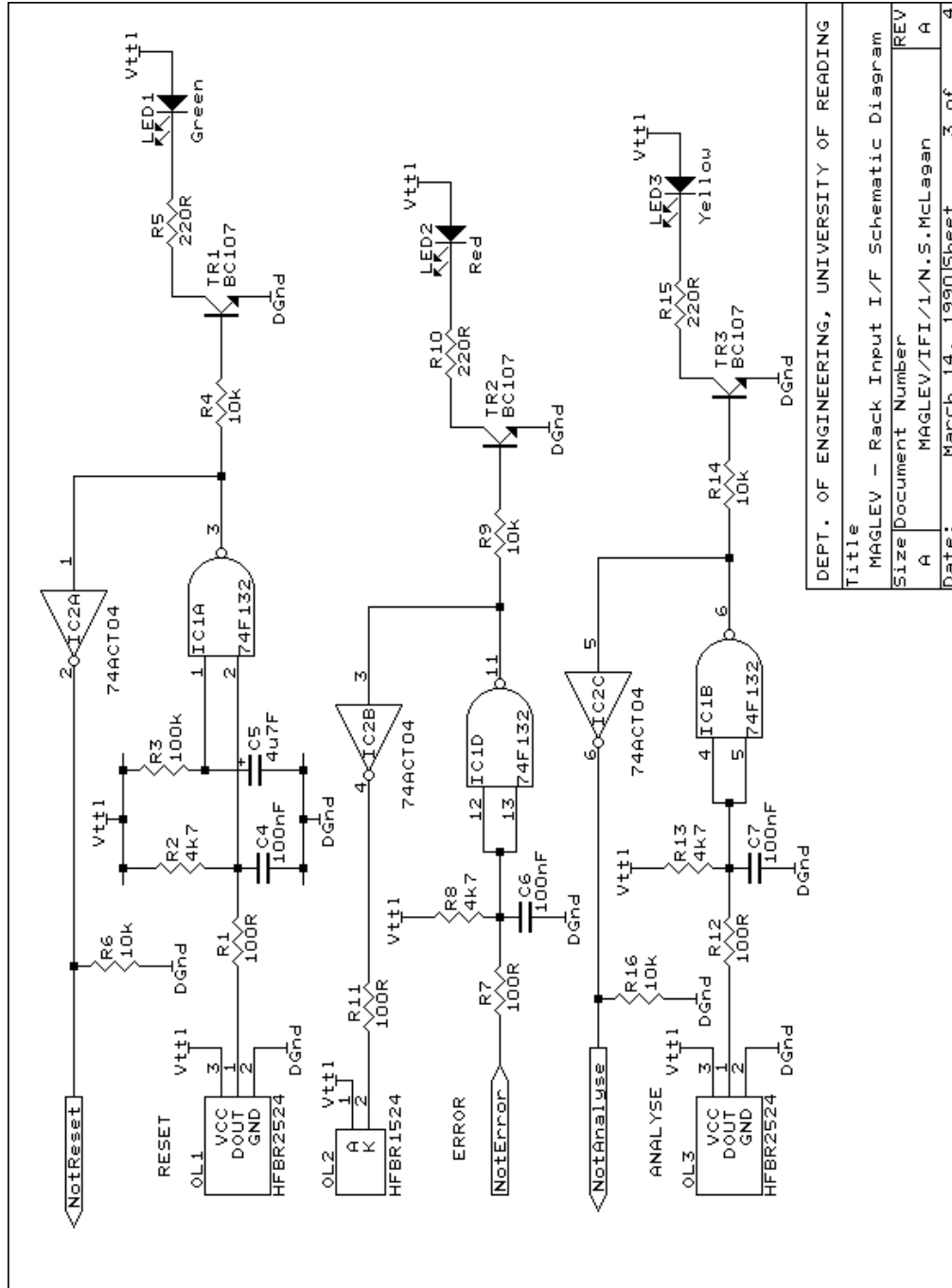
D.8 Chassis optical input interface card



D.8.1 Chassis input interface power supply

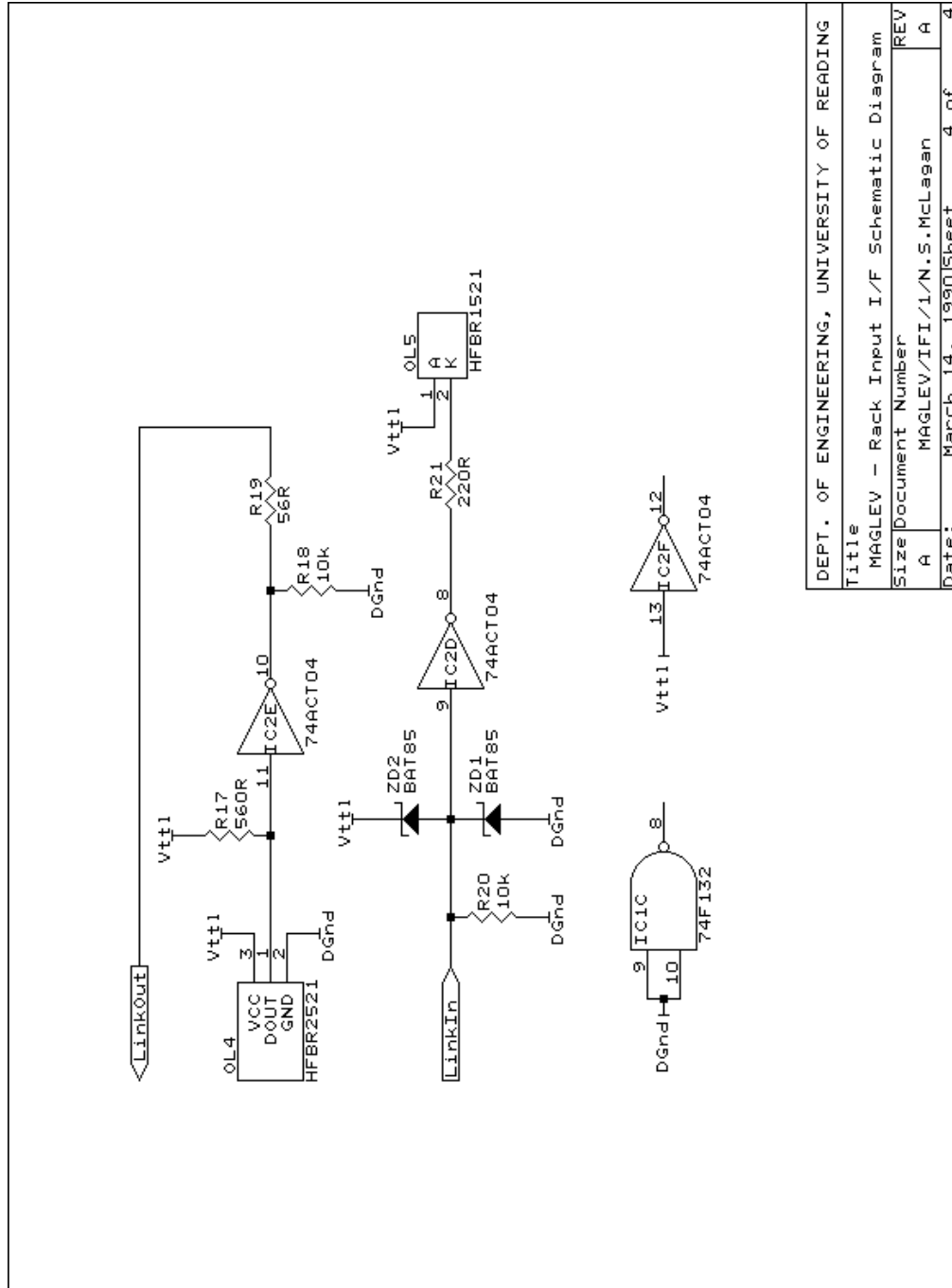


D.8.2 Chassis input interface control signals



DEPT. OF ENGINEERING, UNIVERSITY OF READING	
Title	MAGLEV - Rack Input I/F Schematic Diagram
Size	Document Number
REV	MAGLEV/IFI/1/N.S.McLagan
Date:	March 14, 1990
Sheet	3 of 4

D.8.3 Chassis input interface data signals



DEPT. OF ENGINEERING, UNIVERSITY OF READING	
Title	MAGLEV - Rack Input I/F Schematic Diagram
Size	Document Number
REV	MAGLEV/IFI/1/N.S.McLagan
Date:	March 14, 1990
Sheet	4 of 4

## D.8.4 Chassis input interface card component parts list

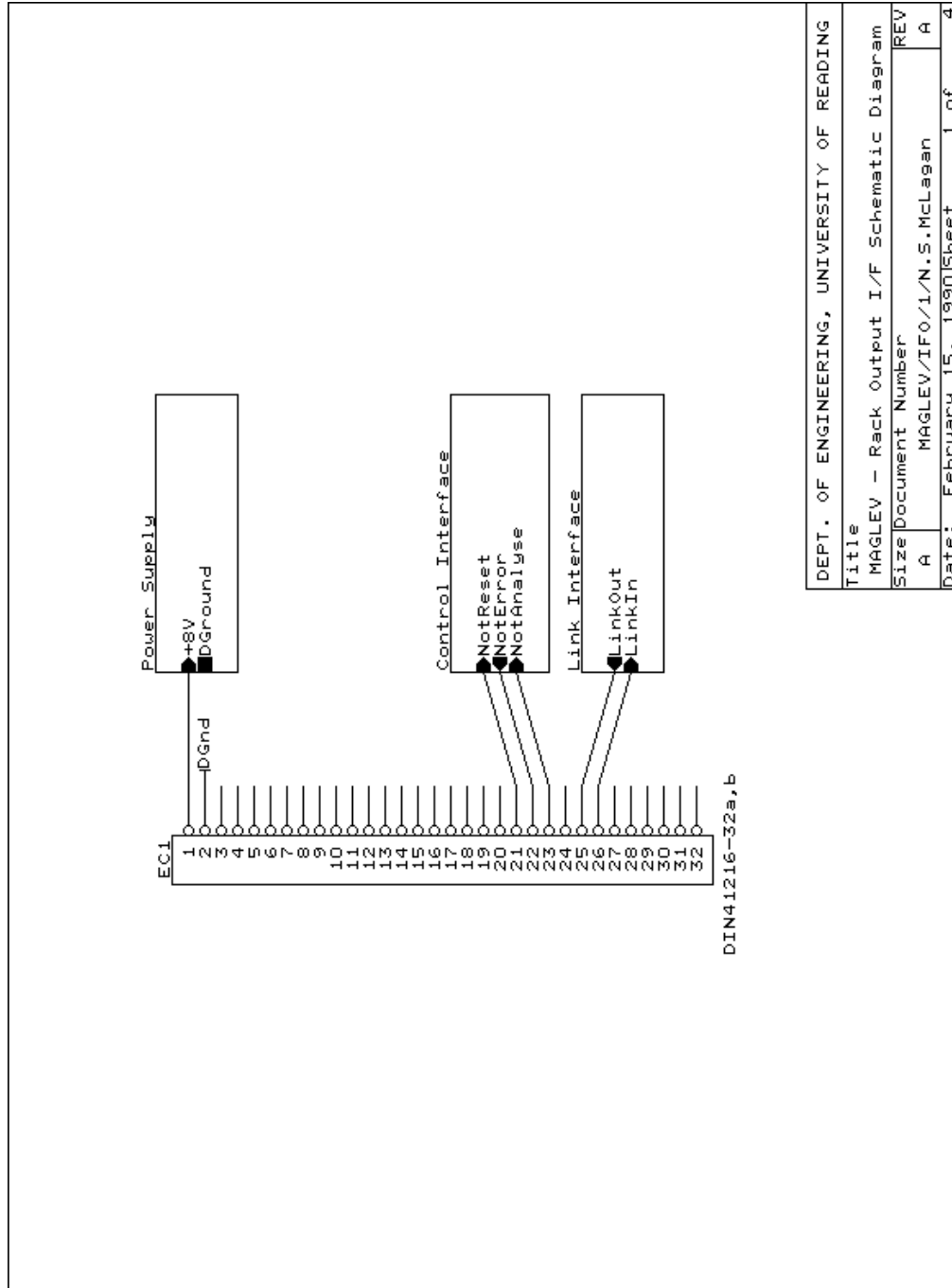
MAGLEV - Rack Input I/F Schematic Diagram  
 MAGLEV/IFI/1/N.S.McLagan

Revised: March 14, 1990  
 Revision: A

Bill Of Materials April 2, 1991 17:27:12 Page 1

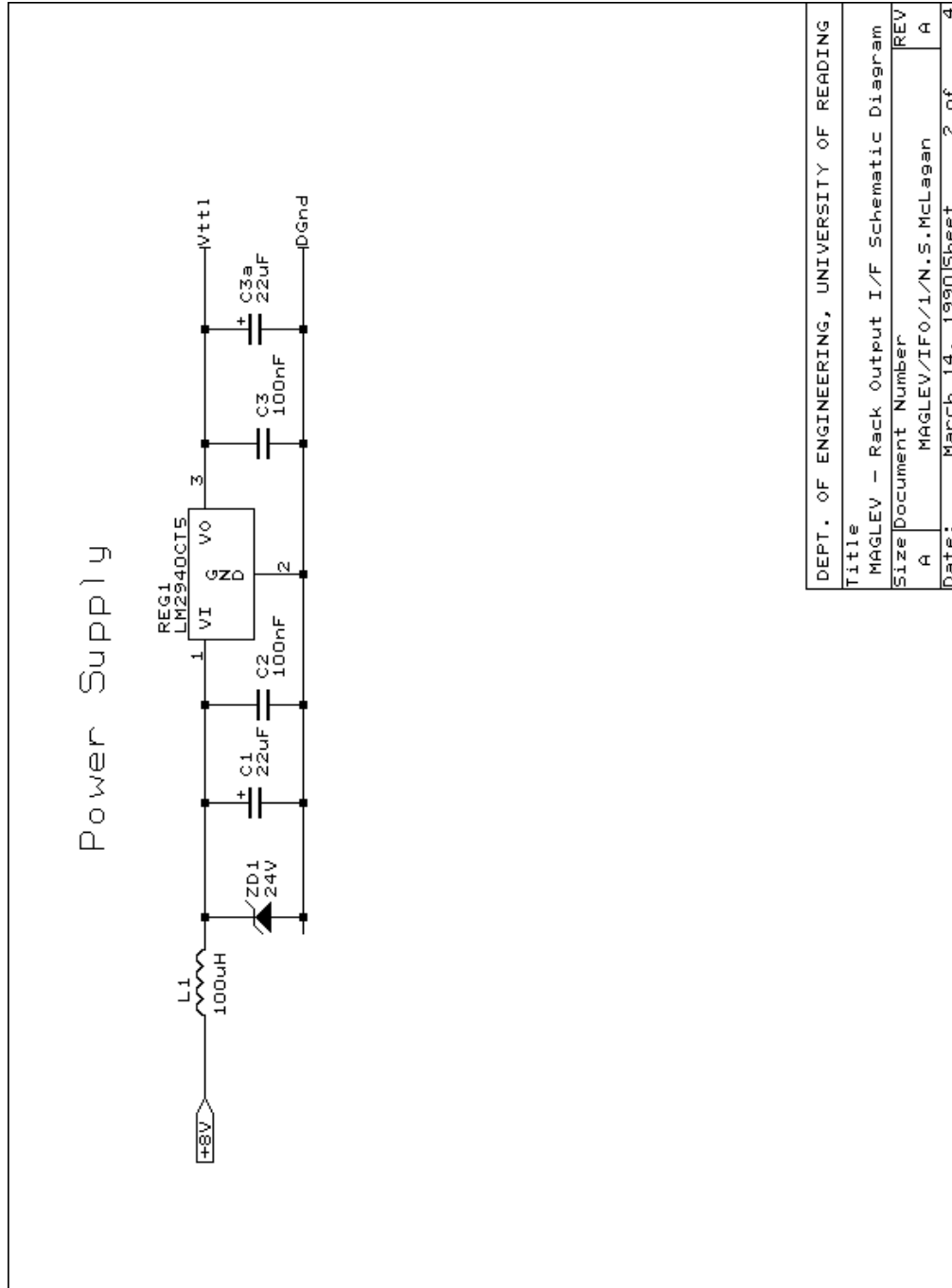
<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
2	C1, C3a	22uF
5	C2, C3, C4, C6, C7	100nF
1	C5	4u7F
1	EC1	DIN41216-32a, b
1	IC1	74F132
1	IC2	74ACT04
1	L1	100uH
1	LED1	Green
1	LED2	Red
1	LED3	Yellow
2	OL1, OL3	HFBR2524
1	OL2	HFBR1524
1	OL4	HFBR2521
1	OL5	HFBR1521
3	R2, R8, R13	4k7
1	R3	100k
7	R4, R6, R9, R14, R16, R18, R20	10k
4	R1, R7, R11, R12	100R
4	R5, R10, R15, R21	220R
1	R17	560R
1	R19	56R
1	REG1	LM2940CT5
3	TR1, TR2, TR3	BC107
1	ZD1	24V
2	ZD1, ZD2	BAT85

D.9 Chassis optical output interface card

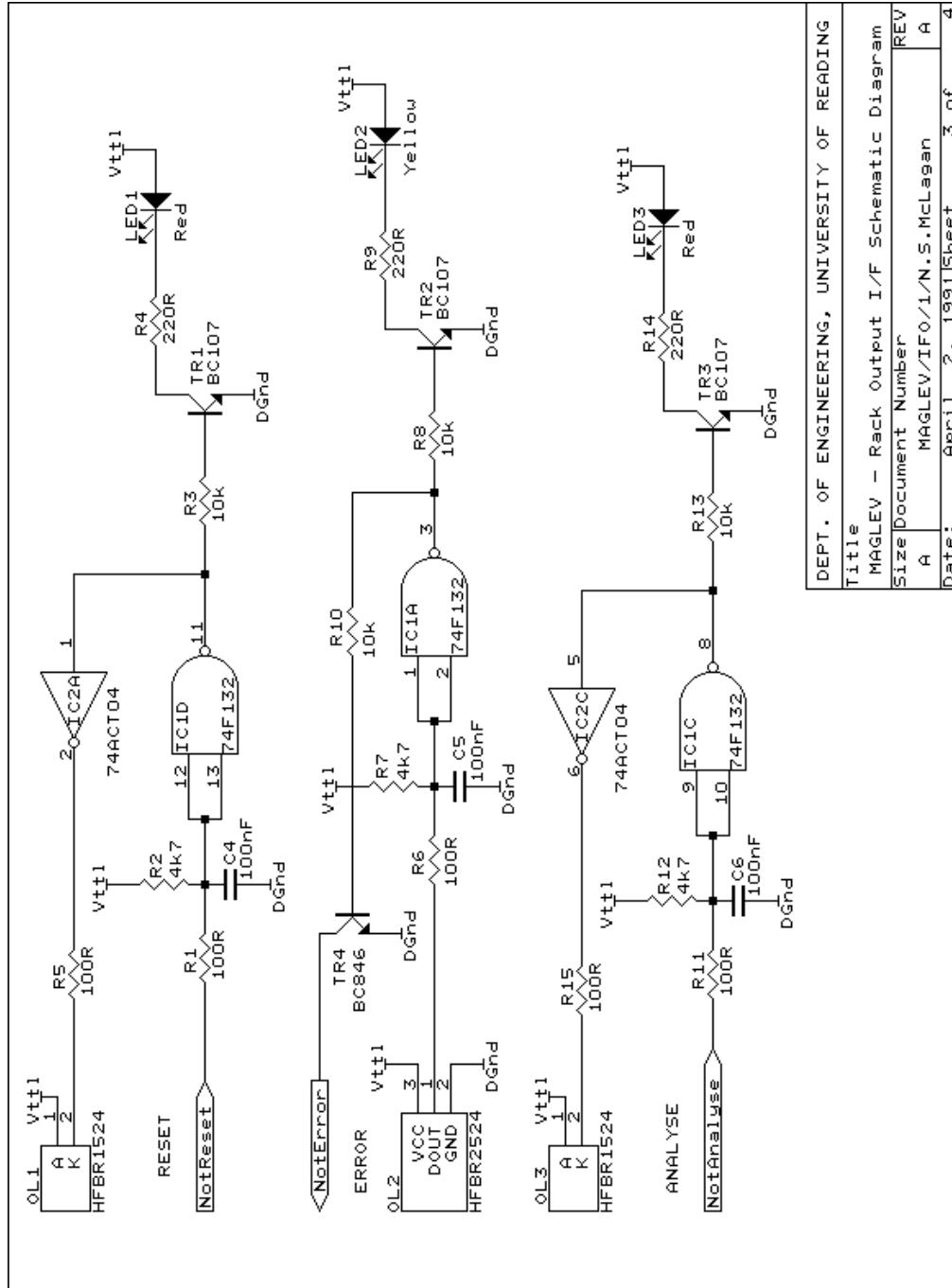




D.9.1 Chassis output interface power supply

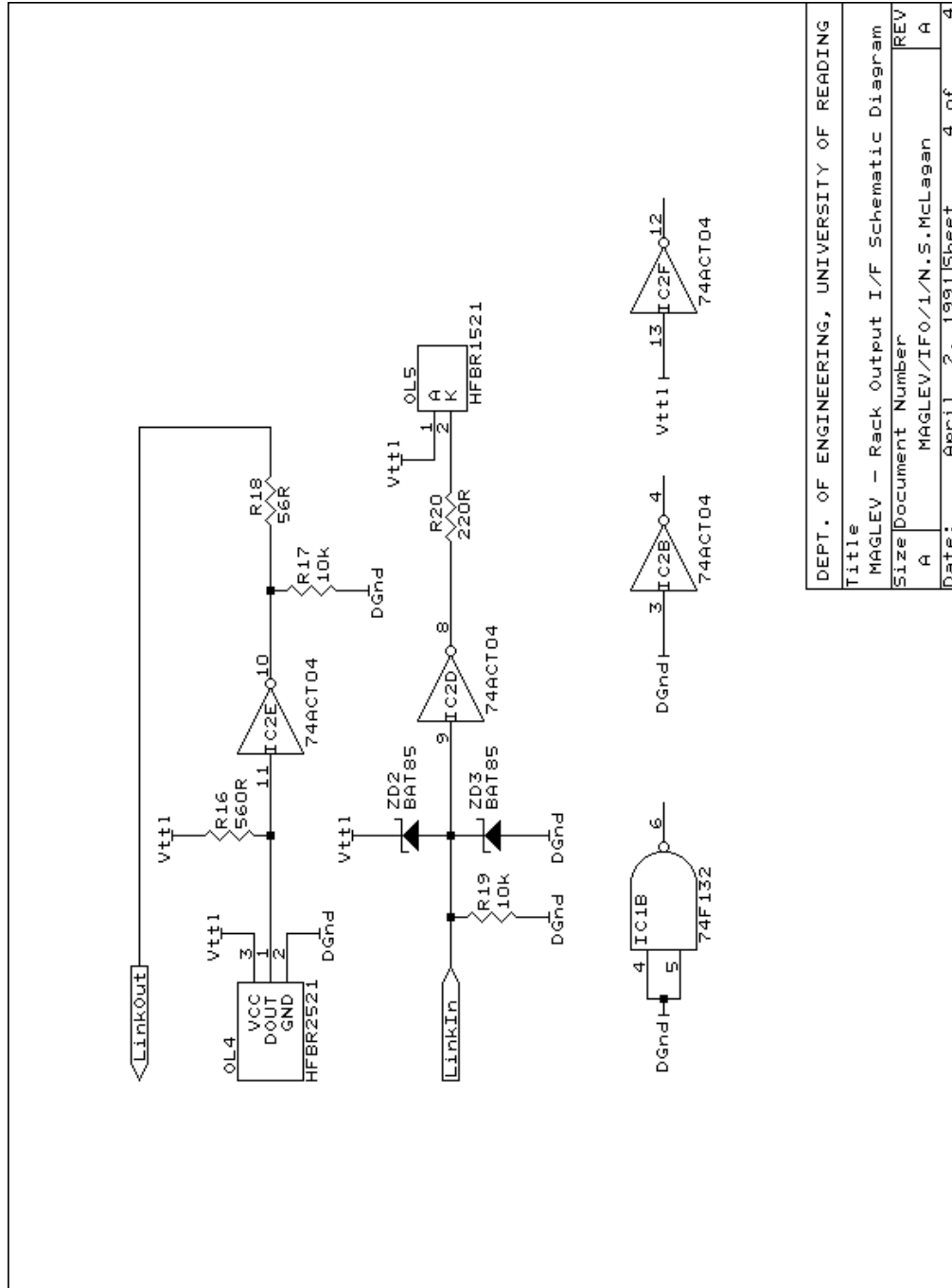


D.9.2 Chassis output interface control signals



DEPT. OF ENGINEERING, UNIVERSITY OF READING	
Title	MAGLEV - Rack Output I/F Schematic Diagram
Size	Document Number
REV	A
REV	MAGLEV/IF0/1/N.S.McLagan
Date:	April 2, 1991
Sheet	3 of 4

D.9.3 Chassis output interface data signals



DEPT. OF ENGINEERING, UNIVERSITY OF READING	
Title	MAGLEV - Rack Output I/F Schematic Diagram
Size	Document Number
REV	MAGLEV/IF0/1/N.S.McLagan
Date:	April 2, 1991
Sheet	4 of 4

## D.9.4 Chassis output interface card component parts list

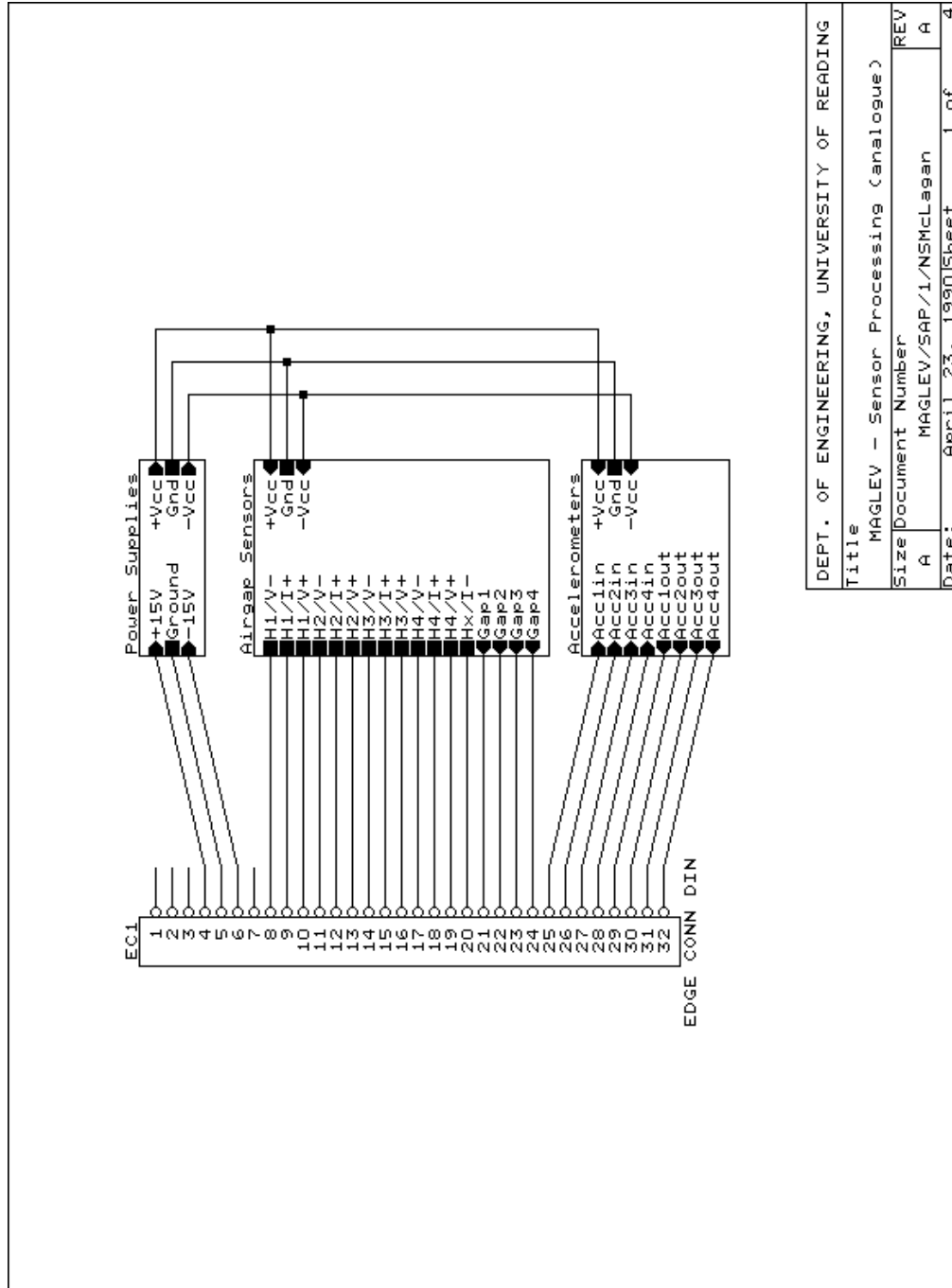
MAGLEV - Rack Output I/F Schematic Diagram  
MAGLEV/IFO/1/N.S.McLagan

Revised: February 15, 1990  
Revision: A

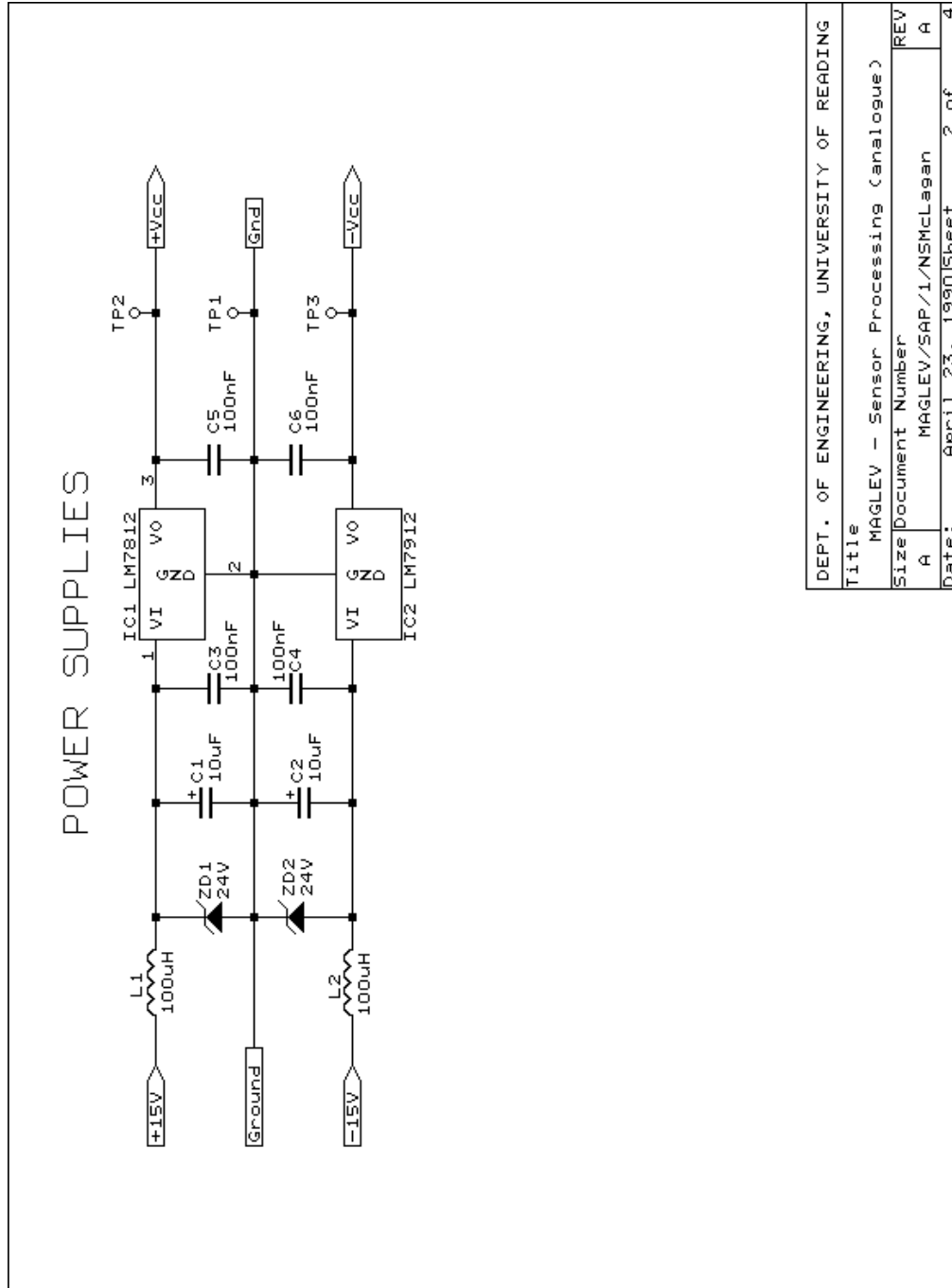
Bill Of Materials                      April 2, 1991                      17:45:09                      Page 1

<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
2	C1, C3a	22uF
5	C2, C3, C4, C5, C6	100nF
1	EC1	DIN41216-32a, b
1	IC1	74F132
1	IC2	74ACT04
1	L1	100uH
2	LED1, LED3	Red
1	LED2	Yellow
2	OL1, OL3	HFBR1524
1	OL2	HFBR2524
1	OL4	HFBR2521
1	OL5	HFBR1521
3	R2, R7, R12	4k7
6	R3, R8, R10, R13, R17, R19	10k
5	R1, R5, R6, R11, R15	100R
4	R4, R9, R14, R20	220R
1	R16	560R
1	R18	56R
1	REG1	LM2940CT5
3	TR1, TR2, TR3	BC107
1	TR4	BC846
1	ZD1	24V
2	ZD2, ZD3	BAT85

D.10 Sensor analogue preprocessor (4 channel) card

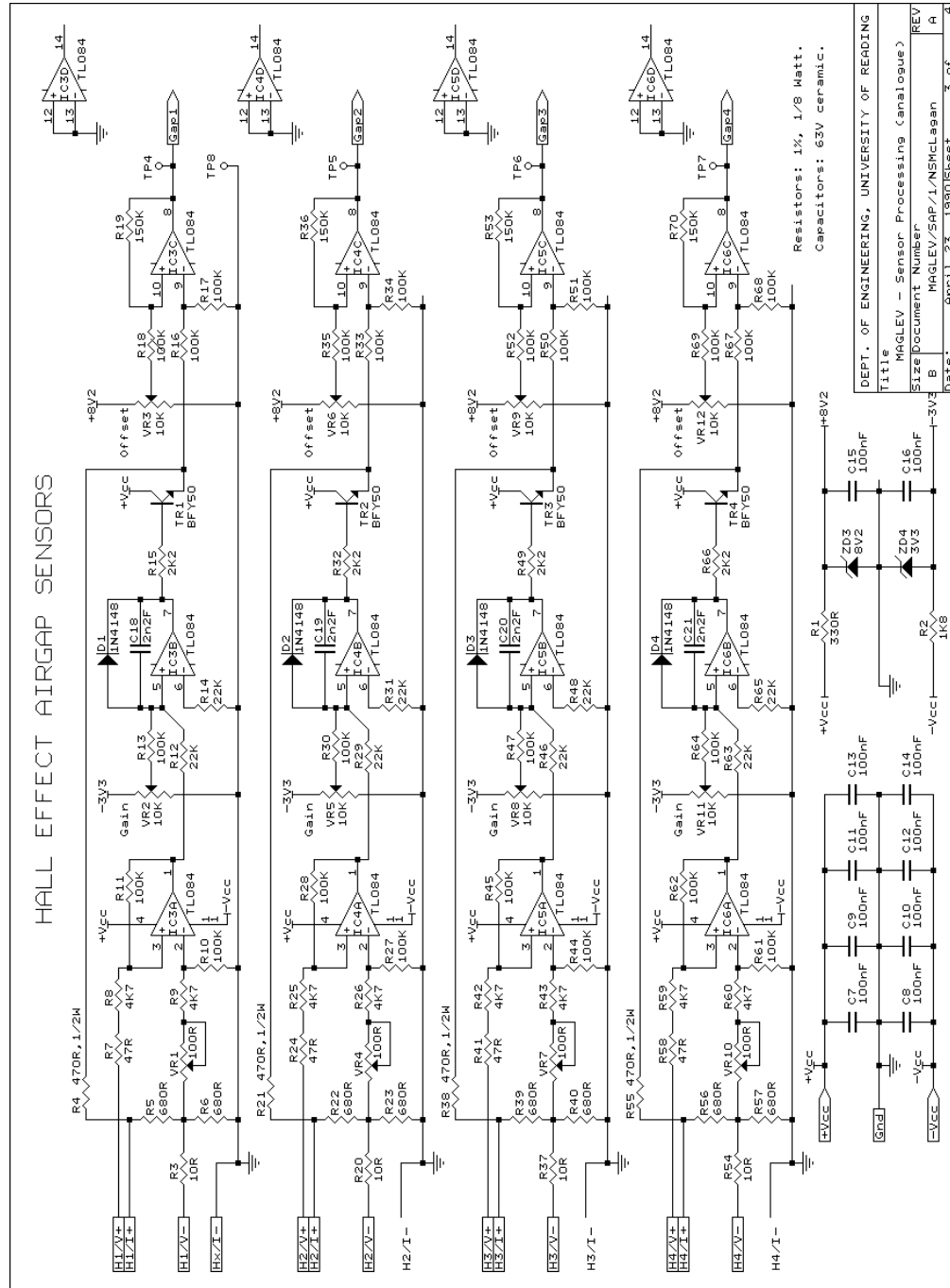


D.10.1 SAP card power supplies



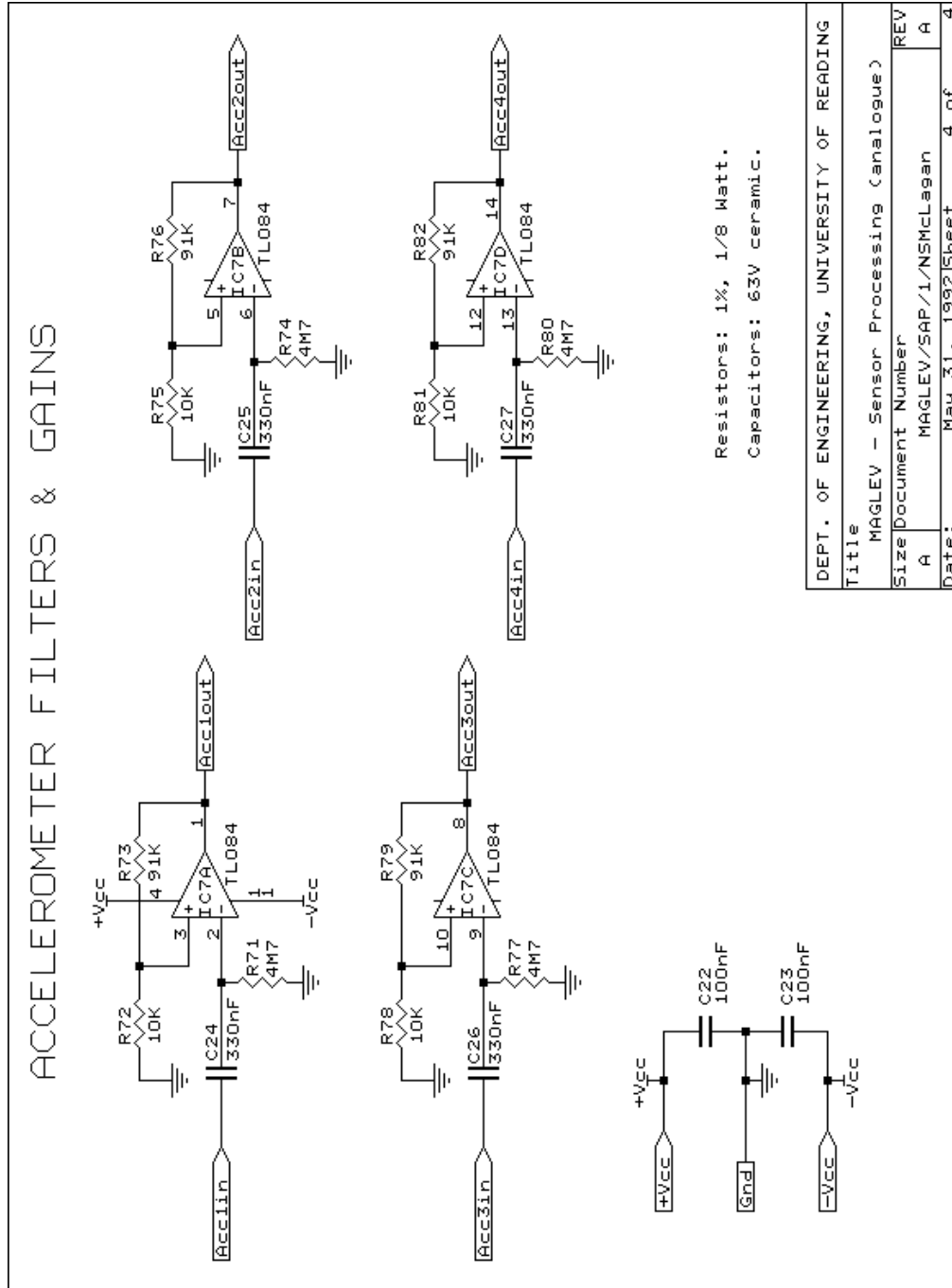
D.10.2 SAP Hall-effect air gap sensor controllers

Note: This circuitry is not implemented because commercial air gap sensors have been used instead. It is included here in case it is used in future systems.



DEPT. OF ENGINEERING, UNIVERSITY OF READING			
Title	MagLEV - Sensor Processing (analogue)		
Size	Document Number		
	B	MagLEV/SAP/1/NSMcLagan	REV
Date:	April 23, 1990	Sheet	3 of 4

D.10.3 SAP sensor filters and amplifiers





## D.10.4 SAP card component parts list

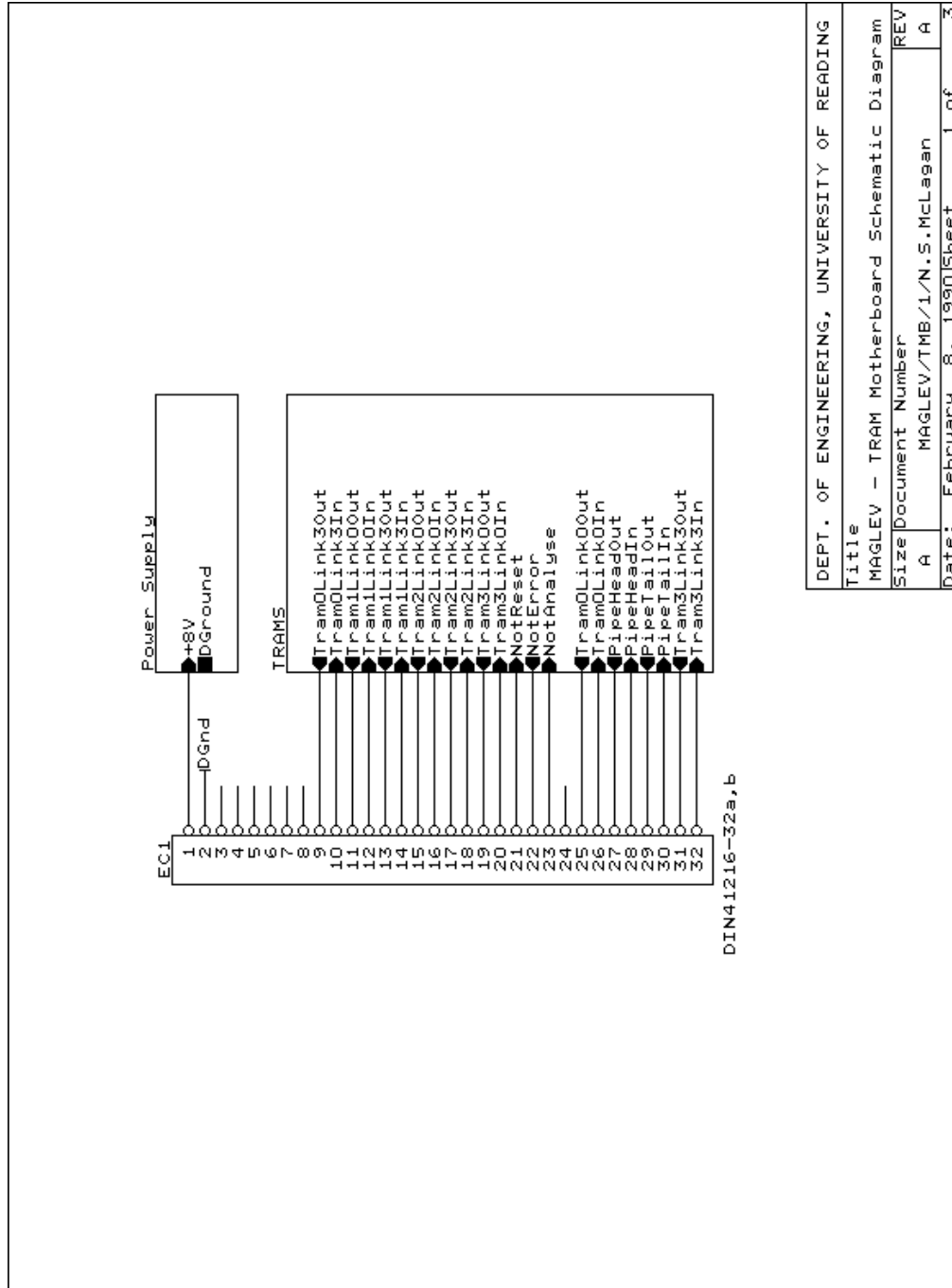
MAGLEV - Sensor Processing (analogue)  
MAGLEV/SAP/1/N.S.McLagan

Revised: November 2, 1989  
Revision: A

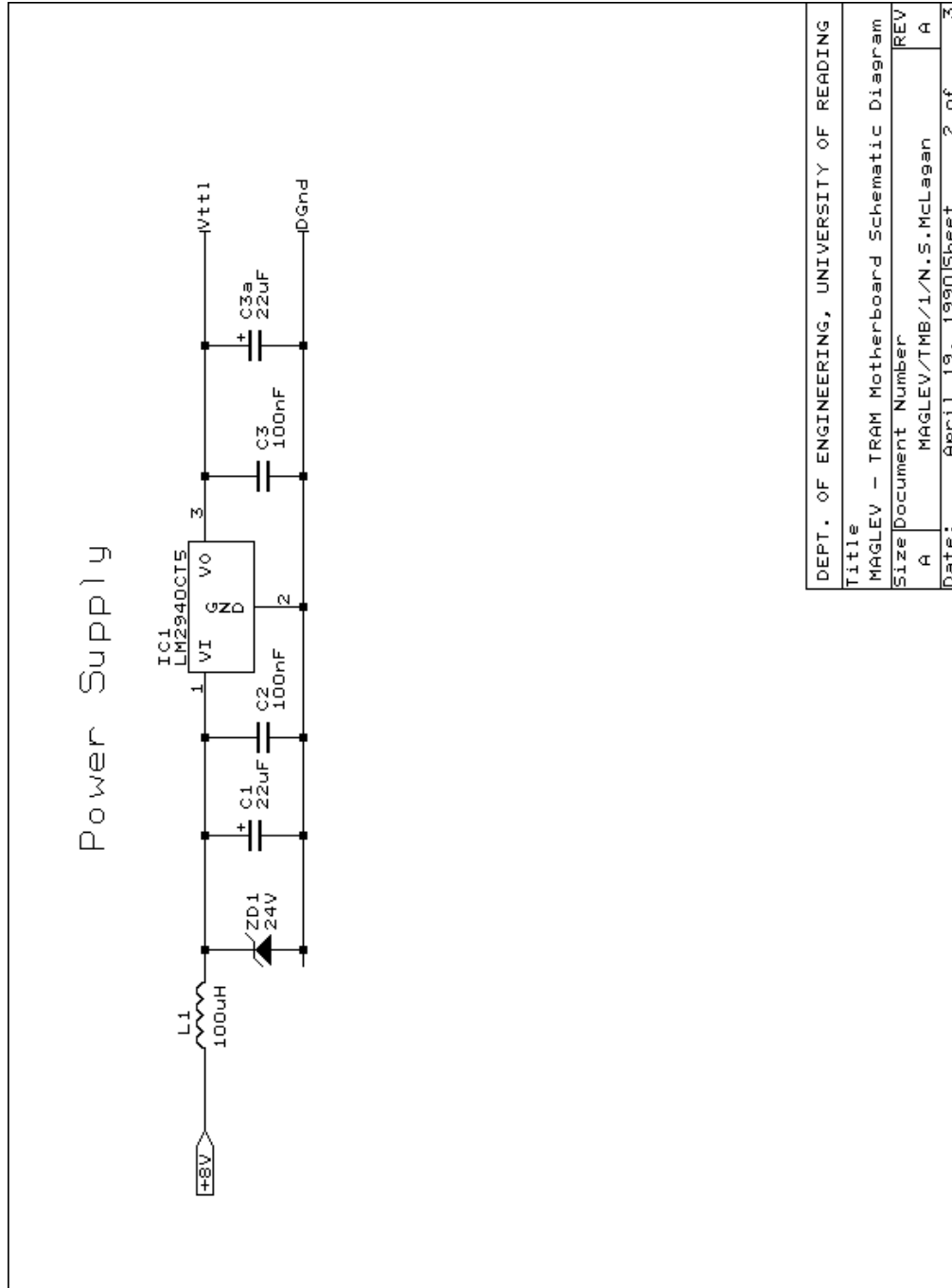
Bill Of Materials November 3, 1989 18:08:46 Page 1

<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
2	C1, C2	10uF
16	C15, C3, C4, C5, C6, C7, C8, C9, C10, C11, C12, C13, C14, C16, C22, C23	100nF
4	C18, C19, C20, C21	2n2F
4	C24, C25, C26, C27	330nF
4	D1, D2, D3, D4	1N4148
1	EC1	DIN41216-32a, c
1	IC1	LM7812
1	IC2	LM7912
5	IC3, IC4, IC5, IC6, IC7	TL084
2	L1, L2	100uH
1	R1	330R
24	R10, R11, R13, R16, R17, R18, R27, R28, R30, R33, R34, R35, R44, R45, R47, R50, R51, R52, R61, R62, R64, R67, R68, R69	100k
8	R12, R14, R29, R31, R46, R48, R63, R65	22k
4	R15, R32, R49, R66	2K2
4	R19, R36, R53, R70	150K
1	R2	1K8
4	R3, R20, R37, R54	10R
4	R4, R21, R38, R55	470R, 1/2W
8	R6, R5, R22, R23, R39, R40, R56, R57	680R
4	R7, R24, R41, R58	47R
4	R71, R74, R77, R80	4M7
4	R72, R75, R78, R81	10K
4	R73, R76, R79, R82	91K
8	R9, R8, R25, R26, R42, R43, R59, R60	4k7
8	TP4, TP1, TP2, TP3, TP5, TP6, TP7, TP8	Test pins
4	TR1, TR2, TR3, TR4	BFY50
4	VR1, VR4, VR7, VR10	100R
9	VR3, VR2, VR5, VR6, VR8, VR9, VR11, VR12	10k
2	ZD1, ZD2	24V
1	ZD3	8V2
1	ZD4	3V3

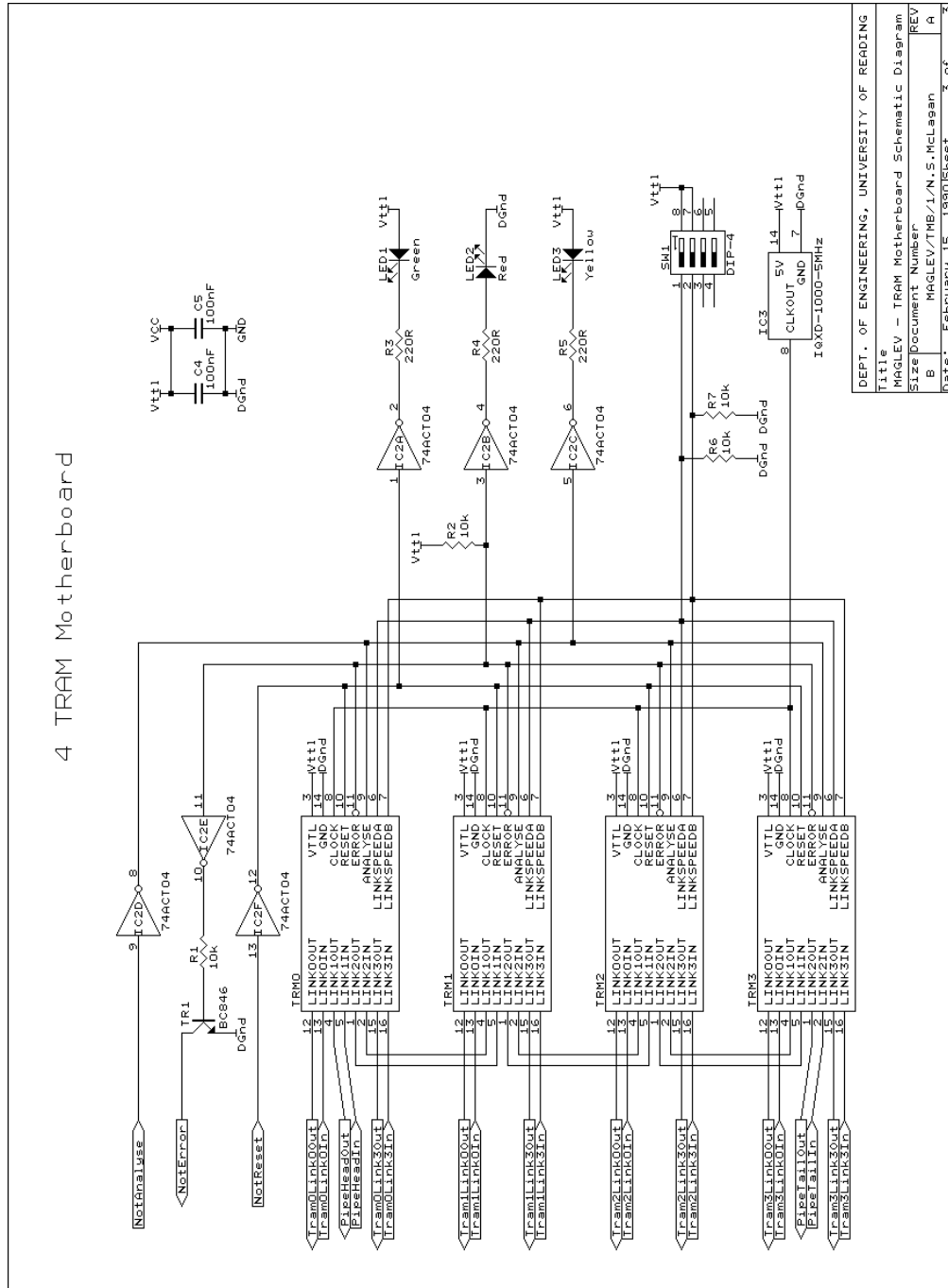
D.11 Transputer motherboard (4 tram) card



D.11.1 TMB card power supply



D.11.2 TMB TRAM connectivity



## D.11.3 TMB card component parts list

MAGLEV - TRAM Motherboard Schematic Diagram Revised: February 7, 1990  
 MAGLEV/TMB/1/N.S.McLagan Revision: A

Bill Of Materials February 8, 1990 14:08:10 Page 1

<u>Quantity</u>	<u>Reference</u>	<u>Part</u>
1	C1	22uF
4	C2,C3,C4,C5	100nF
1	EC1	DIN41216-32a,b
1	IC1	LM2940CT5
1	IC2	74ACT04
1	IC3	IQXD-1000-5MHz Oscillator
1	L1	100uH
1	LED1	Green LED
1	LED2	Red LED
1	LED3	Yellow LED
4	R1,R2,R6,R7	10k
3	R3,R4,R5	220R
1	SW1	DIP 4-way SPST
1	TR1	BC107
1	ZD1	24V

# Appendix E

---

## Control system software

This Appendix lists the suspension control programs for the vehicle and the single electromagnet systems. The three development support programs are also described. The various system software components, all of which are written in occam, are listed below:

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## E.1 Occam

The features which differentiate occam from conventional languages are now outlined to assist the reader in understanding the control system software. The description of occam is comprised of six parts namely: primitive processes; combining processes; data types; channels; timers and program configuration.

### E.1.1 Primitive processes

Occam programs are built up using processes, the simplest of which is an action (primitive process). The primitive processes include assignment, input, output, skip and stop. Table E.1 lists examples of these occam primitive processes.

**Table E.1** Occam primitive processes

PRIMITIVE PROCESS	ACTION
assignment	$x := y + 4$
input	keyboard ? character
output	screen ! character
no action, terminate	SKIP
no action, never terminate	STOP

### E.1.2 Combining processes

The action of one or more processes can be combined by a construction. A construction builds a process of the kinds listed in Table E.2. The SEQ, IF, PAR and ALT constructions can be replicated by the addition of an index specifier similar to that found in a conventional FOR loop statement.



**Table E.2** Occam combining processes

COMBINING PROCESS	CONSTRUCTION
sequential	SEQ
conditional	IF
selected	CASE
repeated	WHILE
parallel	PAR
alternative	ALT

### E.1.3 Data types

The primitive data types supported by occam are boolean values, bytes, integers (16, 32 and 64 bits) and ANSI/IEEE standard floating point numbers (32 and 64 bits). Non-primitive data types are limited to arrays, including multi-dimensional arrays. There is no structured data support similar to conventional record structures. The occam handling of arrays of differing sizes when used as process parameters is more flexible than with many conventional languages.

### E.1.4 Channels

Channels provide unbuffered, unidirectional, point-to-point communication of data between two concurrent processes. The format and type of data passed via a channel is specified by the channel protocol. The protocol declaration is similar to a record declaration in a conventional language. Variant protocols are supported in a similar way to conventional variant records. When a channel is declared, its type can be specified either by a data type or by a protocol. Channels are vitally important in concurrent systems because they facilitate synchronised communication between the concurrent program threads. Figure E.1 lists an example process which performs channel input and output using a replicated sequential construction.

```

PROTOCOL input.p IS INT, BYTE :

PROC data.expander( CHAN OF input.p  data.in,
                   CHAN OF BYTE  data.out )

    INT  length :
    BYTE  character :

    SEQ
        data.in ? length, character
        SEQ  index = 1 FOR length
            data.out ! character
    :

```

**Figure E.1** Occam channel example

### E.1.5 Timers

A timer provides a real-time clock facility. Timer is a primitive type, just like channels and data types. Only two operations are permitted on a timer: input and input-after. Input simply receives the present clock time, whilst input-after waits until the specified time before performing an input. Timers are very useful within control systems for generating signals at fixed or variable time intervals. Figure E.2 lists an example process which generates a periodic trigger signal. Modulo arithmetic must be used with timers since the hardware timer counters will restart periodically.

```

PROC Pulse.Generator(CHAN OF BOOL  trigger,
                    VAL INT  time.period )

TIMER  clock :
INT    time :

SEQ
    clock ? time
    WHILE TRUE
        SEQ
            trigger ! TRUE
            time := time PLUS time.period
            clock ? AFTER time
    :

```

**Figure E.2** Occam timer example

### E.1.6 Program configuration

Having coded an algorithm, configuration information dependent on the physical resources being used may be needed. There are three areas that may require configuration. First, where a multi-processor system is used, the top hierarchical level of the program consists of a PLACED PAR construction which allocates processes to processors. Secondly, the channels linking processes which execute on different processors must use PLACE CHAN to allocate the channels to physical transputer links. The PLACE configuration can also be used to allocate variables to specific memory locations, eg. for memory mapped hardware devices. Finally, the processes within a parallel process construction can be prioritised using PRI PAR. However, this is limited to only two levels of priority on the T2, T4 and T8 series of processors. Figure E.3 lists a program configuration example.

```
CHAN OF REAL32  signal :  
  
PLACED PAR  
  
  PROCESSOR 1 T8  
    PLACE signal AT link0out :  
      signal.generator( signal )  
  
  PROCESSOR 2 T2  
    PLACE signal AT linklin :  
      convert.signal( signal )
```

**Figure E.3** Occam configuration example

## E.2 Vehicle suspension controller

### E.2.1 Top-level Program configuration

```

#USE "system.tsr"
#USE "controll.tsr"
#USE "executiv.tsr"
#USE userio

PROC Head.Controller.Process( CHAN OF BOOL data.conversion.request,
    CHAN OF converter.signal.p ADConverter.in,

    CHAN OF signal.p signal.exchange.out,
    CHAN OF signal.p signal.exchange.in,

    CHAN OF controller.p export.controller.params,
    CHAN OF exception.p import.exception.reports,

    CHAN OF ANY PC.screen,
    CHAN OF INT PC.keyboard )

-- Head.Controller() is the separately compiled process for all the processes
-- running on the First main controller processor (T800-25 Mhz, 1MB preferably).

CHAN OF converter.signal.p dummy.DACs :
CHAN OF signal.p reference.signals :

[2]CHAN OF signal.p accs.to.mode.cont, gaps.to.mode.cont :
[2]CHAN OF signal.p refs.to.mode.cont, force.from.mode.cont :
[2]CHAN OF signal.p gaps.forces.to.mag.cont, current.from.magnet.cont :

[2]CHAN OF signal.p mode.cont.data, magnet.cont.data :
CHAN OF monitor.p data.to.buffer, data.to.monitor, temp :

CHAN OF controller.p controller.params :
CHAN OF BOOL exception.manager.reset, exception.shutdown :

[2]CHAN OF controller.p mode.cont.params, magnet.cont.params :
[6]CHAN OF exception.p exception.reports :
CHAN OF BOOL dummy.switch :
CHAN OF exception.p exception.notification :

CHAN OF signal.gen.p ref.signal.params, ref.signal.status :
CHAN OF data.buffer.p data.buffer.params :
CHAN OF BOOL buffer.data.request :

PROC Buffer( CHAN OF monitor.p in, out)
    REAL32 time :
    [4][num.magnets]REAL32 magnet.data :
    [7][num.magnets]REAL32 mode.data :
    WHILE TRUE
        SEQ
            in ? time; magnet.data; mode.data
            out ! time; magnet.data; mode.data
    :

PRI PAR
    PAR
        Signal.Data.Manager( head.processor, ADConverter.in, reference.signals,
            accs.to.mode.cont, gaps.to.mode.cont,
            refs.to.mode.cont, force.from.mode.cont,
            gaps.forces.to.mag.cont, current.from.magnet.cont,
            dummy.DACs,
            signal.exchange.out, signal.exchange.in,
            mode.cont.data, magnet.cont.data, data.to.buffer )

        Command.Message.Manager( head.processor, controller.params,
            magnet.cont.params, mode.cont.params,
            export.controller.params, exception.manager.reset )

        Reference.Signal.Generator( data.conversion.request, reference.signals,
            ref.signal.params, ref.signal.status,
            exception.shutdown, exception.reports[0] )

```

```

PAR index = 0 FOR 2
  Vehicle.Mode.Controller( index, refs.to.mode.cont[index],
                           accs.to.mode.cont[index], gaps.to.mode.cont[index],
                           force.from.mode.cont[index], mode.cont.data[index],
                           mode.cont.params[index], exception.reports[index+1] )

PAR index = 0 FOR 2
  Magnet.Force.Controller( index, gaps.forces.to.mag.cont[index],
                           current.from.magnet.cont[index],
                           magnet.cont.data[index],
                           magnet.cont.params[index],
                           exception.reports[index+3] )

Monitor.Data.Buffer( data.to.buffer, buffer.data.request,
                    data.to.monitor, data.buffer.params,
                    exception.reports[5] )

Buffer( data.to.monitor, temp )

Exception.Report.Manager( head.processor, exception.manager.reset,
                          import.exception.reports, exception.reports,
                          dummy.switch, exception.notification,
                          exception.shutdown )

-- LOW priority process --
User.Interface( ref.signal.params, ref.signal.status,
               controller.params, data.buffer.params,
               PC.keyboard, PC.screen,
               buffer.data.request, temp,
               exception.notification )
:

#USE "system.tsr"
#USE "controll.tsr"

PROC Tail.Controller.Process( CHAN OF converter.signal.p currents.to.DACs,
                             CHAN OF BOOL DAC.switch,

                             CHAN OF signal.p signal.exchange.out,
                             CHAN OF signal.p signal.exchange.in,

                             CHAN OF exception.p export.exception.reports,
                             CHAN OF controller.p import.controller.params )

-- Tail.Controller() is the separately compiled process for all the processes
-- running on the Second main controller processor (T800-20 Mhz 32KB, ideally).

CHAN OF converter.signal.p dummy.ADC :
CHAN OF signal.p          dummy.sig.gen :

[2]CHAN OF signal.p accs.to.mode.cont, gaps.to.mode.cont :
[2]CHAN OF signal.p refs.to.mode.cont, force.from.mode.cont :
[2]CHAN OF signal.p gaps.forces.to.mag.cont, current.from.magnet.cont :

[2]CHAN OF signal.p mode.cont.data, magnet.cont.data :
CHAN OF monitor.p dummy.buffer.data :

CHAN OF controller.p dummy.params.out :
CHAN OF exception.p dummy.exception.report :
CHAN OF BOOL exception.manager.reset, dummy.shutdown :

[2]CHAN OF controller.p mode.cont.params, magnet.cont.params :
[4]CHAN OF exception.p exception.reports :

PRI PAR
  PAR
    Signal.Data.Manager( tail.processor, dummy.ADC, dummy.sig.gen,
                        accs.to.mode.cont, gaps.to.mode.cont,
                        refs.to.mode.cont, force.from.mode.cont,
                        gaps.forces.to.mag.cont, current.from.magnet.cont,
                        currents.to.DACs,
                        signal.exchange.out, signal.exchange.in,
                        mode.cont.data, magnet.cont.data, dummy.buffer.data )

    Command.Message.Manager( tail.processor, import.controller.params,
                            magnet.cont.params, mode.cont.params,
                            dummy.params.out, exception.manager.reset )

  PAR index = 0 FOR 2

```

```

    Vehicle.Mode.Controller( (index + 2), refs.to.mode.cont[index],
                             accs.to.mode.cont[index], gaps.to.mode.cont[index],
                             force.from.mode.cont[index], mode.cont.data[index],
                             mode.cont.params[index], exception.reports[index] )

    PAR index = 0 FOR 2
      Magnet.Force.Controller( (index + 2), gaps.forces.to.mag.cont[index],
                               current.from.magnet.cont[index],
                               magnet.cont.data[index],
                               magnet.cont.params[index],
                               exception.reports[index+2] )

      Exception.Report.Manager( tail.processor, exception.manager.reset,
                               dummy.exception.report, exception.reports,
                               DAC.switch, export.exception.reports,
                               dummy.shutdown )

    PAR
      SKIP
:

#USE "system.tsr"
#USE "converte.tsr"

PROC ADC.Process( CHAN OF BOOL start.conversion.in,
                 CHAN OF converter.signal.p ADC.signals.out )

-- ADC.Process() is the separately compiled process for all the processes
-- running on the ADC card processor (T212 - 16 bit integer processor).

-- Define PORTs for the ADC hardware --
PORT OF INT multiplexor :
PLACE multiplexor AT #6100 :

PORT OF INT adc :
PLACE adc AT #6000 :

CHAN OF BOOL end.of.conversion :
VAL event IS 8 : -- Transputer external hardware interrupt channel
PLACE end.of.conversion AT event :

-- Program code for ADC.Process() --
PRI PAR
  ADC.Driver( start.conversion.in, ADC.signals.out,
             multiplexor, adc, end.of.conversion )
  SKIP
:

#USE "system.tsr"
#USE "converte.tsr"

PROC DAC.Process( CHAN OF converter.signal.p DAC.signals.in,
                 CHAN OF BOOL switch.pressed.out )

-- DAC.Process() is the separately compiled process for all the processes
-- running on the DAC card processor (T212 - 16 bit integer processor).

-- Define PORTs for the DAC hardware --
PORT OF INT dac1, dac2, dac3, dac4 :
PLACE dac1 AT #6100 :
PLACE dac2 AT #6200 :
PLACE dac3 AT #6300 :
PLACE dac4 AT #6400 :

-- Define a PORT for the watchdog timer --
PORT OF INT watchdog :
PLACE watchdog AT #6700 :

-- Define a PORT for the front panel push switch --
PORT OF INT switch :
PLACE switch AT #6000 :

-- Program code for ADC.Process() --
PRI PAR
  DAC.Driver( DAC.signals.in, dac1, dac2, dac3, dac4, watchdog )
  Switch.Monitor( switch, switch.pressed.out )

```

```

:

-- Define physical link addresses --
VAL link0out IS 0 :
VAL link1out IS 1 :
VAL link2out IS 2 :
VAL link3out IS 3 :
VAL link0in IS 4 :
VAL link1in IS 5 :
VAL link2in IS 6 :
VAL link3in IS 7 :

CHAN OF BOOL          conversion.request :
CHAN OF converter.signal.p sensor.signals :

CHAN OF signal.p signals.to.tail :
CHAN OF signal.p signals.to.head :

CHAN OF controller.p tail.controller.params :
CHAN OF exception.p tail.exception.reports :

CHAN OF converter.signal.p current.demands :
CHAN OF BOOL          DAC.switch.pressed :

CHAN OF ANY PC.screen :
CHAN OF INT PC.keyboard :

PLACED PAR

PROCESSOR 1 T8 -- Head.Controllers
  PLACE conversion.request AT link1out :
  PLACE sensor.signals AT link1in :

  PLACE signals.to.tail AT link3out :
  PLACE signals.to.head AT link3in :

  PLACE tail.controller.params AT link2out :
  PLACE tail.exception.reports AT link2in :

  PLACE PC.screen AT link0out :
  PLACE PC.keyboard AT link0in :

  Head.Controller.Process( conversion.request, sensor.signals,
                           signals.to.tail, signals.to.head,
                           tail.controller.params, tail.exception.reports,
                           PC.screen, PC.keyboard )

PROCESSOR 2 T8 -- Tail.Controllers
  PLACE current.demands AT link2out :
  PLACE DAC.switch.pressed AT link2in :

  PLACE signals.to.head AT link0out :
  PLACE signals.to.tail AT link0in :

  PLACE tail.exception.reports AT link1out :
  PLACE tail.controller.params AT link1in :

  Tail.Controller.Process( current.demands, DAC.switch.pressed,
                           signals.to.head, signals.to.tail,
                           tail.exception.reports, tail.controller.params )

PROCESSOR 3 T2 -- ADC
  PLACE conversion.request AT link2in :
  PLACE sensor.signals AT link2out :

  ADC.Process( conversion.request, sensor.signals )

PROCESSOR 4 T2 -- DAC
  PLACE current.demands AT link0in :
  PLACE DAC.switch.pressed AT link0out :

  DAC.Process( current.demands, DAC.switch.pressed )

```

## E.2.2 System Constants &amp; Comms Protocols Library

```

-- CONSTANTS --

VAL num.magnets IS 4 : -- Number of vehicle magnets to be controlled
VAL num.modes IS 4 : -- Number of vehicle modes to be controlled

VAL head.processor IS TRUE :
VAL tail.processor IS NOT head.processor :

-- Controller modes --
VAL local IS 0 :
VAL vehicle IS local + 1 :
VAL user IS vehicle + 1 :

-- PROTOCOLS --

PROTOCOL exception.p IS -- Used to convey exception reports --
  INT:[]BYTE; -- Exception message text
  BYTE; -- Magnet or mode index
  REAL32; -- Exceptional or errant signal value
  BOOL: -- Severity flag (de-levitation requirement)

PROTOCOL controller.p -- Used to convey commands to the controllers --
CASE
  magnet.control.params; -- Conveys parameters to magnet force controllers
  REAL32; -- Control system sampling interval
  [num.magnets][num.modes]REAL32 -- Modes-magnets transformation matrix
  mode.control.params; -- Conveys parameters to suspension mode controllers
  REAL32; -- Control system sampling interval
  [num.modes][num.magnets]REAL32; -- Magnets-modes transformation matrix
  REAL32; -- State estimator filter frequency
  REAL32; -- Track trajectory filter frequency
  [num.modes]REAL32; -- Mode controller integral action time constant
  [num.modes]REAL32; -- Mode controller position feedback gain
  [num.modes]REAL32; -- Mode controller velocity feedback gain
  [num.modes]REAL32; -- Mode controller acceleration feedback gain
  INT; -- Control mode
  BOOL -- Reference signal injection select
  initialise.system -- Requests relevant system initialisation
:

PROTOCOL data.buffer.p -- Used to convey commands to the data buffer --
CASE
  data.buffer.params; -- Conveys parameters for storage of logged data
  REAL32; -- Data logging sample interval
  REAL32 -- Data logging duration
  data.buffer.log -- Commands storage of data at next ref signal cycle start
  data.buffer.select; -- Select source of data output from data buffer
  BOOL -- Output stored data (NOT on-line data stream)
:

PROTOCOL signal.gen.p -- Used to convey commands to the signal generator --
CASE
  signal.gen.params; -- Conveys parameters to the reference signal generator
  REAL32; -- Control system sampling interval
  REAL32; -- Mean value of air gap reference
  [num.modes]REAL32; -- Mean air gap mode factors
  BOOL; -- Dynamic reference signal select
  BOOL; -- Select sine wave reference signal (NOT square wave)
  REAL32; -- Reference signal frequency
  REAL32; -- Reference signal amplitude
  [num.modes]REAL32 -- Position reference mode factors
  signal.gen.levitate; -- Command vehicle levitation up/down
  BOOL -- Levitate vehicle (NOT de-levitate)
  signal.gen.levitated; -- Status report from signal generator
  BOOL -- Vehicle levitated (NOT de-levitated)
:

PROTOCOL converter.signal.p -- Used to convey converter signals --
CASE
  ADC.acc.raw.t; INT16 -- Raw ADC acc measurement
  ADC.gap.raw.t; INT16 -- Raw ADC gap measurement
  DAC.I.mA.t; BYTE; INT16 -- Magnet index; current in mA

```





## E.2.3 ADC and DAC Driver processes Library

```

#USE "system.tsr"

PROC ADC.Driver( CHAN OF BOOL data.request.in,
  CHAN OF converter.signal.p ADC.signals.out,
  PORT OF INT multiplexor, adc,
  CHAN OF BOOL end.of.conversion )

-- ADC.Driver waits for a start conversion trigger signal and then requests the
-- A/D conversion of each acceleration and air gap signal before scaling them and
-- outputting them to the data signal pool manager.
--
-- This process uses no external variables and must be configured for
-- high priority operation on the ADC card processor (T212).

-- Gap and Acc sensor multiplexor addresses :
VAL gap1.chan IS 1 :
VAL gap2.chan IS 2 :
VAL gap3.chan IS 4 :
VAL gap4.chan IS 8 :
VAL acc1.chan IS 16 :
VAL acc2.chan IS 32 :
VAL acc3.chan IS 64 :
VAL acc4.chan IS 128 :

-- Channel sequence definition (accs & gaps must be ordered 1-4).
-- Accelerations are read first since they can be processed before the air
-- gap signals are needed.
VAL INT num.adc.reads IS 2 * num.magnets :
VAL [num.adc.reads]INT sensor.sequence IS
  [ acc1.chan, acc2.chan, acc3.chan, acc4.chan,
    gap1.chan, gap2.chan, gap3.chan, gap4.chan ] :

BOOL go, done :
INT adc.reading, value, time :
TIMER clock :

SEQ

  adc ? adc.reading -- Start the converter rolling

  WHILE TRUE
    SEQ
      -- ADC conversions are achieved by setting the multiplexor channel address,
      -- then reading the ADC (which gives the previous conversion value and starts
      -- the next conversion. End of conversion is notified by a channel.

      multiplexor ! sensor.sequence[ 0 ] -- Select first multiplexor channel
      clock ? time
      clock ? AFTER (time PLUS 3) -- 3 us settling time for multiplexor

      data.request.in ? go -- Wait for request for data

      end.of.conversion ? done -- Clear last end of conversion notification
      adc ? adc.reading -- Start conversion of first channel

      -- Read each sensor signal and then scale and output --
      SEQ chan.index = 0 FOR num.adc.reads
        SEQ
          multiplexor ! sensor.sequence[ (chan.index + 1) REM num.adc.reads ]
          clock ? time
          clock ? AFTER (time PLUS 3) -- 3 us settling time for multiplexor

          end.of.conversion ? done -- Wait for conversion to complete
          adc ? adc.reading -- Read value from the ADC
          value := (adc.reading /\ #FFF0) -- 12 bit ADC, mask other bits

          CASE sensor.sequence[ chan.index]

            acc1.chan, acc2.chan, acc3.chan, acc4.chan
              ADC.signals.out ! ADC.acc.raw.t; INT16 value

            gap1.chan, gap2.chan, gap3.chan, gap4.chan
              ADC.signals.out ! ADC.gap.raw.t; INT16 value
  :

```

```

#USE "system.tsr"

PROC DAC.Driver( CHAN OF converter.signal.p DAC.signals.in,
                PORT OF INT dac0, dac1, dac2, dac3,
                PORT OF INT watchdog )

-- DAC.Driver scales the magnet current demands and sends them to the DACs
-- It also resets the watchdog timer each time a current demand is processed.
--
-- This process uses no external variables and must be configured for
-- high priority operation on the DAC card processor (T212).

-- DAC specification --
VAL levels.per.fsd IS 4096 (INT32):
VAL volts.per.fsd IS 10 :
VAL min.DAC.level IS 0 :
VAL max.DAC.level IS 4095 :

-- Electromagnet current amplifier details --
VAL amps.per.volt IS 2 :

-- Calculate composite denominator term --
VAL INT32 mA.per.fsd IS INT32 (1000 * (amps.per.volt * volts.per.fsd)) :

BYTE magnet :
INT16 I.mA :
INT DAC.drive :

WHILE TRUE
SEQ
  DAC.signals.in ? CASE DAC.I.mA.t; magnet; I.mA

  DAC.drive := INT ((INT32 I.mA) * levels.per.fsd) / mA.per.fsd
  IF
    (DAC.drive < min.DAC.level)
      DAC.drive := min.DAC.level
    (DAC.drive > max.DAC.level)
      DAC.drive := max.DAC.level
  TRUE
  SKIP

  CASE INT magnet
  0
    dac0 ! DAC.drive
  1
    dac1 ! DAC.drive
  2
    dac2 ! DAC.drive
  3
    dac3 ! DAC.drive

  watchdog ! 0
:

```

```

#USE "system.tsr"

PROC Switch.Monitor( PORT OF INT  switch,
                    CHAN OF BOOL  switch.pressed )

-- Switch.Monitor generates an exception message each time the push switch
-- on the front panel of the DAC card is pressed. Debouncing and hysteresis
-- are required before accepting a switch actuation.

-- This process uses no external variables and MUST be configured for low
-- priority operation.

VAL [5]BYTE message IS [0 (BYTE), 0 (BYTE), 68 (BYTE), 65 (BYTE), 67 (BYTE) ] :
VAL REAL32 zero IS 0.0 (REAL32) :
VAL INT sample.time.ticks IS 156 : -- approximately 10 ms

INT filter, time, input :
BOOL pressed, pressed.before :
TIMER clock :

SEQ
  filter := 0
  pressed := FALSE
  clock ? time

  WHILE TRUE
    SEQ
      switch ? input
      input := (input /\ 1) * 1000

      -- Debounce the switch output using a low-pass filter with Tc = 10 Ts
      filter := ( (filter * 9) + input ) / 10

      -- Detect switch transitions and apply debouncing --
      pressed.before := pressed
      pressed := (filter > 500)
      IF
        pressed AND (NOT pressed.before)
          SEQ
            filter := filter + 500
            switch.pressed ! TRUE
            (NOT pressed) AND pressed.before
            filter := filter - 500
          TRUE
        SKIP

      -- Wait for next sampling instant --
      time := time PLUS sample.time.ticks
      clock ? AFTER time
:

```

## E.2.4 Control processes Library

```

#USE "system.tsr"
#USE  snqlmath

PROC Reference.Signal.Generator( CHAN OF BOOL request.data.conversion.out,
                                CHAN OF signal.p  ref.signals.out,

                                CHAN OF signal.gen.p parameters.in,
                                CHAN OF signal.gen.p status.out,
                                CHAN OF BOOL shutdown.request.in,
                                CHAN OF exception.p exception.report.out )

-- Reference.Signal.Generator() receives parameters and commands from the user
-- interface and exception report manager. It initiates each iteration of the
-- control system by requesting the ADC to read the sensor signals. It also
-- generates a time reference signal and a position refernce signal for a smooth
-- startup and shutdown as well as generating periodic signals for test purposes.
--
-- This process uses no external variables and must be configured for
-- high priority operation.

-- Worldly & other constants --
VAL two.pi IS 2.0 (REAL32) * 3.1415926 (REAL32) :
VAL set.down.on.track IS 0.008 (REAL32) :
VAL start.stop.time.constant IS 0.5 (REAL32) :

-- General variables --
CHAN OF signal.gen.p status.buffer :
BOOL buffered.status :

BOOL running, levitate, fully.up, fully.down, previously.fully.down :
BOOL dynamic.ref.selected, sine.wave.selected :
REAL32 sample.interval, mean.gap, ref.freq, ref.amplitude :
[num.modes]REAL32 mean.gap.coeffs, dyn.ref.coeffs, mode.refs :
REAL32 filter.decay.coeff, filter.input.coeff, filter1, filter2 :
REAL32 gap.ref, mean.ref, dyn.ref, time, sine.wave, cosine.wave :

-- Sampling values and variables --
VAL ticks.per.sec IS 1000000.0 (REAL32) :
INT sample.interval.ticks, sample.time, time.now :
REAL32 cycle.time :
TIMER clock :

PAR
  WHILE TRUE
    SEQ
      status.buffer ? CASE signal.gen.levitated; buffered.status
      status.out ! signal.gen.levitated; buffered.status
    SEQ
      running := FALSE
      previously.fully.down := TRUE
      WHILE TRUE
        PRI ALT
          ALT
            shutdown.request.in ? levitate
            levitate := FALSE
            parameters.in ? CASE
              signal.gen.levitate; levitate
            SKIP
            signal.gen.params; sample.interval; mean.gap; mean.gap.coeffs;
            dynamic.ref.selected; sine.wave.selected; ref.freq;
            ref.amplitude; dyn.ref.coeffs
          SEQ
            sample.interval.ticks := INT ROUND (ticks.per.sec * sample.interval)
            filter.decay.coeff := exp(-(sample.interval/start.stop.time.constant))
            filter.input.coeff := 1.0 (REAL32) - filter.decay.coeff
            ref.amplitude := ref.amplitude / 2.0 (REAL32) -- was pk-pk
            IF
              NOT running -- Then Initialise system --
                SEQ
                  running := TRUE
                  levitate := FALSE
                  filter1 := set.down.on.track
                  filter2 := filter1

```

```

        time := 0.0 (REAL32)
        clock ? sample.time
    TRUE
    SKIP

running & SKIP
SEQ
-- Set mean reference gap for either up or down --
IF
    levitate
    gap.ref := mean.gap
    NOT levitate
    SEQ
        gap.ref := set.down.on.track
        time := 0.0 (REAL32)

-- Ensure smooth startup & shutdown by filtering the reference signal --
filter1 := (filter1 * filter.decay.coeff)+(gap.ref * filter.input.coeff)
filter2 := (filter2 * filter.decay.coeff)+(filter1 * filter.input.coeff)
mean.ref := filter2
fully.up := (mean.ref < (mean.gap + 1.0E-4(REAL32)))
previously.fully.down := fully.down
fully.down := (mean.ref > (set.down.on.track - 1.0E-4(REAL32)))

-- Add dynamic reference to mean reference if required --
IF
    (fully.up AND dynamic.ref.selected)
    SEQ
        -- Advance time and limit domain to prevent loss of precision --
        IF
            (time < (1.0(REAL32) / ref.freq))
            time := time + sample.interval
            TRUE
            time := 0.0 (REAL32)

        -- Generate dynamic reference component --
        sine.wave := ref.amplitude * SIN( two.pi * (ref.freq * time) )
        cosine.wave := ref.amplitude * COS( two.pi * (ref.freq * time) )
        IF
            sine.wave.selected
            dyn.ref := sine.wave
            TRUE -- square wave --
            IF
                (sine.wave > 0.0 (REAL32))
                dyn.ref := ref.amplitude
            TRUE
                dyn.ref := - ref.amplitude
        TRUE
        dyn.ref := 0.0(REAL32)

-- Wait for next sampling time --
clock ? time.now
cycle.time := REAL32 TRUNC (time.now MINUS sample.time)
sample.time := sample.time PLUS sample.interval.ticks
IF
    (time.now AFTER sample.time)
    VAL [ ]BYTE message IS "Error: Sampling period too short, cycle time:"

    SEQ
        exception.report.out ! SIZE message::message; BYTE 0;
            (cycle.time / ticks.per.sec) * 1000.0 (REAL32); TRUE
        sample.time := time.now
    TRUE
    clock ? AFTER sample.time

IF
    NOT fully.down
    SEQ
        -- Request conversion of sensor signals by the ADC --
        request.data.conversion.out ! TRUE

        -- Output the time reference and mode reference signals --
        SEQ index = 0 FOR num.modes
            mode.refs[index] := (mean.ref * mean.gap.coeffs[index]) +
                (dyn.ref * dyn.ref.coeffs[index])
        --mode.refs[2] := (cosine.wave * dyn.ref.coeffs[2])

        ref.signals.out ! time.stamp.t; time
        ref.signals.out ! mode.pos.refs.t; mode.refs
    (fully.down AND (NOT previously.fully.down))
    status.buffer ! signal.gen.levitated; FALSE

```

```

TRUE
SKIP
:
#USE "system.tsr"

PROC Signal.Data.Manager( VAL BOOL head.manager,

    CHAN OF converter.signal.p from.analogue.converter,
    CHAN OF signal.p sig.gen.refs.in,
    []CHAN OF signal.p accs.to.mode.cont, gaps.to.mode.cont,
    []CHAN OF signal.p refs.to.mode.cont, force.from.mode.cont,
    []CHAN OF signal.p gaps.and.forces.to.mag.cont, current.from.mag.cont,
    CHAN OF converter.signal.p to.analogue.converter,

        CHAN OF signal.p exchange.data.out, exchange.data.in,

        []CHAN OF signal.p data.from.mode.cont,
        []CHAN OF signal.p force.from.magnet.cont,
        CHAN OF monitor.p data.to.monitor.buffer )

-- Signal.Data.Manager() runs on both main processors and controls
-- the flow of all signals from the ADC through to the DAC. The Boolean
-- 'head.manager' determines which processes are connected to this process.
--
-- This process uses no external variables and should be configured for
-- high priority operation.

VAL num.local.magnet.controllers IS SIZE gaps.and.forces.to.mag.cont :
VAL num.local.mode.controllers IS SIZE accs.to.mode.cont:

-- ADC input voltage range --
VAL volts.per.fsd IS 5.0 (REAL32) / 32768.0 (REAL32) :

-- Accelerometer details --
VAL Gs.per.volt IS 0.2 (REAL32):
VAL G IS 9.81 (REAL32) :
VAL acc.multiplier IS (volts.per.fsd * Gs.per.volt) * G :

-- Gap sensor details --
VAL metres.per.volt IS 0.00125 (REAL32) :
VAL gap.multiplier IS volts.per.fsd * metres.per.volt :
VAL sensor.offset IS 0.0032 (REAL32) : -- 3.2 mm
VAL net.track.gap IS 0.009 (REAL32) : -- 9 mm
VAL gap.offset IS (net.track.gap - sensor.offset) :

BYTE magnet, MAGNET, mode, MODE :
INT m, M :

INT16 magnet.acc.raw, magnet.gap.raw :

REAL32 time, magnet.acc, magnet.gap, magnet.current, MAGNET.CURRENT :
[num.magnets]REAL32 magnet.accs, magnet.gaps, magnet.currents :
REAL32 magnet.force, MAGNET.FORCE :
[num.magnets]REAL32 magnet.forces, MAGNET.FORCES :

REAL32 mode.force, MODE.FORCE :
[num.modes]REAL32 mode.pos.refs, mode.forces :

INT16 magnet.current.mA, MAGNET.CURRENT.mA :

REAL32 gap, acc, vel, pos, trk.pos, GAP, ACC, VEL, POS, TRK.POS :
[num.modes]REAL32 gaps, accs, vels, poss, trk.poss :

WHILE TRUE
SEQ
-- Get time stamp and reference signals from the signal generator --
IF head.manager
SEQ
sig.gen.refs.in ? CASE time.stamp.t; time
sig.gen.refs.in ? CASE mode.pos.refs.t; mode.pos.refs
exchange.data.out ! time.stamp.t; time
exchange.data.out ! mode.pos.refs.t; mode.pos.refs
NOT head.manager
SEQ
exchange.data.in ? CASE time.stamp.t; time
exchange.data.in ? CASE mode.pos.refs.t; mode.pos.refs

```

```

-- And send to the mode controllers --
SEQ controllers = 0 FOR num.local.mode.controllers
  refs.to.mode.cont[ controllers ] ! mode.pos.refs.t; mode.pos.refs

-- Get magnet acceleration measurements from the ADC / other processor --
SEQ magnet.index = 0 FOR num.magnets
  SEQ
  IF
  head.manager
  SEQ
  magnet := BYTE magnet.index
  from.analogue.converter ? CASE ADC.acc.raw.t; magnet.acc.raw
  magnet.acc := acc.multiplier * (REAL32 ROUND magnet.acc.raw)
  exchange.data.out ! magnet.acc.t; magnet; magnet.acc
  NOT head.manager
  exchange.data.in ? CASE magnet.acc.t; magnet; magnet.acc
  magnet.accs[ INT magnet ] := magnet.acc

-- And send to the mode controllers --
SEQ controllers = 0 FOR num.local.mode.controllers
  accs.to.mode.cont[ controllers ] ! magnet.accs.t; magnet.accs

-- Get magnet air gap measurements from the ADC / other processor --
SEQ magnet.index = 0 FOR num.magnets
  SEQ
  IF
  head.manager
  SEQ
  magnet := BYTE magnet.index
  from.analogue.converter ? CASE ADC.gap.raw.t; magnet.gap.raw
  magnet.gap := gap.offset - (gap.multiplier * (REAL32 ROUND magnet.gap.raw))
  exchange.data.out ! magnet.gap.t; magnet; magnet.gap
  NOT head.manager
  exchange.data.in ? CASE magnet.gap.t; magnet; magnet.gap
  magnet.gaps[ INT magnet ] := magnet.gap

-- And send to the mode controllers --
SEQ controllers = 0 FOR num.local.mode.controllers
  gaps.to.mode.cont[ controllers ] ! magnet.gaps.t; magnet.gaps

-- Get force demands from mode controllers and exchange with other processor --
SEQ controllers = 0 FOR num.local.mode.controllers
  SEQ
  force.from.mode.cont[controllers] ? CASE mode.force.t; mode; mode.force
  PAR
  exchange.data.out ! mode.force.t; mode; mode.force
  exchange.data.in ? CASE mode.force.t; MODE; MODE.FORCE
  mode.forces[ INT mode ] := mode.force
  mode.forces[ INT MODE ] := MODE.FORCE

-- And send to the magnet controllers --
SEQ controllers = 0 FOR num.local.magnet.controllers
  gaps.and.forces.to.mag.cont[ controllers ] ! magnet.gaps.t; magnet.gaps
SEQ controllers = 0 FOR num.local.magnet.controllers
  gaps.and.forces.to.mag.cont[ controllers ] ! mode.forces.t; mode.forces

-- Get current demands from the magnet controllers and exchange --
-- with the other processor --
SEQ controllers = 0 FOR num.local.magnet.controllers
  SEQ
  current.from.mag.cont[controllers] ? CASE magnet.current.t;
  magnet; magnet.current
  magnet.current.mA := INT16 ROUND (1000.0(REAL32) * magnet.current)
  IF
  head.manager
  PAR
  exchange.data.out ! magnet.current.t; magnet; magnet.current
  exchange.data.in ? CASE magnet.current.t; MAGNET; MAGNET.CURRENT
  NOT head.manager
  SEQ
  PAR
  exchange.data.out ! magnet.current.t; magnet; magnet.current
  exchange.data.in ? CASE magnet.current.t; MAGNET; MAGNET.CURRENT
  to.analogue.converter ! DAC.I.mA.t; magnet; magnet.current.mA
  MAGNET.CURRENT.mA := INT16 ROUND (1000.0(REAL32) * MAGNET.CURRENT)
  to.analogue.converter ! DAC.I.mA.t; MAGNET; MAGNET.CURRENT.mA
  magnet.currents[ INT magnet ] := magnet.current
  magnet.currents[ INT MAGNET ] := MAGNET.CURRENT

```



```

-- Get the internal signals from the magnet controllers --
SEQ controllers = 0 FOR num.local.magnet.controllers
  SEQ
    force.from.magnet.cont[controllers] ? CASE magnet.force.t;
                                         magnet; magnet.force
  PAR
    exchange.data.out ! magnet.force.t; magnet; magnet.force
    exchange.data.in ? CASE magnet.force.t; MAGNET; MAGNET.FORCE
    magnet.forces[ INT magnet ] := magnet.force
    magnet.forces[ INT MAGNET ] := MAGNET.FORCE

-- and the internal signals from the mode controllers --
SEQ controllers = 0 FOR num.local.mode.controllers
  SEQ
    data.from.mode.cont[controllers] ? CASE mode.block.t; mode; gap; acc;
                                         vel; pos; trk.pos
  PAR
    exchange.data.out ! mode.block.t; mode; gap; acc; vel; pos; trk.pos
    exchange.data.in ? CASE mode.block.t; MODE; GAP; ACC; VEL; POS; TRK.POS
    m, M := INT mode, INT MODE
    gaps[m], accs[m], vels[m], poss[m], trk.poss[m] := gap, acc, vel, pos, trk.pos
    gaps[M], accs[M], vels[M], poss[M], trk.poss[M] := GAP, ACC, VEL, POS, TRK.POS

-- And send ALL control system data signals to the data monitor's buffer --
IF head.manager
  [4][num.magnets]REAL32 magnet.data :
  PLACE magnet.data IN VECSPACE :
  [7][num.modes]REAL32 mode.data :
  PLACE mode.data IN VECSPACE :
  SEQ
    magnet.data[0] := magnet.gaps
    magnet.data[1] := magnet.accs
    magnet.data[2] := magnet.forces
    magnet.data[3] := magnet.currents
    mode.data[0] := mode.pos.refs
    mode.data[1] := gaps
    mode.data[2] := accs
    mode.data[3] := vels
    mode.data[4] := poss
    mode.data[5] := trk.poss
    mode.data[6] := mode.forces
    data.to.monitor.buffer ! time; magnet.data; mode.data
  TRUE
  SKIP
:

#USE "system.tsr"
#USE snglmath

PROC Vehicle.Mode.Controller( VAL INT mode.index,
  CHAN OF signal.p position.references.in,
  CHAN OF signal.p magnet.accs.in, magnet.gaps.in,
  CHAN OF signal.p mode.force.out,
  CHAN OF signal.p internal.signals.out,

  CHAN OF controller.p parameters.in,
  CHAN OF exception.p exception.out )

-- Calculate.Mode.Force() performs the following tasks:
-- 1. Receives the air gap and acceleration sensor signals for each magnet.
-- 2. Transforms the sensor signals to vehicle mode 'mode.index' signals.
-- 3. Estimates the mode velocity, position and track position.
-- 4. Filters the track position to form a reference track trajectory.
-- 5. Controls the absolute vehicle mode position using the above as a reference.
-- 6. Outputs the resultant vehicle mode force demand.

-- This process uses no external variables and should be configured for
-- high priority operation.

VAL pi IS 3.1415926 (REAL32) :
VAL two.pi IS 2.0 (REAL32) * pi :

VAL vel.limit IS 0.1 (REAL32) : -- 0.1 mm/ms velocity limit --
VAL [] BYTE warning.message IS "Warning: Excessive velocity, V = " :
```

```

REAL32 sample.interval :
REAL64 sample.interval.r64 :
[num.modes][num.magnets]REAL32 magnets.to.modes.transform :
[num.magnets]REAL32 mode.transform :
[num.modes]REAL32 integral.times, stiffnesses, dampings, massnesses :
REAL32 integral.time, stiffness, damping, massness :
INT control.mode :
BOOL track.ref.select :

REAL32 est.cutoff.Hz, traj.cutoff.Hz :
REAL64 est.input.factor, est.decay.factor :
REAL64 traj.input.factor, traj.decay.factor :

REAL64 mode.pos.ref :
[num.modes]REAL32 mode.pos.refs :
REAL64 track.pos.ref, pos.ref :
[num.magnets]REAL32 magnet.gaps, magnet.accs :
REAL32 gap, acc :
REAL64 acc.r64, acc.lp, acc.hp, vel.hp, pos.hp, pos.error :
REAL64 track.pos, traj.pos.f1, traj.pos.f2, track.trajectory :
REAL32 acc.feedback, vel.feedback, pos.feedback, int.feedback, pos.error.r32 :
REAL32 min.integral.force, max.integral.force :
REAL32 force.demand, acc.hp.r32, vel.hp.r32, pos.hp.r32, track.pos.r32 :

WHILE TRUE
  ALT
    parameters.in ? CASE
      mode.control.params; sample.interval; magnets.to.modes.transform;
      est.cutoff.Hz; traj.cutoff.Hz;
      integral.times; stiffnesses; dampings; massnesses;
      control.mode; track.ref.select
    SEQ
      -- Select relevant mode control parameters --
      mode.transform := magnets.to.modes.transform[ mode.index ]
      integral.time := integral.times[ mode.index ]
      stiffness:= stiffnesses[ mode.index ]
      damping := dampings[ mode.index ]
      massness := massnesses[ mode.index ]
      CASE control.mode
        local, user
          SEQ
            min.integral.force := 200.0 (REAL32)
            max.integral.force := 500.0 (REAL32)
          vehicle
            IF
              (mode.index = 0) -- heave mode
                SEQ
                  min.integral.force := 700.0 (REAL32)
                  max.integral.force := 2500.0 (REAL32)
            TRUE
              SEQ
                min.integral.force := -1000.0 (REAL32)
                max.integral.force := 1000.0 (REAL32)

      -- Calculate filter coefficients --
      sample.interval.r64 := REAL64 sample.interval
      est.decay.factor := REAL64 exp((-two.pi)*(est.cutoff.Hz*sample.interval))
      est.input.factor := 1.0 (REAL64) - est.decay.factor
      traj.decay.factor:=REAL64 exp((-two.pi)*(traj.cutoff.Hz*sample.interval))
      traj.input.factor := 1.0 (REAL64) - traj.decay.factor

  initialise.system
  SEQ -- reset filters etc.
    acc.lp := 0.0 (REAL64)
    vel.hp := 0.0 (REAL64)
    pos.hp := 0.0 (REAL64)
    track.pos := 0.0 (REAL64)
    traj.pos.f1 := track.pos
    traj.pos.f2 := traj.pos.f1
    int.feedback := 0.0 (REAL32)

  position.references.in ? CASE mode.pos.refs.t; mode.pos.refs
  SEQ -- run controller
    mode.pos.ref := REAL64 mode.pos.refs[ mode.index ]
  IF
    track.ref.select
      track.pos.ref, pos.ref := mode.pos.ref, 0.0 (REAL64)
  TRUE
    track.pos.ref, pos.ref := 0.0 (REAL64), mode.pos.ref

```

```

PAR
  SEQ
    -- Input the magnet air gaps --
    magnet.gaps.in ? CASE magnet.gaps.t; magnet.gaps

    -- Transform the magnet gaps to obtain the mode gap --
    gap := 0.0 (REAL32)
    SEQ index = 0 FOR num.magnets
      gap := gap + (mode.transform[index] * magnet.gaps[index])

  SEQ
    -- Input the (high pass filtered) magnet accelerations --
    magnet.accs.in ? CASE magnet.accs.t; magnet.accs

    -- Transform the magnet accelerations to the mode acceleration --
    acc := 0.0 (REAL32)
    SEQ index = 0 FOR num.magnets
      acc := acc + (mode.transform[index] * magnet.accs[index])

    -- High-pass filter the acceleration to remove any offset --
    acc.r64 := REAL64 acc
    acc.lp := (acc.lp * est.decay.factor) + (acc.r64 * est.input.factor)
    acc.hp := acc.r64 - acc.lp
    acc.hp.r32 := REAL32 ROUND acc.hp

    -- Estimate the absolute velocity and position --
    vel.hp := (vel.hp * est.decay.factor) + (acc.hp * sample.interval.r64)
    vel.hp.r32 := REAL32 ROUND vel.hp
    pos.hp := (pos.hp * est.decay.factor) + (vel.hp * sample.interval.r64)
    pos.hp.r32 := REAL32 ROUND pos.hp

    -- Estimate the absolute track position --
    track.pos := (pos.hp + track.pos.ref) - (REAL64 gap)
    track.pos.r32 := REAL32 ROUND track.pos

    -- and filter to form the track trajectory --
    traj.pos.f1 := (traj.pos.f1*traj.decay.factor)+(track.pos*traj.input.factor)
    traj.pos.f2 := (traj.pos.f2*traj.decay.factor)+(traj.pos.f1*traj.input.factor)
    track.trajectory := traj.pos.f2

    -- Calculate the absolute position error --
    pos.error := (pos.hp - pos.ref) - track.trajectory
    pos.error.r32 := REAL32 ROUND pos.error

    -- Calculate the feedback components --
    acc.feedback := massness * acc.hp.r32
    vel.feedback := damping * vel.hp.r32
    pos.feedback := stiffness * pos.error.r32
    IF
      (int.feedback < min.integral.force)
        int.feedback := min.integral.force
      (int.feedback > max.integral.force)
        int.feedback := max.integral.force
      (integral.time > 0.0 (REAL32) )
        int.feedback := int.feedback +
          ( pos.error.r32*sample.interval ) * (stiffness/integral.time) )
    TRUE
      int.feedback := 0.0 (REAL32)

    -- Total the force requirement --
    force.demand := ((int.feedback + pos.feedback)+(vel.feedback + acc.feedback))

  PAR
    -- Output mode force demand --
    mode.force.out ! mode.force.t; BYTE mode.index; force.demand

    -- Output internal signals for monitoring --
    internal.signals.out ! mode.block.t; BYTE mode.index; gap; acc.hp.r32;
      vel.hp.r32; pos.hp.r32; track.pos.r32

    -- Check velocity signal magnitude --
    IF
      (vel.hp.r32 < (-vel.limit)) OR (vel.hp.r32 > vel.limit)
        exception.out ! SIZE warning.message::warning.message;
          BYTE mode.index; vel.hp.r32; TRUE
    TRUE
      SKIP

```

```

#USE "system.tsr"
#USE  snlmath

PROC Magnet.Force.Controller( VAL INT  magnet.index,
    CHAN OF signal.p  gaps.and.forces.in,
    CHAN OF signal.p  current.out,
    CHAN OF signal.p  magnet.force.out,

    CHAN OF controller.p  parameters.in,
    CHAN OF exception.p  exception.out )

-- Calculate.magnet.current uses the nonlinear magnet force model to determine
-- the required current for the demanded force at the present airgap.

-- Worldly constants --
VAL pi IS 3.1415926 (REAL32) :
VAL mu.air IS 1.2566E-6 (REAL32) : -- Permeability of free space
-- These are used to make the equations more readable --
VAL zero IS 0.0 (REAL32) :
VAL one IS 1.0 (REAL32) :
VAL two IS 2.0 (REAL32) :
VAL four IS 4.0 (REAL32) :

-- Electromagnet parameters --
VAL y IS 0.0015 (REAL32) : -- Lateral offset between magnet & track poles
VAL l IS 0.200 (REAL32) : -- Magnet length
VAL w IS 0.033 (REAL32) : -- Width between the magnet pole pieces
VAL h IS 0.063 (REAL32) : -- Height of the magnet pole pieces
VAL t IS 0.030 (REAL32) : -- Width between the track pole pieces
VAL p IS 0.0095 (REAL32) : -- Width of the pole pieces

VAL N.coils IS 274.0 (REAL32) : -- Number of coil turns
VAL min.current IS 0.0 (REAL32) : -- Impose current limit
VAL max.current IS 20.0 (REAL32) : -- Impose current limit
VAL mu.iron IS 2000.0 (REAL32) : -- Maximum permeability of core material
VAL flux.roll.start IS 1.0 (REAL32) : -- Start of permeability roll-off (/Tesla)
VAL flux.roll.stop IS 1.7 (REAL32) : -- End of permeability roll-off (/Tesla)

VAL T.eddy IS 0.0015 (REAL32) : -- Target eddy current time constant
VAL N.phase.lead IS 3.0 (REAL32) : -- Phase-lead ratio to achieve the above

-- Input and transformation variables --
REAL32 sample.interval, mag.force :
[num.magnets][num.modes]REAL32 modes.to.magnets.matrix :
[num.modes]REAL32 magnet.transform, mode.forces :
[num.magnets]REAL32 magnet.gaps :

-- Nonlinear magnet model variables --
REAL32 T.phase.lead, input.factor, decay.factor :
REAL32 flux.LP, flux.comp :
REAL32 R.track, R.leakage, R.airgap, R.magnet :
REAL32 force.demand, airgap, force.per.pole :
REAL32 airgap.flux, flux.squared, leakage.flux, magnet.flux :
REAL32 flux.density, mu.magnet :
REAL32 airgaps.plus.track.mmf, magnet.mmf :
REAL32 current.demand :

-- Calculate the track and leakage reluctances --
VAL R.track IS ( t + (four*p) ) / ( (mu.iron*mu.air) * (l*p) ) :
VAL R.leakage IS w / ( mu.air * ( (1+((two*w)/pi)) * ((h/two)+(w/pi)) ) ) :

WHILE TRUE
    ALT
        parameters.in ? CASE
            magnet.control.params; sample.interval; modes.to.magnets.matrix
            SEQ
                -- Select relevant magnet control parameters --
                magnet.transform := modes.to.magnets.matrix[ magnet.index ]

                -- Calculate phase-lead compensator coefficients --
                IF
                    (T.eddy > sample.interval)
                        T.phase.lead := T.eddy
                    TRUE
                        T.phase.lead := sample.interval

                decay.factor := exp(- (sample.interval / T.phase.lead))
                input.factor := one - decay.factor

```

```

initialise.system
    flux.LP := zero -- Reset phase-lead compensator

gaps.and.forces.in ? CASE magnet.gaps.t; magnet.gaps
SEQ
    -- Calculate airgap reluctance --
    airgap := magnet.gaps[ magnet.index ]
    R.airgap := airgap / ( (mu.air*1) * ( p + ((two/pi)*airgap) ) )

    gaps.and.forces.in ? CASE mode.forces.t; mode.forces
    mag.force := 0.0 (REAL32)
    SEQ index = 0 FOR num.modes
        mag.force := mag.force + (magnet.transform[index] * mode.forces[index])

    IF
        (force.demand < zero)
            force.demand := zero
        TRUE
            force.demand := mag.force

    -- Calculate the gross force per pole --
    force.per.pole := force.demand /
        ( two * ( one - ( (y*y)/airgap) / (airgap+((pi*p)/two)) ) )

    -- Calculate the required airgap flux --
    flux.squared := force.per.pole * ( two*airgap ) / R.airgap )
    IF
        (flux.squared > zero)
            airgap.flux := SQRT( flux.squared )
        TRUE
            airgap.flux := zero

    -- Calculate the mmf required to overcome the airgap and track reluctances
    airgaps.plus.track.mmf := airgap.flux * ( two*R.airgap ) + R.track )

    -- Calculate the consequential leakage flux --
    leakage.flux := airgaps.plus.track.mmf / R.leakage

    -- Calculate the resulting electromagnet flux --
    magnet.flux := airgap.flux + leakage.flux

    -- Apply phase lead compensation to the magnet flux demand --
    flux.LP := (flux.LP * decay.factor) + (magnet.flux * input.factor)
    flux.comp := (N.phase.lead * magnet.flux) - ((N.phase.lead-one) * flux.LP)

    -- Calculate the magnet reluctance at this flux level --
    flux.density := magnet.flux / (1 * p)
    IF
        (flux.density < flux.roll.start)
            mu.magnet := mu.iron
        (flux.density < flux.roll.stop)
            mu.magnet := mu.iron * (1.1(REAL32) - ( (flux.density-flux.roll.start)/
                (flux.roll.stop - flux.roll.start) ) )
        TRUE
            mu.magnet := mu.iron * 0.1(REAL32)
    R.magnet := ( two*h ) + (w+(two*p)) ) / ( (mu.air*mu.magnet) * (1*p) )

    -- Calculate the mmf required to overcome the magnet reluctance --
    magnet.mmf := flux.comp * R.magnet

    -- Finally, calculate the current required to produce the total mmf --
    current.demand := (airgaps.plus.track.mmf + magnet.mmf) / N.coils
    IF
        (current.demand > max.current)
            current.demand := max.current
        (current.demand < min.current)
            current.demand := min.current
        TRUE
            SKIP

    -- Output magnet current demand (and force demand for monitoring) --
    PAR
        current.out ! magnet.current.t; BYTE magnet.index; current.demand
        magnet.force.out ! magnet.force.t; BYTE magnet.index; mag.force

```

```

#USE "system.tsr"

PROC Command.Message.Manager( VAL BOOL head.manager,
    CHAN OF controller.p commands.in,
    []CHAN OF controller.p magnet.controller.commands,
    []CHAN OF controller.p mode.controller.commands,
    CHAN OF controller.p commands.out,
    CHAN OF BOOL exception.manager.reset )

VAL num.local.magnet.controllers IS SIZE magnet.controller.commands :
VAL num.local.mode.controllers IS SIZE mode.controller.commands :

REAL32 sample.time, est.freq, traj.freq, mass :
[num.modes][num.magnets]REAL32 input.matrix :
[num.magnets][num.modes]REAL32 output.matrix :
[num.modes]REAL32 integral.T, stiffness, damping, massness :
INT control.mode :
BOOL ref.sig.injection.select :

WHILE TRUE
    commands.in ? CASE

        magnet.control.params; sample.time; output.matrix
        SEQ
        IF
            head.manager
                commands.out ! magnet.control.params;
                    sample.time; output.matrix
        TRUE
        SKIP

        SEQ channels = 0 FOR num.local.magnet.controllers
            magnet.controller.commands[ channels ] ! magnet.control.params;
                sample.time; output.matrix

        mode.control.params; sample.time; input.matrix; est.freq; traj.freq;
        integral.T; stiffness; damping; massness;
        control.mode; ref.sig.injection.select

        SEQ
        IF
            head.manager
                commands.out ! mode.control.params;
                    sample.time; input.matrix; est.freq; traj.freq;
                    integral.T; stiffness; damping; massness;
                    control.mode; ref.sig.injection.select
        TRUE
        SKIP

        SEQ channels = 0 FOR num.local.mode.controllers
            mode.controller.commands[ channels ] ! mode.control.params;
                sample.time; input.matrix; est.freq; traj.freq;
                integral.T; stiffness; damping; massness;
                control.mode; ref.sig.injection.select

        initialise.system
        SEQ
        IF
            head.manager
                commands.out ! initialise.system
        TRUE
        SKIP

        SEQ channels = 0 FOR num.local.magnet.controllers
            magnet.controller.commands[ channels ] ! initialise.system

        SEQ channels = 0 FOR num.local.mode.controllers
            mode.controller.commands[ channels ] ! initialise.system

        exception.manager.reset ! TRUE
    :

```

```

#USE "system.tsr"

PROC Exception.Report.Manager( VAL BOOL head.manager,
                               CHAN OF BOOL manager.reset,
                               CHAN OF exception.p exception.in,
                               []CHAN OF exception.p exceptions.in,
                               CHAN OF BOOL switch.pressed.in,
                               CHAN OF exception.p exception.out,
                               CHAN OF BOOL shutdown.request)

VAL num.exception.channels IS SIZE exceptions.in :

BOOL reset, send.report, report.received :

INT message.length, b.message.length :
[80]BYTE message :
PLACE message IN VECSPACE :
[80]BYTE b.message :
PLACE b.message IN VECSPACE :
BYTE index, b.index :
REAL32 value, b.value :
BOOL delevitate, b.delevitate :
BOOL switch.pressed :

CHAN OF exception.p exception.buffer :

SEQ
  report.received := FALSE
  send.report := TRUE
  PAR
    WHILE TRUE
      SEQ
        PRI ALT
          ALT channels = 0 FOR num.exception.channels
            exceptions.in[ channels ] ? message.length::message; index; value; delevitate
            report.received := TRUE
          exception.in ? message.length::message; index; value; delevitate
            report.received := TRUE
          switch.pressed.in ? delevitate
            SEQ
              message.length := 0
              report.received := TRUE
            manager.reset ? reset
            SEQ
              report.received := FALSE
              send.report := TRUE

          switch.pressed := report.received AND (message.length = 0)

        IF
          switch.pressed AND send.report
            SEQ
              exception.buffer ! message.length::message; index; value; delevitate
              report.received := FALSE
            report.received AND send.report
            SEQ
              exception.buffer ! message.length::message; index; value; delevitate
              send.report := FALSE
            TRUE
            SKIP

    WHILE TRUE
      SEQ
        exception.buffer ? b.message.length::b.message; b.index; b.value; b.delevitate
        IF
          head.manager AND b.delevitate
            shutdown.request ! TRUE
          TRUE
            SKIP
        exception.out ! b.message.length::b.message; b.index; b.value; b.delevitate

```

## E.2.5 Executive processes Library

```

#USE "system.tsr"

PROC Monitor.Data.Buffer( CHAN OF monitor.p monitor.data.in,
                        CHAN OF BOOL data.request.in,
                        CHAN OF monitor.p monitor.data.out,

                        CHAN OF data.buffer.p commands.and.params.in,
                        CHAN OF exception.p exception.report.out )

-- Monitor.Data.Buffer() receives all data signals from the control system for
-- each iteration of the loop. This data can be optionally stored at a
-- specified sampling rate and duration. The output data can then be either
-- from the on-line data or from that stored in the buffer.
--
-- This process uses no external variables and should be configured for
-- high priority operation.

BOOL logging, log.pending, data.complete, use.stored.data, request.data :

REAL32 time.stamp, sample.time, sample.interval, sample.duration :
[4][num.magnets]REAL32 magnet.data :
[7][num.modes]REAL32 mode.data :

VAL buffer.size IS 2000 :
INT write.index, read.index :

-- Place the large buffer arrays in slow off-processor memory --
[buffer.size]REAL32 buffered.time.stamp :
PLACE buffered.time.stamp IN VECSPACE :
[buffer.size][4][num.magnets]REAL32 buffered.magnet.data :
PLACE buffered.magnet.data IN VECSPACE :
[buffer.size][7][num.modes]REAL32 buffered.mode.data :
PLACE buffered.mode.data IN VECSPACE :

SEQ
  logging := FALSE
  log.pending := FALSE
  data.complete := FALSE

  -- Reset variable storage
  time.stamp := 0.0 (REAL32)
  SEQ var.index = 0 FOR 4
    SEQ magnet.index = 0 FOR num.magnets
      magnet.data[var.index][magnet.index] := 0.0 (REAL32)
  SEQ var.index = 0 FOR 7
    SEQ mode.index = 0 FOR num.modes
      mode.data[var.index][mode.index] := 0.0 (REAL32)

  WHILE TRUE
    PRI ALT
      monitor.data.in ? time.stamp; magnet.data; mode.data
      SEQ
        -- Log data into buffer when appropriate --
        logging := logging OR (log.pending AND (time.stamp = 0.0 (REAL32)))
        log.pending := log.pending AND (NOT logging)
        IF
          logging AND (time.stamp >= sample.time)
          SEQ
            write.index := write.index + 1
            buffered.time.stamp[write.index] := time.stamp
            buffered.mode.data[write.index] := mode.data
            buffered.magnet.data[write.index] := magnet.data
            data.complete := (write.index = (buffer.size-1)) OR
              (sample.time >= sample.duration)
            sample.time := sample.time + sample.interval
          logging
            data.complete := (time.stamp = 0.0 (REAL32))
          TRUE
            SKIP
        logging := logging AND (NOT data.complete)

      commands.and.params.in ? CASE
        data.buffer.select; use.stored.data -- Select output source
        SKIP
        data.buffer.params; sample.interval; sample.duration
        SKIP

```



```

data.buffer.log -- Start storing data to buffer
SEQ
  logging := FALSE
  log.pending := TRUE
  data.complete := FALSE
  sample.time := 0.0 (REAL32)
  write.index := -1
  read.index := -1

data.request.in ? request.data
IF
  use.stored.data AND (logging OR data.complete)
  SEQ
    read.index := (read.index + 1) REM (write.index + 1)
    monitor.data.out ! buffered.time.stamp[read.index];
                      buffered.magnet.data[read.index];
                      buffered.mode.data[read.index]
  TRUE
    monitor.data.out ! time.stamp; magnet.data; mode.data
:

#USE "system.tsr"
#USE  userio

PROC User.Interface( CHAN OF signal.gen.p  signal.gen.params.out, signal.gen.status.in,
                    CHAN OF controller.p  controller.params.out,
                    CHAN OF data.buffer.p  data.buffer.params.out,

                    CHAN OF INT  keyboard,
                    CHAN OF ANY  screen,

                    CHAN OF BOOL  data.request,
                    CHAN OF monitor.p  monitor.data.in,

                    CHAN OF exception.p  exception.reports.in )

-- User.Interface() provides the overall executive control of the suspension system.
-- A terminal can be connected (optically) to the vehicle to access a menu-driven
-- facility which permits levitation control as well as as modification of all
-- control system parameters. User.Interface() also provides data monitoring
-- facilities either asynchronously for fast sampling or synchronously to provide
-- real-time monitoring. The push button switch on the DAC card can also be used
-- to levitate and de-levitate the vehicle.

-- MENU MANIPULATION PROCEDURES --
PROC Menu.Title( VAL [] BYTE title )
-- Menu.Title() centres, underlines and displays the supplied text.
VAL offset IS (80 - (SIZE title)) / 2 :
SEQ
  goto.xy( screen, 0,0 )
  clear.eos( screen )
  goto.xy( screen, offset,0 )
  write.text.line( screen, title )
  goto.xy( screen, offset,1 )
  SEQ index = 1 FOR SIZE title
    write.char( screen, '~' )
  SEQ index = 1 FOR 3
    newline( screen )
:

PROC Menu.Line( VAL []BYTE option )
-- Menu.Line() offsets and displays the supplied text.
SEQ
  SEQ index = 1 FOR 20
    write.char( screen, ' ' )
  write.text.line( screen, option )
:

PROC Menu.Line.b( VAL []BYTE option, true.msg, false.msg, VAL BOOL value )
-- Menu.Line.b() offsets and displays the supplied option text.
-- It also uses the supplied Boolean value to selectively display a second
-- text message.
SEQ
  SEQ index = 1 FOR 20
    write.char( screen, ' ' )
  write.full.string( screen, option )
  IF
    (value = TRUE)

```

```

        write.text.line( screen, true.mesg )
        (value = FALSE)
        write.text.line( screen, false.mesg )
    :

PROC Menu.Line.r( VAL []BYTE option, units, VAL REAL32 value, VAL INT i,d )
-- Menu.Line.r() offsets and displays the supplied option text.
-- It also displays the supplied REAL32 value followed by the units text.
SEQ
SEQ index = 1 FOR 20
    write.char( screen, ' ' )
    write.full.string( screen, option )
    write.real32( screen, value, i,d )
    write.text.line( screen, units )
:

PROC Menu.Line.ra( VAL []BYTE option, units, VAL []REAL32 value,
                  VAL REAL32 divisor, VAL INT i,d )
-- Menu.Line.ra() offsets and displays the supplied option text.
-- It also displays the supplied []REAL32 values followed by the units text.
SEQ
SEQ index = 1 FOR 20
    write.char( screen, ' ' )
    write.full.string( screen, option )
    SEQ index = 0 FOR SIZE value
        SEQ
            write.real32( screen, value[index]/divisor, i,d )
            write.char( screen, ' ' )
        write.text.line( screen, units )
:

PROC Get.Option( INT char )
-- Get.Option() prompts the user for a single character input.
SEQ
write.full.string( screen, "*c*n          Select option: " )
keyboard ? char
char := (char /\ #DF)
:

PROC Get.Value.r( VAL []BYTE prompt, REAL32 new.value, VAL REAL32 factor )
-- Get.Value.r() prompts the user with the supplied prompt and then
-- inputs and scales returns a REAL32 value from the keyboard.
INT delimiter :
SEQ
write.text.line( screen, prompt )
write.full.string( screen, "          Enter new parameter value: " )
new.value := 0.0 (REAL32)
delimiter := INT ' '
read.echo.real32( keyboard, screen, new.value, delimiter )
new.value := new.value * factor
:

PROC Get.Value.ra( VAL []BYTE prompt, []REAL32 new.value, VAL REAL32 factor )
-- Get.Value.ra() prompts the user with the supplied prompt and then
-- inputs and scales returns []REAL32 values from the keyboard.
INT delimiter :
SEQ
write.text.line( screen, prompt )
write.full.string( screen, "          Enter new parameter values: " )
SEQ index = 0 FOR SIZE new.value
    SEQ
        new.value[index] := 0.0 (REAL32)
        delimiter := INT ' '
        read.echo.real32( keyboard, screen, new.value[index], delimiter )
        new.value[index] := new.value[index] * factor
:

-- VARIABLE DECLARATIONS TO HOLD COMPLETE SET OF SYSTEM PARAMETERS --

-- Reference signal generator variables --
REAL32 sample.interval, mean.gap :
BOOL    dynamic.ref.signal, sine.wave.ref.signal :
REAL32 ref.frequency, ref.amplitude :
[num.modes]REAL32 mean.gap.coeffs :
[num.modes]REAL32 pos.ref.coeffs :

-- Controller parameters --
INT control.mode :

[num.modes][num.magnets]REAL32 input.matrix :
```

```

[num.magnets][num.modes]REAL32 output.matrix :
[num.modes]REAL32 integral.T, stiffness, damping, massness :
REAL32 est.cutoff.Hz, traj.cutoff.Hz :
BOOL track.reference :

-- Data signal buffer parameters --
REAL32 buffer.interval, buffer.duration :
BOOL buffer.output :

#USE "Defaults.tsr"

PROC Initialise.Reference.Signal.Generator.Parameters ( )
-- This procedure initialises all parameters for the ref signal generator.
SEQ
sample.interval := default.sample.interval
mean.gap := default.mean.gap
dynamic.ref.signal := default.dynamic.ref.signal
sine.wave.ref.signal := default.sine.wave.ref.signal
track.reference := default.track.reference
IF
track.reference
ref.frequency := default.track.ref.frequency
NOT track.reference
ref.frequency := default.pos.ref.frequency
ref.amplitude := default.ref.amplitude
CASE control.mode
local
pos.ref.coeffs := default.local.ref.coeffs
vehicle
pos.ref.coeffs := default.vehicle.ref.coeffs
user
pos.ref.coeffs := default.user.ref.coeffs
:

PROC Reference.Signal.Generator.Menu ( )
-- This procedure enables interactive modification of the reference signal
-- generator parameters.
BOOL finished :
INT option :
SEQ
finished := FALSE
WHILE NOT finished
SEQ
Menu.Title( "MAGLEV VEHICLE SUSPENSION - Signal Generator Parameters" )

Menu.Line( "Reset all parameters to default values" )
newline( screen )
Menu.Line.r( "Sampling interval ( ", " ms )", sample.interval*kilo,3,2 )
Menu.Line.r( "Operating air gap ( ", " mm )", mean.gap*kilo,1,2 )
Menu.Line.b( "Dynamic reference signal ( ", "On )", "Off )", dynamic.ref.signal )
Menu.Line.b( "Waveform of dynamic reference signal ( ", "Sine )", "Square )",
sine.wave.ref.signal )
Menu.Line.b( "Track/Vehicle reference signal ( ", "Track )", "Vehicle )", track.reference
)

Menu.Line.r( "Frequency of reference signal ( ", " Hz )", ref.frequency,2,2 )
Menu.Line.r( "Amplitude of reference signal ( ", " mm )", ref.amplitude*kilo,2,2 )
Menu.Line.ra( "Mode distribution of reference ( ", " )", pos.ref.coeffs,one,1,1 )
newline( screen )
Menu.Line( "Quit this menu." )

Get.Option( option )
CASE BYTE option
'R'
Initialise.Reference.Signal.Generator.Parameters ( )
'S'
Get.Value.r( "Sampling interval", sample.interval, one/kilo )
'O'
Get.Value.r( "Air gap", mean.gap, one/kilo )
'D'
dynamic.ref.signal := NOT dynamic.ref.signal
'W'
sine.wave.ref.signal := NOT sine.wave.ref.signal
'T'
track.reference := NOT track.reference
'F'
Get.Value.r( "Reference frequency", ref.frequency, one )
'A'
Get.Value.r( "Reference amplitude", ref.amplitude, one/kilo )
'M'

```

```

        Get.Value.ra( "Factors for each mode reference", pos.ref.coeffs, one)
    'Q'
        finished := TRUE
    ELSE
        beep( screen )
    IF
        (sample.interval < 0.0001 (REAL32))
            sample.interval := 0.0001 (REAL32)
        (sample.interval > 0.99 (REAL32))
            sample.interval := 0.99 (REAL32)
    TRUE
    SKIP
:

PROC Initialise.Controller.Parameters( )
-- This procedure initialises all parameters for the mode and magnet controllers.
SEQ
CASE control.mode
    local
        SEQ
            input.matrix := local.matrix
            output.matrix := local.matrix
    vehicle
        SEQ
            input.matrix := veh.input.matrix
            output.matrix := veh.output.matrix
    user
        SEQ
            input.matrix := user.input.matrix
            output.matrix := user.output.matrix
est.cutoff.Hz := default.est.cutoff.Hz
traj.cutoff.Hz := default.traj.cutoff.Hz
CASE control.mode
    local
        SEQ
            integral.T := local.integral.T
            stiffness := local.stiffness
            damping := local.damping
            massness := local.massness
    vehicle
        SEQ
            integral.T := veh.integral.T
            stiffness := veh.stiffness
            damping := veh.damping
            massness := veh.massness
    user
        SEQ
            integral.T := user.integral.T
            stiffness := user.stiffness
            damping := user.damping
            massness := user.massness
-- Also set the mode reference coefficients for the ref signal generator --
CASE control.mode
    local
        pos.ref.coeffs := default.local.ref.coeffs
    vehicle
        pos.ref.coeffs := default.vehicle.ref.coeffs
    user
        pos.ref.coeffs := default.user.ref.coeffs
CASE control.mode
    local
        mean.gap.coeffs := default.local.gap.coeffs
    vehicle
        mean.gap.coeffs := default.vehicle.gap.coeffs
    user
        mean.gap.coeffs := default.user.gap.coeffs
:

PROC Controller.Menu( )
-- This procedure enables interactive modification of the mode and magnet
-- controller parameters.
BOOL finished :
INT option :
SEQ
    finished := FALSE
    WHILE NOT finished
        SEQ
            Menu.Title( "MAGLEV VEHICLE SUSPENSION - Controller Parameters" )

```

```

Menu.Line.b( "Local mode controller ", "- Selected", "", (control.mode=local) )
Menu.Line.b( "Vehicle mode controller ", "- Selected", "", (control.mode=vehicle) )
Menu.Line.b( "User defined controller ", "- Selected", "", (control.mode=user) )
newline( screen )
Menu.Line.r( "Estimation filter frequency ( ", " Hz)", est.cutoff.Hz,1,2)
Menu.Line.r( "Track trajectory filter frequency ( ", " Hz)", traj.cutoff.Hz,2,1 )
newline( screen )
Menu.Line( "Absolute Position Controller Parameters" )
Menu.Line.ra( "Integral time constant ( ", " s)", integral.T,one,1,1 )
Menu.Line.ra( "Stiffness ( ", " kg/mm)", stiffness,kilo.g,3,1 )
Menu.Line.ra( "Damping ( ", " kg/(mm/s)", damping,kilo.g,3,1 )
Menu.Line.ra( "Massness ( ", " kg)", massness,one,3,1 )
newline( screen )
Menu.Line( "Quit this menu." )

Get.Option( option )
CASE BYTE option
  'L','V','U'
  SEQ
    CASE BYTE option
      'L'
        control.mode := local
      'V'
        control.mode := vehicle
      'U'
        control.mode := user
    Initialise.Controller.Parameters( )
  'E'
    Get.Value.r( "Estimation filter frequency", est.cutoff.Hz, one)
  'T'
    Get.Value.r( "Trajectory filter frequency", traj.cutoff.Hz, one )
  'I'
    Get.Value.ra( "Integral action time constant", integral.T, one )
  'S'
    Get.Value.ra( "Stiffness", stiffness, kilo.g )
  'D'
    Get.Value.ra( "Damping", damping, kilo.g )
  'M'
    Get.Value.ra( "Massness", massness, one )
  'Q'
    finished := TRUE
  ELSE
    beep( screen )
:

PROC Initialise.Signal.Buffer.Parameters( )
-- This procedure initialises all parameters for the signal data buffer.
SEQ
  buffer.interval := default.buffer.interval
  buffer.duration := default.buffer.duration
  buffer.output := default.buffer.output
:

PROC Signal.Buffer.Menu( )
-- This procedure enables interactive modification of the parameters for the
-- signal data buffer.
BOOL finished :
INT option :
SEQ
  finished := FALSE
  WHILE NOT finished
    SEQ
      Menu.Title( "MAGLEV VEHICLE SUSPENSION - Signal Buffer Parameters" )

      Menu.Line( "Reset all parameters to default values" )
      newline( screen )
      Menu.Line.r( "Interval between buffer samples( ", " ms)", buffer.interval*kilo,2,1 )
      Menu.Line.r( "Duration (maximum) of buffer sampling( ", " s)", buffer.duration,2,1)
      newline( screen )
      Menu.Line( "Log signals into buffer now" )
      newline( screen )
      Menu.Line.b( "Select buffer output source ", "- stored data",
                  "- real-time data", buffer.output )

      newline( screen )
      Menu.Line( "Quit this menu." )

      Get.Option( option )
      CASE BYTE option
        'R'

```

```

        Initialise.Signal.Buffer.Parameters ( )
    'I'
        Get.Value.r( "Buffer interval", buffer.interval, one/kilo )
    'D'
        Get.Value.r( "Buffer duration", buffer.duration, one )
    'L'
        SEQ
            data.buffer.params.out ! data.buffer.params;  buffer.interval;
                                     buffer.duration
            data.buffer.params.out ! data.buffer.log
    'S'
        buffer.output := NOT buffer.output
    'Q'
        finished := TRUE
    ELSE
        beep( screen )
:

-- LOCAL VARIABLE DECLARATIONS FOR USER.INTERFACE() --

-- Menu control variables --
BOOL levitate, key.pressed :
INT option :

-- Exception report variables --
INT message.length :
[80]BYTE message :
BYTE index :
REAL32 value :
BOOL delevitate, switch.pressed :

-- Procedure code for User.Interface() --

#USE "Monitor.tsr"
SEQ
    control.mode := vehicle -- Select multi-variable vehicle control mode.

    Initialise.Signal.Buffer.Parameters( )
    Initialise.Controller.Parameters( )
    Initialise.Reference.Signal.Generator.Parameters( )

    controller.params.out ! initialise.system

    levitate := FALSE
    key.pressed := FALSE

    WHILE TRUE
        SEQ
            controller.params.out ! mode.control.params;  sample.interval; input.matrix;
                                     est.cutoff.Hz; traj.cutoff.Hz; integral.T; stiffness;
                                     damping; massness; control.mode; track.reference
            controller.params.out ! magnet.control.params;  sample.interval; output.matrix
            data.buffer.params.out ! data.buffer.params;  buffer.interval; buffer.duration
            data.buffer.params.out ! data.buffer.select;  buffer.output
            signal.gen.params.out ! signal.gen.params;  sample.interval; mean.gap;
                                     mean.gap.coeffs; dynamic.ref.signal; sine.wave.ref.signal;
                                     ref.frequency; ref.amplitude; pos.ref.coeffs

        PRI ALT
            keyboard ? option
            SEQ
                key.pressed := TRUE
                option := (option /\ #DF)
                CASE BYTE option
                    'L'
                        IF
                            NOT levitate
                                SEQ
                                    levitate := TRUE
                                    controller.params.out ! initialise.system
                                    signal.gen.params.out ! signal.gen.levitate;  levitate
                                TRUE
                            SKIP
                    'D'
                        SEQ
                            levitate := FALSE
                            signal.gen.params.out ! signal.gen.levitate;  levitate
                    'C'
                        Controller.Menu( )
                    'R'

```

```

        Reference.Signal.Generator.Menu( )
    'S'
        Signal.Buffer.Menu( )
    'M'
        Data.Monitor( data.request, monitor.data.in, keyboard, screen,
data.buffer.params.out )
        ELSE
            beep( screen )

        Menu.Title( "MAGLEV VEHICLE SUSPENSION CONTROL SYSTEM" )
        Menu.Line.b( "", "De-levitate vehicle.", "Levitate vehicle.", levitate )
        Menu.Line( "Controller parameters." )
        Menu.Line( "Reference signal parameters." )
        Menu.Line( "Signal buffer parameters." )
        Menu.Line( "Monitor controller signals." )
        write.full.string( screen, "*c*n          Select option: " )

signal.gen.status.in ? CASE signal.gen.levitated; levitate
controller.params.out ! initialise.system

exception.reports.in ? message.length::message; index; value; delevitate
SEQ
switch.pressed := (message.length = 0)
IF
    switch.pressed
    SEQ
        levitate := NOT levitate
        signal.gen.params.out ! signal.gen.levitate; levitate
    NOT switch.pressed
    SEQ
        IF
            NOT key.pressed
            keyboard ? option
            TRUE
                newline( screen )
            newline( screen )
            write.len.string( screen, message.length, message )
            write.real32( screen, value, 3,3 )
            newline( screen )
            newline( screen )
            write.full.string( screen, "*c*n          Select option: " )

```

:

## E.2.6 Default parameters Library for Executive

```

-- DEFAULT VALUES FOR ALL CONTROL SYSTEM PARAMETERS --

-- Useful constants (to improve readability) --
VAL zero IS 0.0 (REAL32) :
VAL qrt IS 0.25 (REAL32) :
VAL half IS 0.5 (REAL32) :
VAL one IS 1.0 (REAL32) :
VAL kilo IS 1000.0 (REAL32) :
VAL g IS 9.81 (REAL32) :
VAL kilo.g IS kilo * g :

-- Default parameter values for the Reference Signal Generator --
VAL default.sample.interval IS 0.00125 (REAL32) : -- 1.25 ms
VAL default.mean.gap IS 0.003 (REAL32) : -- 3.0 mm
VAL default.local.gap.coeffs IS [ one, one, one, one ] :
VAL default.user.gap.coeffs IS [ one, one, one, zero ] :
VAL default.vehicle.gap.coeffs IS [ one, zero, zero, zero ] :

VAL default.dynamic.ref.signal IS FALSE : -- constant gap ref
VAL default.sine.wave.ref.signal IS TRUE :
VAL default.track.reference IS TRUE :

VAL default.pos.ref.frequency IS 10.0 (REAL32) : -- 10 Hz
VAL default.track.ref.frequency IS 0.5 (REAL32) : -- 0.5 Hz
VAL default.ref.amplitude IS 0.001 (REAL32) : -- 1 mm pk-pk

VAL default.local.ref.coeffs IS [ one, one, one, one ] :
VAL default.user.ref.coeffs IS [ one, one, one, zero ] :
VAL default.vehicle.ref.coeffs IS [ one, zero, zero, zero ] :

-- Default parameter values for the Mode & Magnet Controllers --
VAL local.matrix IS [ [ one, zero, zero, zero ],
                    [ zero, one, zero, zero ],
                    [ zero, zero, one, zero ],
                    [ zero, zero, zero, one ] ] :

VAL veh.input.matrix IS [ [ qrt, qrt, qrt, qrt ],
                        [ qrt, -qrt, -qrt, qrt ],
                        [ qrt, qrt, -qrt, -qrt ],
                        [ qrt, -qrt, qrt, -qrt ] ] :

VAL veh.output.matrix IS [ [ qrt, qrt, qrt, qrt ],
                          [ qrt, -qrt, qrt, -qrt ],
                          [ qrt, -qrt, -qrt, qrt ],
                          [ qrt, qrt, -qrt, -qrt ] ] :

VAL user.input.matrix IS [ [ one, zero, zero, zero ],
                          [ zero, one, zero, zero ],
                          [ zero, zero, half, half ],
                          [ zero, zero, zero, zero ] ] :

VAL user.output.matrix IS [ [ one, zero, zero, zero ],
                           [ zero, one, zero, zero ],
                           [ zero, zero, half, zero ],
                           [ zero, zero, half, zero ] ] :

VAL REAL32 default.est.cutoff.Hz IS 0.1 (REAL32) :
VAL REAL32 default.traj.cutoff.Hz IS 4.0 (REAL32) :

VAL veh.integral.T IS [ one, one, one, zero ] : -- seconds
VAL veh.stiffness IS
  [ 100.0E+4 (REAL32), 100.0E+4 (REAL32), 100.0E+4 (REAL32), zero ] : -- N/m
VAL veh.damping IS
  [ 2.6E+4 (REAL32), 2.6E+4 (REAL32), 2.6E+4 (REAL32), 2.6E+4 (REAL32) ] : -- N/m/s
VAL veh.massness IS
  [ 60.0 (REAL32), 60.0 (REAL32), 60.0 (REAL32), 60.0 (REAL32) ] : -- kg

VAL local.integral.T IS [ one, one, one, one ] : -- seconds
VAL local.stiffness IS
  [ 25.0E+4 (REAL32), 25.0E+4 (REAL32), 25.0E+4 (REAL32), 25.0E+4 (REAL32) ] : -- N/m
VAL local.damping IS
  [ 0.65E+4 (REAL32), 0.65E+4 (REAL32), 0.65E+4 (REAL32), 0.65E+4 (REAL32) ] : -- N/m/s
VAL local.massness IS
  [ 15.0 (REAL32), 15.0 (REAL32), 15.0 (REAL32), 15.0 (REAL32) ] : -- kg

```



```

VAL user.integral.T IS [ one, one, one, zero ] : -- seconds
VAL user.stiffness IS
  [ 25.0E+4 (REAL32), 25.0E+4 (REAL32), 50.0E+4 (REAL32), zero ] : -- N/m
VAL user.damping IS
  [ 0.65E+4 (REAL32), 0.65E+4 (REAL32), 1.3E+4 (REAL32), zero ] : -- N/m/s
VAL user.massness IS
  [ 15.0 (REAL32), 15.0 (REAL32), 30.0 (REAL32), zero ] : -- kg

-- Default parameter values for the Signal Buffer --
VAL default.buffer.interval IS 0.005 (REAL32) : -- 5 ms
VAL default.buffer.duration IS 99.000 (REAL32) : -- 99 s
VAL default.buffer.output IS FALSE : -- Select on-line signals

```

## E.2.7 Data Monitor process Library for Executive

```

#USE "system.tsr"
#USE userio
#USE strings

PROC Data.Monitor( CHAN OF BOOL data.request.out,
                  CHAN OF monitor.p monitored.data.in,

                  CHAN OF INT keyboard,
                  CHAN OF ANY screen,

                  CHAN OF data.buffer.p data.buffer.params.out )

-- Data.Monitor receives data from the control system via the data buffer.
-- Data selected by the keyboard is the sent to the screen. Each data item
-- is toggled on/off using its initial letter. 'B' toggles bar graph/tabular
-- output, and 'W' causes the output to wait briefly to allow the Network
-- Monitor EXE program to break free from the data stream, thus allowing the
-- Data Logger EXE program to be run to log data to disc.

-- Display variable tables etc. --
VAL num.vars IS 12 :

VAL one IS 1.0 (REAL32) :
VAL ten IS 10.0 (REAL32) :
VAL twenty IS 20.0 (REAL32) :
VAL kilo IS 1000.0 (REAL32) :

VAL [num.vars][2]BYTE var.name IS
  [ "T=", "G=", "A=", "F=", "I=", "r=", "g=", "a=", "v=", "p=", "t=", "f=" ] :
VAL [num.vars]REAL32 var.scaler IS
  [ one, kilo, one, one, kilo, kilo, one, one, kilo, kilo, one ] :
VAL [num.vars]REAL32 var.FSD IS
  [ one, ten, one, kilo, twenty, ten, ten, one, one, ten, ten, kilo ] :
VAL [num.vars]INT var.bp IS
  [ 2, 1, 1, 4, 2, 1, 1, 1, 1, 1, 1, 4 ] :
VAL [num.vars]INT var.ap IS
  [ 3, 3, 3, 1, 2, 1, 3, 3, 3, 3, 3, 1 ] :
VAL [num.vars]BOOL unipolar.var IS
  [ TRUE, TRUE, FALSE, TRUE, TRUE, TRUE, FALSE, FALSE, FALSE, FALSE, FALSE, TRUE ] :
VAL [num.vars]BOOL initial.display.vars IS
  [ TRUE, TRUE, FALSE, FALSE, FALSE, TRUE, FALSE, FALSE, FALSE, FALSE, FALSE, FALSE ] :

[num.vars]BOOL display.on :
[num.vars][4]REAL32 display.table :

[80]BYTE display.line :
[200]BYTE string :
INT char, string.index, line.index :
REAL32 time :
BOOL bar.display.selected, buffer.output, finished :

SEQ
  display.on := initial.display.vars
  bar.display.selected := TRUE
  buffer.output := FALSE
  finished := FALSE

```

```

WHILE NOT finished
SEQ
  PRI ALT
  keyboard ? char
  SEQ
    CASE BYTE char
      'W','w'
        SEQ index1 = 1 FOR 3000
        SEQ index2 = 1 FOR 100
        SKIP
      'B','b'
        bar.display.selected := NOT bar.display.selected
      'L','l'
        data.buffer.params.out ! data.buffer.log
      'S','s'
        SEQ
          buffer.output := NOT buffer.output
          data.buffer.params.out ! data.buffer.select; buffer.output
      'Q','q'
        finished := TRUE
    ELSE
      SEQ index = 1 FOR num.vars - 1
      IF
        ((BYTE char) = var.name[index][0])
        display.on[index] := NOT display.on[index]
      TRUE
      SKIP

  TRUE & SKIP
  SKIP

-- Get some data from the controller --
data.request.out ! TRUE
monitored.data.in ? time; -- reference signal time stamp
                        [display.table FROM 1 FOR 4]; -- magnet signals
                        [display.table FROM 5 FOR 7] -- mode signals

IF
  (time = 0.0 (REAL32))
  write.endstream( screen )
TRUE
SKIP

-- Scale the variables before display --
SEQ var.index = 1 FOR num.vars - 1
IF
  display.on[ var.index ]
  SEQ index = 0 FOR 4
    display.table[var.index][index] := var.scaler[var.index] *
    display.table[var.index][index]
  TRUE
  SKIP

-- Display value of each selected variable --
IF
  bar.display.selected
  SEQ
    goto.xy( screen, 0, 24 )
    clear.eol( screen )
  TRUE
  SKIP

string[0] := '*c'
string[1] := '*n'
string.index := 2

-- Copy time stamp to display string --
append.text( string.index, string, var.name[0])
append.real32( string.index, string, time, var.bp[0], var.ap[0] )
string[ string.index ] := ' '
string.index := string.index + 1

-- Copy other required signals --
SEQ var.index = 1 FOR num.vars-1
IF
  display.on[ var.index ]
  SEQ
    append.text( string.index, string, var.name[ var.index ] )
    SEQ index = 0 FOR 4
      SEQ
        append.real32( string.index, string, display.table[var.index][index],

```

```

                var.bp[var.index], var.ap[var.index] )
                string[ string.index ] := ' '
                string.index := string.index + 1
        TRUE
        SKIP
write.len.string( screen, string.index, string )

IF
bar.display.selected
SEQ -- Display line graph for each selected variable --
SEQ index = 0 FOR SIZE display.line
    display.line[ index ] := ' '
SEQ index = 1 FOR 9
    display.line[ index * 8 ] := '.'
display.line[ 0 ] := '|'
display.line[ 40 ] := '|'

SEQ var.index = 1 FOR num.vars - 1 -- exclude time --
SEQ index = 0 FOR 4
    IF
        display.on[ var.index ]
        SEQ
            line.index := INT ROUND ((80.0 (REAL32) * display.table[var.index][index])
                / var.FSD[var.index])
        IF
            NOT unipolar.var[ var.index ]
                line.index := line.index + 40
            TRUE
            SKIP
        IF
            (line.index > 79)
                line.index := 79
            (line.index < 0)
                line.index := 0
            TRUE
            SKIP
        display.line[line.index] := var.name[var.index][0]
        IF
            (display.line[line.index] <> 'r')
                display.line[ line.index ] := BYTE (index + 49)
            TRUE
            SKIP
        TRUE
        SKIP
    goto.xy( screen, 0, 23 )
    write.full.string( screen, display.line )
TRUE
SKIP
:

```

### E.3 Single magnet suspension controller

```

PROC Maglev.Controller( CHAN OF INT keyboard,
                       CHAN OF ANY screen,
                       CHAN OF INT16 ADC.in, ADC.out,
                       DAC.in, DAC.out )

#####

Single Magnet (Cantilever) Controller

Features: - Track trajectory filter
          - Absolute position controller (4 term)
          - Full non-linear magnet force model for current calculation
          - Real time data monitoring and logging

Author: Neil McLagan
Version 1.0
Last modified: 24-1-91

All variables are in elementary units (eg. secs, metres, Hz, metres/sec)
unless the variable name is post-fixed with an alternative, eg. airgap.mm
Airgap is positive, velocity and acceleration have same direction as airgap.

#####

#USE "Protocols.tsr"
#USE userio

-----

PROC Set.default.parameters(REAL32 integral.time, stiffness, damping, massness,
                           sampling.period, estim.cutoff.Hz, track.cutoff.Hz,
                           mass, operating.airgap,
                           airgap.frequency, airgap.amplitude, logging.period,
                           BYTE airgap.waveform )

-- Set default values for controller parameters --

SEQ
-- Default ride characteristics --
integral.time := 1.0 (REAL32) -- seconds
stiffness := 250000.0 (REAL32) -- Newtons/metre
damping := 6500.0 (REAL32) -- Newtons/(metre/second)
massness := 15.0 (REAL32) -- Newtons/(metre/second^2) = Kilogrammes

-- Initialise sampling period and filter cut-off frequencies --
sampling.period := 0.0005 (REAL32)
estim.cutoff.Hz := 0.1 (REAL32)
track.cutoff.Hz := 4.0 (REAL32)

-- Default mass --
mass := 13.0 (REAL32)

-- Default airgap reference characteristics --
operating.airgap := 0.003 (REAL32) -- 3 mm --
airgap.frequency := 0.05 (REAL32) -- 0.05 Hz --
airgap.amplitude := 0.001 (REAL32) -- 1 mm --
logging.period := 0.020 (REAL32) -- 20 ms --
airgap.waveform := 'C' -- Constant airgap --

:

-----

#USE "Protocols.tsr"

PROC Read.ADC( CHAN OF INT16 ADC.in, ADC.out,
              VAL INT mux.channel,
              REAL32 adc )

-- Read.ADC requests an ADC conversion for each selected channel.
-- It then scales the values appropriately before outputting them.

INT16 adc.value :
REAL32 adc.volts, sensor.gap, magnet.gap :

VAL REAL32 metres.per.volt IS 0.00125 (REAL32) :

```

```

VAL REAL32 sensor.offset IS 0.003500 (REAL32) :
VAL REAL32 magnet.offset IS 0.003740 (REAL32) :
VAL REAL32 magnet.sensor.length.ratio IS 1.446 (REAL32) :

SEQ
  ADC.out ! INT16 mux.channel
  ADC.in ? adc.value

  adc.volts := (REAL32 ROUND adc.value) / 6553.6(REAL32) -- convert to volts

  IF
    (mux.channel = 1) -- airgap channel request
    SEQ
      sensor.gap := (adc.volts * metres.per.volt) + sensor.offset
      magnet.gap := (sensor.gap - magnet.offset) * magnet.sensor.length.ratio
      adc := magnet.gap

    (mux.channel = 16) -- acceleration channel request
    SEQ
      adc := -(adc.volts / 5.0(REAL32)) -- convert to g's
      adc := adc * 9.81(REAL32) -- convert to m/s/s

:

-----

PROC Write.DAC( CHAN OF INT16 DAC.in, DAC.out,
               VAL REAL32 current.demand )

-- Write.DAC scales the requested current drive and sends it to the DAC.

VAL min.current IS 0.0 (REAL32) :
VAL max.current IS 19.9 (REAL32) :
REAL32 current :

SEQ
  current := current.demand
  IF
    current > max.current
      current := max.current
    current < min.current
      current := min.current
  TRUE
  SKIP

  DAC.out ! INT16 ROUND( current * 204.8(REAL32) )

:

-----

VAL num.airgap.chans IS 3 :
VAL num.acc.chans IS 2 :

PROC Interface.to.outside.world( CHAN OF INT16 ADC.in, ADC.out,
                                DAC.in, DAC.out,
                                CHAN OF control.p trigger,
                                CHAN OF data.p current,
                                [num.airgap.chans] CHAN OF data.p airgap.chan,
                                [num.acc.chans] CHAN OF data.p acc.chan,
                                CHAN OF control.p cycle.finished,
                                CHAN OF exception.p exception )

-- Interface.to.outside.world communicates the current demands and
-- sensor values to and from the DAC and ADC drivers.

-- A-D converter sensor addresses --
VAL acc.sensor IS 16 :
VAL airgap.sensor IS 1 :

BOOL final.trigger, final.current, start.converting :
REAL32 acc, airgap, current.demand :

SEQ
  final.current := FALSE
  WHILE NOT final.current
    ALT
      trigger ? final.trigger; start.converting
    SEQ
      -- Read in acceleration --

```

```

Read.ADC( ADC.in, ADC.out, acc.sensor, acc )
PAR i = 0 FOR num.acc.chans
  acc.chan[i] ! final.trigger; acc

  -- Read in position --
Read.ADC( ADC.in, ADC.out, airgap.sensor, airgap )
PAR i = 0 FOR num.airgap.chans
  airgap.chan[i] ! final.trigger; airgap

-- Output current demand to magnet current amplifier --
current ? final.current; current.demand
SEQ
  IF
    final.current
    Write.DAC( DAC.in, DAC.out, 0.0 (REAL32) )
    TRUE
    Write.DAC( DAC.in, DAC.out, current.demand )
  cycle.finished ! final.current; TRUE
:

-----
#USE "Protocols.tsr"
#USE dblmath

VAL num.force.chans IS 2 :
VAL num.velocity.chans IS 1 :

PROC Calculate.magnet.force( CHAN OF data.p airgap.in, airgap.ref.in, acc.in,
  [num.force.chans] CHAN OF data.p force.out,
  [num.velocity.chans] CHAN OF data.p velocity.out,
  CHAN OF exception.p exception.out,
  VAL REAL32 integral.time, stiffness, damping, massness,
  mass,
  sampling.period,
  est.cutoff.Hz, track.cutoff.Hz )

-- Calculate.magnet.force receives airgap and acceleration signals and performs
-- the functions of track trajectory filter and absolute position control.

VAL pi IS 3.1415926 (REAL64) :
VAL two.pi IS 2.0 (REAL64) * pi :
VAL gravity.acc IS 9.81 (REAL32) :

VAL int.force.limit IS 500.0 (REAL32) : -- 500 Newton integral limit
VAL vel.limit IS 0.2 (REAL32) : -- 0.2 mm/ms velocity limit --
VAL [] BYTE warning.message IS "Warning: Excessive velocity, V = " :

BOOL final.airgap, final.airgap.ref, final.acc, final.force :

REAL64 est.input.factor, est.decay.factor :
REAL64 track.input.factor, track.decay.factor :

REAL32 airgap, airgap.ref, acc.meas :
REAL64 acc.meas.r64, acc.lp, acc.hp, vel.hp, pos.hp, pos.error :
REAL64 track.pos, track.pos.fl, track.pos.f2, track.trajectory :
REAL32 acc.feedback, vel.feedback, pos.feedback, int.feedback :
REAL32 force.demand, vel.r32 :

SEQ
  -- Set filter factors --
  est.decay.factor := Dexp( (- two.pi) * (REAL64 (est.cutoff.Hz * sampling.period)) )
  est.input.factor := 1.0 (REAL64) - est.decay.factor

  track.decay.factor := Dexp( (- two.pi) * (REAL64 (track.cutoff.Hz * sampling.period)) )
  track.input.factor := 1.0 (REAL64) - track.decay.factor

  -- Initialise filters and integrators --
  PAR
    airgap.in ? final.airgap; airgap
    airgap.ref.in ? final.airgap.ref; airgap.ref
    acc.in ? final.acc; acc.meas

  final.force := (final.airgap AND (final.airgap.ref AND final.acc))
  PAR
    PAR i = 0 FOR num.force.chans
      force.out[i] ! final.force; 0.0 (REAL32)
    PAR i = 0 FOR num.velocity.chans
      velocity.out[i] ! final.force; 0.0 (REAL32)

  acc.lp := 0.0 (REAL64)

```

```

vel.hp := 0.0 (REAL64)
pos.hp := 0.0 (REAL64)

track.pos := REAL64 (airgap.ref - airgap)
track.pos.f1 := track.pos
track.pos.f2 := track.pos.f1

int.feedback := 0.0 (REAL32)

WHILE NOT final.force
  SEQ
    PAR
      -- Input the airgap and airgap reference --
      airgap.in ? final.airgap; airgap
      airgap.ref.in ? final.airgap.ref; airgap.ref

    SEQ
      -- Input the (high pass filtered) acceleration --
      acc.in ? final.acc; acc.meas

      -- Estimate the absolute acceleration --
      acc.meas.r64 := REAL64 acc.meas
      acc.lp := (acc.lp * est.decay.factor) + (acc.meas.r64 * est.input.factor)
      acc.hp := acc.meas.r64 - acc.lp

      -- Estimate the absolute velocity and position --
      vel.hp := (vel.hp * est.decay.factor) + (acc.hp * (REAL64 sampling.period))
      pos.hp := (pos.hp * est.decay.factor) + (vel.hp * (REAL64 sampling.period))

      -- Estimate the absolute track position --
      track.pos := (REAL64 (airgap.ref - airgap)) + pos.hp

      -- and filter to form the track trajectory --
      track.pos.f1 := (track.pos.f1*track.decay.factor) + (track.pos*track.input.factor)
      track.pos.f2 := (track.pos.f2*track.decay.factor) + (track.pos.f1*track.input.factor)
      track.trajectory := track.pos.f2

      -- Calculate the absolute position error --
      pos.error := (pos.hp - track.trajectory)

      -- Calculate the feedback components --
      acc.feedback := massness * (REAL32 ROUND acc.hp)
      vel.feedback := damping * (REAL32 ROUND vel.hp)
      pos.feedback := stiffness * (REAL32 ROUND pos.error)
    IF
      (int.feedback < (-int.force.limit))
        int.feedback := -int.force.limit
      (int.feedback > int.force.limit)
        int.feedback := int.force.limit
      (integral.time > 0.0 (REAL32) )
        int.feedback := int.feedback +
          ( ((airgap-airgap.ref)*sampling.period) * (stiffness/integral.time) )
    TRUE
      int.feedback := 0.0 (REAL32)

      -- Total the force requirement (and account for mass) --
      force.demand := ( (int.feedback + pos.feedback) +
        (vel.feedback + acc.feedback) ) + (mass * gravity.acc)

      -- Output force demand & velocity --
      final.force := (final.airgap AND (final.airgap.ref AND final.acc))
      vel.r32 := REAL32 ROUND vel.hp
    PAR
      PAR i = 0 FOR num.force.chans
        force.out[i] ! final.force; force.demand
      PAR i = 0 FOR num.velocity.chans
        velocity.out[i] ! final.force; vel.r32

      -- Check velocity signal magnitude --
    IF
      (vel.r32 < (-vel.limit)) OR (vel.r32 > vel.limit)
        exception.out ! SIZE warning.message::warning.message; vel.r32
    TRUE
      SKIP

```

:

```

-----
#USE "Protocols.tsr"
#USE snglmath

VAL num.current.chans IS 2 :

PROC Calculate.magnet.current( CHAN OF data.p airgap.in,
                               force.demand.in,
                               [num.current.chans] CHAN OF data.p current.required.out,
                               CHAN OF exception.p exception.out,
                               VAL REAL32 sampling.period )

-- Calculate.magnet.current uses the nonlinear magnet force model to determine
-- the required current for the demanded force at the present airgap.

-- Worldly constants --
VAL pi IS 3.1415926 (REAL32) :
VAL mu.air IS 1.2566E-6 (REAL32) : -- Permeability of free space
-- These are used to make the equations more readable --
VAL zero IS 0.0 (REAL32) :
VAL one IS 1.0 (REAL32) :
VAL two IS 2.0 (REAL32) :
VAL four IS 4.0 (REAL32) :

-- Electromagnet parameters --
VAL y IS 0.0015 (REAL32) : -- Lateral offset between magnet & track poles
VAL l IS 0.200 (REAL32) : -- Magnet length
VAL w IS 0.033 (REAL32) : -- Width between the magnet pole pieces
VAL h IS 0.063 (REAL32) : -- Height of the magnet pole pieces
VAL t IS 0.030 (REAL32) : -- Width between the track pole pieces
VAL p IS 0.0095 (REAL32) : -- Width of the pole pieces

VAL N.coils IS 274.0 (REAL32) : -- Number of coil turns
VAL min.current IS 0.0 (REAL32) : -- Impose current limit
VAL max.current IS 20.0 (REAL32) : -- Impose current limit
VAL mu.iron IS 2000.0 (REAL32) : -- Maximum permeability of the core material
VAL flux.roll.start IS 1.0 (REAL32) : -- Start of permeability roll-off (/Tesla)
VAL flux.roll.stop IS 1.7 (REAL32) : -- End of permeability roll-off (/Tesla)

VAL T.eddy IS 0.0015 (REAL32) : -- Target eddy current time constant
VAL N.lead.lag IS 3.0 (REAL32) : -- Lead lag ratio to achieve the above

-- Nonlinear magnet model variables --
REAL32 T.lead.lag, lead.lag.input.factor, lead.lag.decay.factor :
REAL32 flux.low.pass, flux.lead.lag :
REAL32 R.track, R.leakage, R.airgap, R.magnet :
REAL32 force.demand, airgap, force.per.pole :
REAL32 airgap.flux, flux.squared, leakage.flux, magnet.flux :
REAL32 flux.density, mu.magnet :
REAL32 airgaps.plus.track.mmf, magnet.mmf :
REAL32 current.demand :

BOOL final.airgap, final.force, final.output :

SEQ
-- Determine lead lag compensator coefficients and initialise --
IF
  (T.eddy > sampling.period)
  T.lead.lag := T.eddy
  TRUE
  T.lead.lag := sampling.period

lead.lag.decay.factor := exp( - (sampling.period / T.eddy) )
lead.lag.input.factor := one - lead.lag.decay.factor
flux.low.pass := zero

-- Calculate the track and leakage reluctances --
R.track := ( t + (four*p) ) / ( (mu.iron*mu.air) * (l*p) )
R.leakage := w / ( mu.air * ( 1+((two*w)/pi) ) * ((h/two)+(w/pi) ) )

final.output := FALSE
WHILE NOT final.output
  SEQ
  PAR
    force.demand.in ? final.force; force.demand
    airgap.in ? final.airgap; airgap

  IF
    (force.demand < zero)
    force.demand := zero

```



```

TRUE
SKIP

-- Calculate airgap reluctance --
R.airgap := airgap / ( (mu.air*1) * ( p + ((two*airgap)/pi) ) )

-- Calculate the gross force per pole --
force.per.pole := force.demand /
  ( two * ( one - ( (y*y)/airgap) / (airgap+((pi*p)/two)) ) )

-- Calculate the required airgap flux --
flux.squared := force.per.pole * ( (two*airgap) / R.airgap )
IF
  (flux.squared > zero)
    airgap.flux := SQRT( flux.squared )
  TRUE
    airgap.flux := zero

-- Calculate the mmf required to overcome the airgap and track reluctances
airgaps.plus.track.mmf := airgap.flux * ( (two*R.airgap) + R.track )

-- Calculate the consequential leakage flux --
leakage.flux := airgaps.plus.track.mmf / R.leakage

-- Calculate the resulting electromagnet flux --
magnet.flux := airgap.flux + leakage.flux

-- Apply lead lag compensation teh the magnet flux demand --
flux.low.pass := (flux.low.pass * lead.lag.decay.factor) +
  (magnet.flux * lead.lag.input.factor)
flux.lead.lag := (N.lead.lag * magnet.flux) - ( (N.lead.lag-one) * flux.low.pass )

-- Calculate the magnet reluctance at this flux level --
flux.density := magnet.flux / (1 * p)
IF
  (flux.density < flux.roll.start)
    mu.magnet := mu.iron
  (flux.density < flux.roll.stop)
    mu.magnet := mu.iron * ( 1.1(REAL32) - ( (flux.density - flux.roll.start) /
      (flux.roll.stop - flux.roll.start) ) )
  TRUE
    mu.magnet := mu.iron * 0.1(REAL32)
R.magnet := ( (two*h) + (w+(two*p)) ) / ( (mu.air*mu.magnet) * (1*p) )

-- Calculate the mmf required to overcome the magnet reluctance --
magnet.mmf := flux.lead.lag * R.magnet

-- Finally, calculate the current required to produce the total mmf --
current.demand := (airgaps.plus.track.mmf + magnet.mmf) / N.coils
IF
  (current.demand > max.current)
    current.demand := max.current
  (current.demand < min.current)
    current.demand := min.current
  TRUE
    SKIP

final.output := (final.airgap AND final.force)
PAR i = 0 FOR num.current.chans
  current.required.out[i] ! final.output; current.demand
:

```

```

-----
#USE "Protocols.tsr"

PROC Handle.exceptions( [] CHAN OF exception.p exceptions.in,
                       CHAN OF BOOL stop.system.out,
                       [] BYTE message,
                       INT message.length,
                       REAL32 message.value )

-- Handle.exceptions initiates a controlled system shutdown upon receiving
-- any exception message (including a user requested shutdown).

VAL number.of.error.channels IS SIZE exceptions.in :
VAL terminate IS 0 :

[80] BYTE ignore.message :
INT ignore.length :
REAL32 ignore.value :

BOOL finished :

SEQ
-- Get first exception from the system --
ALT i = 0 FOR number.of.error.channels
  exceptions.in[i] ? message.length::message; message.value
  SKIP

finished := FALSE
PAR
-- Instruct system to shut down --
stop.system.out ! TRUE

-- Accept (but ignore) any further exceptions --
WHILE NOT finished
  ALT i = 0 FOR number.of.error.channels
    exceptions.in[i] ? ignore.length::ignore.message; ignore.value
    finished := (i = terminate)
:

```

```

-----
#USE "Protocols.tsr"

PROC Data.Buffer( CHAN OF data.p v1.in,v1.out, v2.in,v2.out, v3.in,v3.out,
                 v4.in,v4.out, v5.in,v5.out, v6.in,v6.out,
                 CHAN OF BOOL output.required )

-- Data.Buffer buffers data between the control system and the data
-- monitoring system, allowing them to run asynchronously.

REAL32 v1.data, v2.data, v3.data, v4.data, v5.data, v6.data :
BOOL v1.finished, v2.finished, v3.finished, v4.finished, v4.finished,
v5.finished, v6.finished :

BOOL ready, output.notified:

SEQ
v1.finished := FALSE
output.notified := FALSE

PAR
WHILE NOT (v1.finished AND output.notified)
-- Continuously read in all variables --
PRI ALT
  output.required ? ready
  PAR
    v1.out ! v1.finished; v1.data
    v2.out ! v2.finished; v2.data
    v3.out ! v3.finished; v3.data
    v4.out ! v4.finished; v4.data
    v5.out ! v5.finished; v5.data
    v6.out ! v6.finished; v6.data
    output.notified := v1.finished

  NOT v1.finished & SKIP
  PAR
    v1.in ? v1.finished; v1.data
    v2.in ? v2.finished; v2.data
    v3.in ? v3.finished; v3.data
    v4.in ? v4.finished; v4.data
    v5.in ? v5.finished; v5.data

```

```

v6.in ? v6.finished; v6.data
:

-----
#USE "Protocols.tsr"
#USE userio
#USE strings

PROC Data.Monitor( CHAN OF data.p gap.in, vel.in, acc.in,
                  force.in, current.in, gap.ref.in,
                  CHAN OF BOOL data.input.trigger,
                  CHAN OF exception.p exception.out,
                  CHAN OF INT keyboard,
                  CHAN OF ANY screen,
                  VAL REAL32 logging.period )

-- Data.Monitor receives data from the control system via the data buffer.
-- Data selected by the keyboard is sent to the screen. Each data item
-- is toggled on/off using its initial letter. 'T' toggles tabular/graph
-- output, and 'P' causes the output to pause briefly to allow the Network
-- Monitor EXE program to break free from the data stream, thus allowing the
-- Data Logger EXE program to be run to log data to disc.

INT char :
BYTE option :

BOOL final.gap, final.vel, final.acc,
      final.force, final.current, final.gap.ref,
      finished :

-- Display variable tables etc. --
VAL num.vars IS 7 :

VAL [num.vars] [2] BYTE var.name IS
[ "T=", "R=", "G=", "V=", "A=", "I=", "F=" ] :
VAL [num.vars] INT var.scaler IS
[ 1, 1000, 1000, 1, 1, 1, 1 ] :
VAL [num.vars] INT var.FSD IS
[ 1, 10, 10, 1, 1, 20, 1000 ] :
VAL [num.vars] INT var.bp IS
[ 2, 1, 1, 1, 1, 2, 4 ] :
VAL [num.vars] INT var.ap IS
[ 3, 1, 3, 3, 3, 2, 1 ] :
VAL [num.vars] BOOL initial.display.vars IS
[ TRUE, TRUE, TRUE, FALSE, FALSE, TRUE, TRUE ] :

[num.vars] BOOL display.on :
[num.vars] REAL32 display.table :

VAL ticks.per.second IS 15625.0 (REAL32) :
TIMER clock :
[80] BYTE display.line :
INT display.time.interval, display.time, time, last.time, line.index :
REAL32 time.interval, real.time :
REAL32 gap.ref, last.gap.ref :
BOOL bar.display.selected :

INT string.index :
[200] BYTE string :

SEQ
display.time.interval := INT TRUNC ( logging.period * ticks.per.second )
display.on := initial.display.vars

SEQ var.index = 0 FOR num.vars
display.table[ var.index ] := 0.0 (REAL32)

bar.display.selected := TRUE
finished := FALSE
clock ? time
clock ? display.time
real.time := 0.0 (REAL32)
last.gap.ref := 0.1 (REAL32)

WHILE NOT finished
SEQ
PRI ALT
keyboard ? char
SEQ
option := BYTE (char /\ #DF)

```

```

IF
  (option = 'L')
    write.endstream( screen )
  (option = 'P')
    SEQ index1 = 1 FOR 30000
      SEQ index2 = 1 FOR 100
        SKIP
  (option = 'Q')
    exception.out ! 0::""; 0.0 (REAL32)
  (option = 'T')
    bar.display.selected := NOT bar.display.selected
TRUE
  SEQ index = 1 FOR num.vars - 1
    IF
      (option = var.name[index][0])
        display.on[index] := NOT display.on[index]
    TRUE
      SKIP

TRUE & SKIP
SKIP

clock ? AFTER display.time
display.time := display.time PLUS display.time.interval

-- Get some data from the controller --
data.input.trigger ! TRUE

last.time := time
clock ? time
time.interval := (REAL32 TRUNC (time MINUS last.time))/ticks.per.second

PAR
  gap.ref.in ? final.gap.ref; display.table[1]
  gap.in ? final.gap; display.table[2]
  vel.in ? final.vel; display.table[3]
  acc.in ? final.acc; display.table[4]
  current.in ? final.current; display.table[5]
  force.in ? final.force; display.table[6]
finished := final.gap

gap.ref := display.table[1]
IF
  ((gap.ref - 0.00009 (REAL32)) > last.gap.ref)
  SEQ
    write.endstream( screen )
    display.table[1] := last.gap.ref
    clock ? display.time
    real.time := 0.0 (REAL32)
  TRUE
    real.time := real.time + time.interval
last.gap.ref := gap.ref

display.table[0] := real.time

-- Scale the variables before display --
SEQ var.index = 1 FOR num.vars - 1
  IF
    display.on[ var.index ]
    display.table[ var.index ] := display.table[ var.index ] *
      (REAL32 TRUNC var.scaler[ var.index ])
  TRUE
    SKIP

-- Display value of each selected variable --
IF
  bar.display.selected
  SEQ
    goto.xy( screen, 0, 24 )
    clear.eol( screen )
  TRUE
    SKIP

string[0] := '*c'
string[1] := '*n'
string.index := 2
SEQ var.index = 0 FOR num.vars
  IF
    display.on[ var.index ]
    SEQ
      append.text( string.index, string, var.name[ var.index ] )

```

```

        append.real32( string.index, string,
            display.table[var.index], var.bp[var.index], var.ap[var.index] )
        string[ string.index ] := ' '
        string.index := string.index + 1
    TRUE
    SKIP
write.len.string( screen, string.index, string )

IF
    bar.display.selected
    SEQ -- Display line graph for each selected variable --
    SEQ index = 0 FOR SIZE display.line
        display.line[ index ] := ' '
    SEQ index = 1 FOR 9
        display.line[ index * 8 ] := '.'
    display.line[ 0 ] := '|'

    SEQ var.index = 1 FOR num.vars - 1 -- exclude time --
    IF
        display.on[ var.index ]
        SEQ
            line.index := INT ROUND ((80.0 (REAL32) * display.table[var.index]) /
                (REAL32 TRUNC var.FSD[var.index]))
            IF
                (line.index > 79)
                    line.index := 79
                (line.index < 0)
                    line.index := 0
            TRUE
            SKIP
            display.line[ line.index ] := var.name[ var.index ][ 0 ]
        TRUE
        SKIP

        goto.xy( screen, 0, 23 )
        write.full.string( screen, display.line )
    TRUE
    SKIP
:

-----
#USE "Protocols.tsr"
#USE  snglmath

VAL num.ref.chans IS 2 :

PROC Controller( CHAN OF control.p  cycle.finished.in,
                CHAN OF control.p  start.cycle.out,
                [num.ref.chans] CHAN OF data.p  airgap.reference.out,
                CHAN OF BOOL  stop.system.in,
                CHAN OF exception.p  exception.out,
                VAL REAL32  sampling.period,
                VAL REAL32  operating.airgap, airgap.frequency,
                airgap.amplitude,
                VAL BYTE  airgap.waveform )

-- Controller controls the scheduling, start up, and shutdown of the magnet.
-- It also checks the execution time and generates the reference signal.

-- Worldly constants --
VAL two.pi IS 2.0 (REAL32) * 3.1415926 (REAL32) :

-- Airgap --
VAL airgap.ramp.limit IS 0.010 (REAL32) :
VAL airgap.ramp.vel IS 0.005 (REAL32) :
REAL32 t, sine, airgap, amplitude.factor :

-- Sampling --
VAL ticks.per.sec IS 1000000.0 (REAL32) :
INT sample.interval.ticks, sample.time, time :
REAL32 cycle.time :
TIMER sampler :

BOOL ramp.up, ramp.down, time.to.wind.down, finished, done :

SEQ
    -- Prepare status --
    t := 0.0 (REAL32)
    amplitude.factor := airgap.amplitude / 2.0 (REAL32) -- was pk-pk --

```

```

airgap := airgap.ramp.limit
ramp.up := TRUE
ramp.down := FALSE
finished := FALSE

-- Allow for all PROCs to initialise etc before timing --
start.cycle.out ! finished; TRUE
PAR i = 0 FOR num.ref.chans
    airgap.reference.out[i] ! finished; airgap
cycle.finished.in ? finished; done

-- Initialise sampling timer --
sample.interval.ticks := INT ROUND( ticks.per.sec * sampling.period)
sampler ? sample.time

WHILE NOT finished
    SEQ
    PRI ALT
        stop.system.in ? time.to.wind.down
    SEQ
        ramp.up := FALSE
        ramp.down := TRUE
    TRUE & SKIP
    SEQ
        ramp.up := ramp.up AND (airgap > operating.airgap)
        finished := ramp.down AND (airgap > airgap.ramp.limit)

IF
    ramp.up
    airgap := airgap - (airgap.ramp.vel * sampling.period)
    ramp.down
    airgap := airgap + (airgap.ramp.vel * sampling.period)
    TRUE
    SEQ
        t := t + sampling.period
        sine := SIN( two.pi * (airgap.frequency * t) )
        CASE airgap.waveform
            'I' -- sine wave --
                airgap := operating.airgap + (amplitude.factor * sine)
            'Q' -- square wave --
                IF
                    (sine > 0.0 (REAL32))
                        airgap := operating.airgap + amplitude.factor
                TRUE
                    airgap := operating.airgap - amplitude.factor
            ELSE -- constant airgap --
                airgap := operating.airgap

-- Wait for next sampling time --
sampler ? time
cycle.time := REAL32 TRUNC (time MINUS sample.time)
sample.time := sample.time PLUS sample.interval.ticks
IF
    (time AFTER sample.time)
    VAL [] BYTE message IS "Error: Sampling period is too short, cycle time was:" :
    SEQ
        exception.out ! SIZE message::message; (cycle.time / ticks.per.sec) * 1000.0 (REAL32)
        sample.time := time
    TRUE
    sampler ? AFTER sample.time

-- Initiate an iteration of the control loop --
start.cycle.out ! finished; TRUE
PAR i = 0 FOR num.ref.chans
    airgap.reference.out[i] ! finished; airgap
cycle.finished.in ? finished; done
:

-----

PROC Levitate( CHAN OF INT keyboard,
              CHAN OF ANY screen,
              CHAN OF INT16 ADC.in, ADC.out, DAC.in, DAC.out,
              VAL REAL32 integral.time, stiffness, damping, massness,
                    sampling.period,
                    est.cutoff.Hz, track.cutoff.Hz,
                    mass, operating.airgap,
                    airgap.frequency, airgap.amplitude, logging.period,
              VAL BYTE airgap.waveform )

```

```

-- Levitate executes the component processes of the control and monitoring
-- system, ensuring that appropriate process priorities are allocated and
-- that a controlled system shutdown is achieved.

[3] CHAN OF data.p gap :
[1] CHAN OF data.p vel :
[2] CHAN OF data.p acc, gap.ref, force, current :
CHAN OF data.p gap.buf, vel.buf, acc.buf, force.buf, current.buf, gap.ref.buf :
[7] CHAN OF exception.p exception :
CHAN OF control.p start.cycle, cycle.finished :
CHAN OF BOOL stop.system, buffer.output.trigger :

VAL release.exception.handler IS 0 :
VAL [] BYTE nothing IS "" :

INT message.length, anychar :
REAL32 message.value :
[80] BYTE message :

SEQ
  PAR
    SEQ
      PRI PAR
        PAR
          Interface.to.outside.world( ADC.in, ADC.out,
                                     DAC.in, DAC.out,
                                     start.cycle, current[1],
                                     gap, acc,
                                     cycle.finished,
                                     exception[1] )

          Calculate.magnet.force( gap[1], gap.ref[1], acc[1],
                                 force, vel,
                                 exception[3],
                                 integral.time, stiffness, damping, massness,
                                 mass, sampling.period,
                                 est.cutoff.Hz, track.cutoff.Hz )

          Calculate.magnet.current( gap[2], force[1],
                                   current,
                                   exception[4],
                                   sampling.period )

          Controller( cycle.finished,
                     start.cycle, gap.ref,
                     stop.system,
                     exception[5],
                     sampling.period,
                     operating.airgap, airgap.frequency, airgap.amplitude,
                     airgap.waveform )

          Data.Buffer( gap[0], gap.buf, vel[0], vel.buf, acc[0], acc.buf,
                     force[0], force.buf, current[0], current.buf,
                     gap.ref[0], gap.ref.buf,
                     buffer.output.trigger )

          Data.Monitor( gap.buf, vel.buf, acc.buf, force.buf, current.buf,
                      gap.ref.buf,
                      buffer.output.trigger,
                      exception[6], keyboard, screen,
                      logging.period )

          exception[ release.exception.handler ] ! 0::""; 0.0(REAL32)

          Handle.exceptions( exception,
                            stop.system,
                            message, message.length, message.value )

        IF
          (message.length > 0)
            SEQ
              newline( screen )
              newline( screen )
              write.len.string( screen, message.length, message )
              write.real32( screen, message.value, 3,3 )
              newline( screen )
              read.char( keyboard, anychar )
            TRUE
          SKIP

```

```

-----
PROC Menu( CHAN OF INT keyboard,
           CHAN OF ANY screen,
           CHAN OF INT16 ADC.in, ADC.out, DAC.in, DAC.out,
           REAL32 integral.time, stiffness, damping, massness,
           sampling.period, est.cutoff.Hz, track.cutoff.Hz,
           mass, operating.airgap,
           airgap.frequency, airgap.amplitude, logging.period,
           BYTE airgap.waveform )

-- Menu permits the setting of system parameters and initiates a control system run.

-----

PROC Write.menu( VAL [] BYTE option,
                 VAL REAL32 value,
                 VAL INT i, d,
                 VAL [] BYTE units )

SEQ
  write.full.string( screen, "
                               " )
  write.full.string( screen, option )
  write.real32( screen, value, i, d )
  write.full.string( screen, units )
  newline( screen )
:

-----

PROC Get.value( VAL [] BYTE text,
                REAL32 new.value,
                VAL REAL32 factor )

INT delimiter :

SEQ
  write.text.line( screen, text )
  write.full.string( screen, "
                               Enter new parameter value: " )
  new.value := 0.0 (REAL32)
  delimiter := INT ' '
  read.echo.real32( keyboard, screen, new.value, delimiter )
  new.value := new.value * factor
:

VAL kilo IS 1000.0 (REAL32) :
VAL kilo.g IS 9810.0 (REAL32) :

INT option.int :
BYTE option :
REAL32 factor :
BOOL finished :

SEQ
  finished := FALSE
  WHILE NOT finished
    SEQ
      write.endstream( screen )

      -- Write menu on screen --
      goto.xy( screen, 0,0 )
      clear.eos( screen )

      write.text.line( screen, "
                               MAGLEV CONTROLLER" )
      write.text.line( screen, "
                               ~~~~~")
      newline( screen )

      Write.menu("I ---- Integral time constant ( ", integral.time, 1,1, " s )" )
      Write.menu("S ---- Stiffness ( ", stiffness/kilo.g, 2,1, " kg/mm )" )
      Write.menu("D ---- Damping ( ", damping/kilo.g, 1,2, " kg/(mm/s)" )
      Write.menu("M ---- Massness ( ", massness, 2,1, " kg )" )
      newline( screen )

      Write.menu("P ---- sampling Period ( ", sampling.period*kilo, 1,2, " ms )" )
      Write.menu("E ---- Estimation cutoff frequency ( ", est.cutoff.Hz, 1,1, " Hz )" )
      Write.menu("T ---- Track cutoff frequency ( ", track.cutoff.Hz, 2,1, " Hz )" )
      Write.menu("L ---- suspended Load ( ", mass, 2,1, " Kg )" )
      newline( screen )

      Write.menu("G ---- airGap ( ", operating.airgap*kilo, 1,2, " mm )" )
      Write.menu("R ---- Reference signal frequency ( ", airgap.frequency, 2,2, " Hz )" )
      Write.menu("A ---- reference signal Amplitude ( ", airgap.amplitude*kilo, 1,2, " mm pk-pk )" )

```



```

Write.menu("O ---- data logging period ( ", logging.period*kilo, 2,1, " ms )")
write.text.line(screen,"                               W ---- Waveform ")
newline( screen )

write.text.line(screen,"                               V ---- leVitate")
write.text.line(screen,"                               Q ---- Default parameters")

write.full.string(screen,"*c*n                               Select option: ")
read.char(keyboard, option.int )

-- Convert to uppercase and BYTE --
option := BYTE (option.int /\ #DF)

CASE option
'I'
  Get.value( "Integral time constant", integral.time, 1.0 (REAL32) )
'S'
  Get.value( "Stiffness", stiffness, kilo.g )
'D'
  Get.value( "Damping", damping, kilo.g )
'M'
  Get.value( "Massness", massness, 1.0 (REAL32) )
'P'
  SEQ
    Get.value( "Sampling period", sampling.period, 0.001(REAL32))
    IF
      (sampling.period < 0.0001 (REAL32))
        sampling.period := 0.0001 (REAL32)
    TRUE
    SKIP
'E'
  Get.value( "Estimation cut-off frequency", est.cutoff.Hz, 1.0(REAL32))
'T'
  Get.value( "Track cut-off frequency", track.cutoff.Hz, 1.0(REAL32))
'L'
  Get.value( "Load", mass, 1.0 (REAL32) )
'G'
  Get.value( "Airgap", operating.airgap, 0.001 (REAL32) )
'R'
  Get.value( "Reference signal frequency", airgap.frequency, 1.0 (REAL32) )
'A'
  Get.value( "Reference signal amplitude", airgap.amplitude, 0.001 (REAL32) )
'O'
  Get.value( "Data logging period", logging.period, 0.001(REAL32))
'W'
  SEQ
    write.text.line( screen, "Waveform" )
    write.full.string( screen, "                               None, sIne or sQuare ? " )
    read.echo.char( keyboard, screen, option.int )
    airgap.waveform := BYTE (option.int /\ #DF)
'V'
  SEQ
    write.text.line( screen, "Levitating" )
    Levitate( keyboard, screen,
      ADC.in, ADC.out, DAC.in, DAC.out,
      integral.time, stiffness, damping, massness,
      sampling.period, est.cutoff.Hz, track.cutoff.Hz,
      mass, operating.airgap,
      airgap.frequency, airgap.amplitude, logging.period,
      airgap.waveform )
'Q'
  finished := TRUE
ELSE
  beep( screen )
:

```

```
-----  
PROC Kernel( CHAN OF INT keyboard,  
             CHAN OF ANY screen,  
             CHAN OF INT16 ADC.in, ADC.out, DAC.in, DAC.out )  
  
-- Kernel is the control system kernel process.  
  
-- Ride characteristics --  
REAL32 integral.time, stiffness, damping, massness :  
REAL32 sampling.period, accel.cutoff.Hz, track.cutoff.Hz :  
REAL32 mass, operating.airgap :  
REAL32 airgap.frequency, airgap.amplitude, logging.period :  
BYTE airgap.waveform :  
  
SEQ  
  WHILE TRUE  
    SEQ  
      Set.default.parameters( integral.time, stiffness, damping, massness,  
                              sampling.period, accel.cutoff.Hz, track.cutoff.Hz,  
                              mass, operating.airgap,  
                              airgap.frequency, airgap.amplitude, logging.period,  
                              airgap.waveform )  
  
      Menu( keyboard, screen,  
            ADC.in, ADC.out, DAC.in, DAC.out,  
            integral.time, stiffness, damping, massness,  
            sampling.period, accel.cutoff.Hz, track.cutoff.Hz,  
            mass, operating.airgap,  
            airgap.frequency, airgap.amplitude, logging.period,  
            airgap.waveform )  
:  
  
-----  
-- Procedure code for Maglev.Controller()  
  
SEQ  
  Kernel( keyboard, screen,  
          ADC.in, ADC.out,  
          DAC.in, DAC.out )  
:
```

---

```
VAL event IS 8 :
```

```
PROC ADC.driver( CHAN OF INT16 in, out )
```

```
INT16 channel, volts :
INT adc, mux, value :
BOOL done :
CHAN OF BOOL ready :
```

```
PLACE ready AT event :
PLACE adc AT #6000 :
PLACE mux AT #6100 :
```

```
-- The ADC outputs the last conversion result and starts a new
-- conversion each time it is read. It then generates an interrupt
-- upon the end of each conversion which is notified by 'ready'.
```

```
SEQ
```

```
value := adc -- start conversions & interrupts rolling
WHILE TRUE
```

```
SEQ
```

```
in ? channel -- wait for adc channel request
```

```
mux := INT channel -- select required channel
```

```
ready ? done
```

```
value := adc -- start conversion
```

```
ready ? done
```

```
value := adc -- read adc result
```

```
out ! INT16 (value /\ #FFF0) -- output adc result
```

```
:
```

---

```
PROC DAC.driver( CHAN OF INT16 in, out )
```

```
INT16 current :
BOOL kill.power :
INT dac1, switch, disable :
```

```
PLACE switch AT #6000 :
```

```
PLACE dac1 AT #6100 :
```

```
PLACE disable AT #6700 :
```

```
SEQ
```

```
WHILE TRUE
```

```
SEQ
```

```
in ? current -- wait for DAC output request
```

```
kill.power := (switch /\ 1) = 1 -- check front panel switch
```

```
IF
```

```
kill.power
```

```
dac1 := 0
```

```
((INT current) < #1000)
```

```
dac1 := (INT current)
```

```
TRUE
```

```
dac1 := #0FFF
```

```
disable := 0 -- reset watchdog timer
```

```
:
```

```
-----  
-- Process and channel Configuration  
  
-- Transputer link addresses --  
VAL link0out IS 0 :  
VAL link1out IS 1 :  
VAL link2out IS 2 :  
VAL link3out IS 3 :  
VAL link0in IS 4 :  
VAL link1in IS 5 :  
VAL link2in IS 6 :  
VAL link3in IS 7 :  
  
-- Define inter-processor links --  
CHAN OF INT host.to.controller :  
CHAN OF ANY controller.to.host :  
  
CHAN OF INT16 controller.to.DAC, controller.to.ADC :  
CHAN OF INT16 ADC.to.controller, DAC.to.controller :  
  
-- Configure process allocation and links --  
PLACED PAR  
  
PROCESSOR 1 T8 -- Controller  
  PLACE controller.to.host AT link0out :  
  PLACE host.to.controller AT link0in :  
  
  PLACE controller.to.ADC AT link1out :  
  PLACE ADC.to.controller AT link1in :  
  
  PLACE controller.to.DAC AT link2out :  
  PLACE DAC.to.controller AT link2in :  
  
  Maglev.Controller( host.to.controller, controller.to.host,  
                    ADC.to.controller, controller.to.ADC,  
                    DAC.to.controller, controller.to.DAC )  
  
PROCESSOR 2 T2 -- ADC  
  PLACE ADC.to.controller AT link2out :  
  PLACE controller.to.ADC AT link2in :  
  
  ADC.driver( controller.to.ADC, ADC.to.controller )  
  
PROCESSOR 3 T2 -- DAC  
  PLACE DAC.to.controller AT link1out :  
  PLACE controller.to.DAC AT link1in :  
  
  DAC.driver( controller.to.DAC, DAC.to.controller )
```

## E.4 Single electromagnet real-time simulator

```

REAL64 FUNCTION Magnet.Force( VAL REAL64 airgap, current )

  VAL num.current.points IS 8 :
  VAL [num.current.points] REAL64 current.point IS
    [ 2.0 (REAL64), 3.0 (REAL64), 4.0 (REAL64), 5.0 (REAL64),
      6.0 (REAL64), 7.0 (REAL64), 8.0 (REAL64), 9.0 (REAL64) ] :

  VAL num.airgap.points IS 4 :
  VAL [num.airgap.points] REAL64 airgap.point IS
    [ 0.002 (REAL64), 0.003 (REAL64), 0.004 (REAL64), 0.005 (REAL64) ] :

  VAL [num.airgap.points][num.current.points] REAL64 force.table IS
    [[24.0 (REAL64), 75.0 (REAL64), 140.0 (REAL64), 212.0 (REAL64),
      300.0 (REAL64), 405.0 (REAL64), 540.0 (REAL64), 690.0 (REAL64)],
     [12.0 (REAL64), 46.0 (REAL64), 85.0 (REAL64), 132.5 (REAL64),
      185.0 (REAL64), 257.0 (REAL64), 357.5 (REAL64), 485.0 (REAL64)],
     [ 8.0 (REAL64), 20.0 (REAL64), 38.5 (REAL64), 69.0 (REAL64),
      108.0 (REAL64), 156.0 (REAL64), 212.5 (REAL64), 277.5 (REAL64)],
     [ 6.0 (REAL64), 12.5 (REAL64), 23.5 (REAL64), 42.0 (REAL64),
      63.0 (REAL64), 93.0 (REAL64), 125.0 (REAL64), 170.0 (REAL64)]]:

  INT current.index, airgap.index :
  REAL64 extra.current.ratio, extra.airgap.ratio :
  REAL64 corner.current, delta.current :
  REAL64 corner.airgap, delta.airgap :

  REAL64 F.Amin.Imin, F.Amax.Imin, F.Amin.Imax, F.Amax.Imax :
  REAL64 F.Amin, F.Amax, F :

  VALOF
  SEQ
  -- Find current index and delta

  current.index := 0
  SEQ each.current = 0 FOR num.current.points - 1
  IF
    (current >= current.point[ each.current ])
    current.index := each.current
  TRUE
  SKIP
  corner.current := current.point[ current.index ]
  delta.current := (current.point[ current.index + 1 ] - corner.current)
  extra.current.ratio := (current - corner.current) / delta.current

  -- Find airgap index and delta

  airgap.index := 0
  SEQ each.airgap = 0 FOR num.airgap.points - 1
  IF
    (airgap >= airgap.point[ each.airgap ])
    airgap.index := each.airgap
  TRUE
  SKIP
  corner.airgap := airgap.point[ airgap.index ]
  delta.airgap := (airgap.point[ airgap.index + 1 ] - corner.airgap)
  extra.airgap.ratio := (airgap - corner.airgap) / delta.airgap

  F.Amin.Imin := force.table[ airgap.index ][ current.index ]
  F.Amin.Imax := force.table[ airgap.index ][ current.index + 1 ]
  F.Amax.Imin := force.table[ airgap.index + 1 ][ current.index ]
  F.Amax.Imax := force.table[ airgap.index + 1 ][ current.index + 1 ]

  F.Amin :=F.Amin.Imin+((F.Amin.Imax-F.Amin.Imin)*extra.current.ratio)
  F.Amax :=F.Amax.Imin+((F.Amax.Imax-F.Amax.Imin)*extra.current.ratio)

  F := F.Amin + ( (F.Amax - F.Amin) * extra.airgap.ratio)
  RESULT F
:

```

```

-----
PROC Simulate.outside.world( CHAN OF INT16  ADC.in, ADC.out,
                             DAC.in, DAC.out,
                             CHAN OF control.p trigger,
                             CHAN OF data.p  current,
                             [num.airgap.chans] CHAN OF data.p airgap.chan,
                             [num.acc.chans] CHAN OF data.p  acc.chan,
                             [num.ext.ref.chans] CHAN OF data.p ext.ref.chan,
                             CHAN OF control.p cycle.finished,
                             CHAN OF exception.p exception,
                             VAL REAL32  sampling.period )

-- Worldy constants --
VAL gravitational.acc IS 9.81 (REAL64) :

-- Load characteristics --
VAL mass IS 11.0 (REAL64) :

-- Magnet characteristics --
VAL L.magnet IS 0.011 (REAL64) :
VAL R.magnet IS 0.79 (REAL64) :
VAL F.min IS 1.0 (REAL64) :
VAL F.max IS 600.0 (REAL64) :

-- Current amplifier characteristics --
VAL k.I.err IS 33.0 (REAL64) :
VAL V.min IS -1.0 (REAL64) :
VAL V.max IS 24.0 (REAL64) :
VAL I.min IS 0.0 (REAL64) :
VAL I.max IS 15.0 (REAL64) :

-- Disturbance characteristics --
VAL airgap.min IS 0.002 (REAL64) :
VAL airgap.max IS 0.006 (REAL64) :
VAL airgap.start IS airgap.max :

-- Feedback sensors time constants and quantization --
VAL T.airgap.transducer IS 0.0005 (REAL64) :
VAL quanta.airgap IS 0.000005 (REAL64) :

VAL w.accel IS 234.4 (REAL64) :
VAL Z.accel IS 0.55 (REAL64) :
VAL quanta.accel IS 0.0005 (REAL64) :

VAL quanta.I IS 0.01 (REAL64) :

-- Simulation calculations --
REAL64 simulation.calculation.interval :
VAL num.steps IS 5 :

-- State variables (and others) --
BOOL final.trigger, final.current, start.converting :
REAL64 acceleration, accel.transducer, accel.tmp :
REAL64 velocity :
REAL64 airgap, airgap.transducer :
REAL64 I.demand, V.magnet, I.magnet, F.magnet :
REAL32 I.demand.real32, airgap.FB, accel.FB :

VAL kilo IS 1000.0 (REAL32) :
VAL ext.ref.sensor.mm IS 3 :
REAL32 ext.gap.ref.mm, ext.gap.ref :
BOOL ext.gap.ref.aborted :

```

```

-----
PROC Integrate( REAL64 y,
               VAL REAL64 x )
  SEQ
  y := y + (x * simulation.calculation.interval)
  :
```

```

PROC Real.pole( REAL64 y,
               VAL REAL64 x, time.constant )

  -- G(s) = 1/(1+sT) --

  REAL64 t :
  SEQ
    t := (x-y) / time.constant
    Integrate( y, t )
  :

PROC Complex.pole( REAL64 y, y.dot,
                  VAL REAL64 x, p, q )

  -- G(s) = 1/(p.s^2 + q.s + 1) --

  REAL64 t :
  SEQ
    t := ((x-y) - (q*y.dot)) / p
    Integrate( y.dot, t )
    Integrate( y, y.dot )
  :

PROC Double.integrate( REAL64 x, x.dot, x.dot.dot,
                      VAL REAL64 lower.limit, upper.limit )

  SEQ
    Integrate( x.dot, x.dot.dot )
    Integrate( x, x.dot )
  IF
    (x < lower.limit)
    SEQ
      x := lower.limit
      x.dot := 0.0 (REAL64)
      x.dot.dot := 0.0 (REAL64)
    (x > upper.limit)
    SEQ
      x := upper.limit
      x.dot := 0.0 (REAL64)
      x.dot.dot := 0.0 (REAL64)
  TRUE
  SKIP
  :

-----

REAL64 FUNCTION Bound( VAL REAL64 x, lower.limit, upper.limit )

  REAL64 x.bounded:

  VALOF
    IF
      (x < lower.limit)
      x.bounded := lower.limit
      (x > upper.limit)
      x.bounded := upper.limit
    TRUE
    x.bounded := x
  RESULT x.bounded
  :

-----

REAL64 FUNCTION Quantize( VAL REAL64 x, quanta )

  INT32 i:

  VALOF
    i := INT32 ROUND (x / quanta)
    RESULT (REAL64 ROUND i) * quanta
  :

```

```

SEQ
-- Initialise state variables --
I.magnet := 0.0 (REAL64)

airgap := airgap.start
velocity := 0.0 (REAL64)
acceleration := 0.0 (REAL64)

accel.tmp := 0.0 (REAL64)
accel.transducer := 0.0 (REAL64)
airgap.transducer := airgap.start

airgap.FB := REAL32 ROUND airgap.start
accel.FB := 0.0 (REAL32)

simulation.calculation.interval :=
    (REAL64 ROUND sampling.period) / (REAL64 ROUND num.steps)

final.current := FALSE
WHILE NOT final.current
    ALT
    -- Feedback signals wanted ? --
    trigger ? final.trigger; start.converting
    PAR
    SEQ -- Read in external airgap reference --
    Read.ADC( ADC.in, ADC.out,
        ext.ref.sensor.mm, ext.gap.ref.mm, ext.gap.ref.aborted)
    ext.gap.ref := (ext.gap.ref.mm / kilo)
    PAR i = 0 FOR num.ext.ref.chans
        ext.ref.chan[i] ! final.trigger; ext.gap.ref
    Write.DAC( DAC.in, DAC.out, -(airgap.FB * kilo))

    PAR i = 0 FOR num.airgap.chans
        airgap.chan[i] ! final.trigger; airgap.FB
    PAR i = 0 FOR num.acc.chans
        acc.chan[i] ! final.trigger; accel.FB

    -- Magnet current demand available ? --
    current ? final.current; I.demand.real32
    SEQ
    I.demand := Bound( REAL64 ROUND I.demand.real32, I.min, I.max )
    I.demand := Quantize( I.demand, quanta.I )

    -- Simulate magnet acceleration and airgap --
    SEQ each.step = 1 FOR num.steps
    SEQ
    V.magnet := Bound( k.I.err*(I.demand-I.magnet), V.min, V.max)

    Real.pole( I.magnet, V.magnet/R.magnet, L.magnet/R.magnet )

    F.magnet := Bound(Magnet.Force(airgap,I.magnet), F.min, F.max)

    acceleration := gravitational.acc - (F.magnet / mass)

    Double.integrate( airgap, velocity, acceleration,
        airgap.min, airgap.max )
    Complex.pole( accel.transducer, accel.tmp, acceleration,
        1.0(REAL64)/(w.accel*w.accel),
        2.0(REAL64)*(Z.accel/w.accel) )
    Real.pole( airgap.transducer, airgap, T.airgap.transducer )

    accel.FB := REAL32 ROUND Quantize(accel.transducer, quanta.accel)
    airgap.FB := REAL32 ROUND Quantize(airgap.transducer, quanta.airgap)

    cycle.finished ! final.current; TRUE

Write.DAC( DAC.in, DAC.out, 0.0 (REAL32) )
:

```



## E.5 Transputer network monitor

```
#####
Network Monitor

Features: - Transfers TDS keyboard and screen across to root transputer
          - Communication may be finished at any time using control-A

Author: Neil McLagan
Version: 1.0
Last modified: 21-12-88
#####

VAL link0out IS 0 :
VAL link1out IS 1 :
VAL link2out IS 2 :
VAL link3out IS 3 :
VAL link0in IS 4 :
VAL link1in IS 5 :
VAL link2in IS 6 :
VAL link3in IS 7 :

[1] CHAN OF ANY from.app :
CHAN OF ANY to.app :
PLACE from.app AT link2in :
PLACE to.app AT link2out :

#USE userio
#USE reinit
#USE interf

PROC Monitor([1] CHAN OF ANY from.app,
             CHAN OF ANY to.screen, to.app,
             CHAN OF INT from.keyboard,
             CHAN OF ANY from.kernel, to.kernel )

VAL k.get.abort.state IS 15 :
VAL abort.polling.interval IS 15 : -- 1 ms

INT key.to.app, dummy, time, state :
BOOL aborted, going :
CHAN OF INT kill, stop :
TIMER clock :

SEQ
  newline( to.screen )
  write.text.line( to.screen, "#####" )
  write.text.line( to.screen, "## Use control-A to return to TDS ##" )
  write.text.line( to.screen, "#####" )
  newline( to.screen )

  aborted := FALSE
  going := TRUE
  PRI PAR
  PAR
    WHILE going
    SEQ
      clock ? time
      clock ? AFTER (time PLUS abort.polling.interval)
      to.kernel ! k.get.abort.state
      from.kernel ? state
      going := (state = 0)
      IF
        going
        SKIP
      TRUE
      PAR
        stop ! 1
        kill ! 1
    WHILE NOT aborted
    ALT
      from.keyboard ? key.to.app
      [4] BYTE key.to.app.table RETYPES key.to.app :
      OutputOrFail.c( to.app, key.to.app.table, kill, aborted )
      kill ? dummy
      aborted := TRUE
    scrstream.multiplexor( from.app, to.screen, stop )
  :
SEQ
  Monitor( from.app, screen, to.app, keyboard, from.kernel, to.kernel )
```

## E.6 Transputer network data logger

```
#####
Network Logger

Features: - Transfers data from root transputer to DOS file

Author: Neil McLagan
Version: 1.0
Last modified: 26-12-88

#####

VAL link0out IS 0 :
VAL link1out IS 1 :
VAL link2out IS 2 :
VAL link3out IS 3 :
VAL link0in IS 4 :
VAL link1in IS 5 :
VAL link2in IS 6 :
VAL link3in IS 7 :

[1] CHAN OF ANY from.app :
CHAN OF ANY to.app :

PLACE from.app AT link2in :
PLACE to.app AT link2out :

#USE userio
#USE interf
#USE krnlhdr

PROC Logger([1] CHAN OF ANY from.app,
            CHAN OF ANY to.screen, to.app,
            CHAN OF INT from.keyboard,
            CHAN OF ANY from.filer, to.filer )

VAL [] BYTE path.name IS "D:\Neil\spreads\" :
[abs.id.size] BYTE file.name :
INT name.len, result, anychar :

CHAN OF ANY buffer.chan :
[30000] BYTE buffer :

SEQ
  newline( to.screen )
  write.text.line( to.screen, "Network Data Logger" )
  write.text.line( to.screen, "======" )
  newline( to.screen )
  newline( to.screen )

  write.full.string( to.screen, "Enter data file name: " )
  read.echo.text.line( from.keyboard, to.screen, name.len, file.name, anychar )
  name.len := name.len - 1

  newline( to.screen )
  write.text.line( to.screen, "Getting data from root transputer ..." )
  newline( to.screen )

PAR
  to.app ! INT 'B'
  SEQ
    scrstream.sink( from.app[0] )
    scrstream.sink( from.app[0] )
    scrstream.sink( from.app[0] )
    scrstream.to.array( from.app[0], buffer )

PAR
  to.app ! INT 'B'
  scrstream.sink( from.app[0] )

write.text.line( to.screen, "Writing data file to DOS ..." )
newline( to.screen )

PAR
  SEQ
    scrstream.from.array( buffer, buffer.chan )
    write.endstream( buffer.chan )
```

```
    scrstream.to.server( buffer.chan, from.filer, to.filer,
                        name.len, file.name, result )

IF
  (result = 0)
    write.full.string( to.screen, "File transfer successful, file: " )
  TRUE
    write.text.line( to.screen, "File transfer failed, file:" )

write.len.string( to.screen, name.len, file.name )
newline( to.screen )
newline( to.screen )

write.full.string( to.screen, "Hit space to finish.")

read.char( from.keyboard, anychar )

:

SEQ
  Logger( from.app, screen, to.app, keyboard, from.filer, to.filer )
```

# Appendix F

---

## Operating instructions

### F.1 Introduction

The control system software runs entirely on the processors in the control system sub-rack units, and having loaded and run the software from the development system PC, the PC itself can be disconnected or switched off. There are no ROMs in the system at present, so the control system program must be loaded from the PC each time the control system is powered up. The actions required to power up the system and connect the PC to the control system racks are listed in Table F.1. Table F.2 lists the actions required to load and run the controller software.

### F.2 Single magnet controller data monitoring

While the controller is running, data is monitored and sent to the PC. Type the relevant variable index letter to toggle the variable display on and off. The monitored variables include <R>eference, air<G>ap, <V>elocity, <A>cceleration, <F>orce and <I>-current. Typing <T> toggles between the moving bar display and simple tabular output and <Q> causes a controlled shutdown and return to the menu.

When data is scrolling down the screen, breaking off to go to the development system using <Control A> will not always register due to the higher priority of the screen server. If this occurs, type <P> which causes the controller output to pause briefly, thus allowing the <Control A> to be registered.

**Table F.1** Mains power and fibre optic signal connections

- 
- 1) Switch on the mains power to the development system PC.
  - 2) Switch on the mains power to the power supply unit (output set to 5 V) feeding the PC's optical fibre interface unit.
  - 3) Switch on the power to the vehicle OR switch on the power to the single magnet controller sub-rack & its associated high power supply.
  - 4) Using a duplex fibre optic cable, connect the reset-out and error-in signals (top and next connectors respectively) on the PC optical interface unit to the reset-in and error-out signals (top and next connectors respectively) on the rack input interface card in the control system sub-rack.
  - 5) Using another duplex fibre optic cable, connect the data-out and data-in signals (bottom and next connectors respectively) on the PC optical interface unit to the data-in and data-out signals (bottom and next connectors respectively) on the rack input interface card in the control system sub-rack.
  - 6) If debugging facilities are required, also connect the analyse signal using a simplex fibre optic cable.
  - 7) If using the vehicle, check that the rack output interface is suitably connected (ie in a similar fashion to the PC to sub-rack connections) to the DAC card in the sub-rack unit with the power controllers.
- 

### F.3 Single magnet controller data logging

Logging of data to a DOS based disc file is achieved by the following:

- select tabular output;
- select the variables to be monitored;
- break out to the transputer development system;
- load the Network Logger EXE <F5> and run it <F6>.

The network logger waits for a few cycles of reference signal in order to clear any buffer queues and then files the selected data for one cycle of reference signal. If the size of the logged data exceeds 32 Kbyte, the Network Logger program will crash (a limitation of an unavoidable system procedure call). Adjust either the number of selected data signals, the output data rate (in the Data.Monitor() process code) or the reference signal frequency. To re-run the Network Monitor or Network Logger at any

**Table F.2** Loading and running the controller software

- 
- 1) Set your working directory to D:\Maglev and start the transputer development system <TDS2>.
  - 2) Toggle the number lock to clear it if necessary and enter <Home> the Maglev system fold.
  - 3) Autoload <Shift F5> the compiler utilities and debugger.
  - 4) Move the cursor to the fold containing the Single Magnet Suspension Controller or the Vehicle Suspension Controller and enter <Home> the fold.
  - 5) Move the cursor to the Network Monitor EXE fold and load <F5> the EXE.
  - 6) Next, move the cursor to the PROGRAM fold and load <ALT 4> the program. If the green reset LED on the PC optical interface doesn't flash during a load, check that the interface unit is powered up. If the reset LEDs on the control system sub-rack cards don't flash during a load, the problem probably lies with the reset+error fibre optic connection. If the LEDs flash but the program doesn't load, the data fibre optic connection is probably wrong.
  - 7) Now run <F6> the loaded Network Monitor EXE to gain access to the controller program.
  - 8) Hit <Enter> and the control system menu should now appear on the screen. You can change the controller parameters or reset them to their default values using various submenus. The system does not prevent parameters being entered which make it unstable. All numbers must be entered with a decimal point and following digit. Failure to do so will crash the system - requiring you to return to the development system <Control A> and go back to step 5.
  - 9) Return to the transputer development system by typing <Control A>.
  - 10) Return to the top level fold by closing the current fold <Page Up> and exit the transputer development system by quitting <Control End>.
- 

stage, sequence through the alternative EXEs <ALT F5> until the right one is found and run it <F6>.

## F.4 Vehicle controller data monitoring

While the controller is running, data can be monitored and sent to the PC. Use the 'Signal Monitor Parameters' menu to set the data monitoring sample time and duration and to initiate a data log. Typing the relevant variable index letter toggles the variable display on and off. The monitored variables include <R>eference, air<G>ap, <V>elocity, <A>cceleration, track <P>osition, <F>orce and <I>-current. Upper case letters give electromagnet signals whilst lower case letters give the vehicle mode signals where appropriate.

When data is scrolling down the screen, breaking off to go to the development system using <Control A> will not always register due to the higher priority of the screen server. If this occurs, type <W> which causes the controller output to pause briefly, thus allowing the <Control A> to be registered.

The following keys have special functions:

- <B> toggles between the moving bar display and simple tabular output.
- <Q> returns to the main menu.
- <L> logs data signals into a buffer.
- <S> toggles screen output between real-time data and logged data.
- <W> waits a few seconds to enable exit to the development system.

## F.5 Vehicle controller data logging

Logging of data to a DOS based disc file is achieved by the following:

- select tabular output;
- select the variables to be monitored;
- break out to the transputer development system;
- load the Network Logger EXE <F5> and run it <F6>.

The network logger waits for the current cycle of reference signal to finish and then files the selected data for one cycle of reference signal. The maximum size of the logged data is limited only by the head processor memory size, and is currently set for 2000 samples. To re-run the Network Monitor or Network Logger at any stage, sequence through the alternative EXEs <ALT F5> until the right one is found and run it <F6>.

## F.6 Guide to using the vehicle controller

Virtually any system parameters can be changed whilst the system is running. However, if you wish to change the reference signal from a track position reference to a vehicle position reference, you *MUST* first de-levitate before making the change. This is because certain filters in the mode position controllers must be re-initialised.

If the system shuts down due to an internal shutdown request, the error message in the top level menu must be cleared before the vehicle can be re-levitated. This is primarily relevant when using the vehicle switch to levitate and de-levitate the system.

There is a problem with the process scheduling which sometimes causes the screen driver to run when the higher priority control code should be running. This causes glitches which disturb the system. When logging data for monitoring purposes, use the 'Signal monitor parameters' menu to initiate a data log to avoid screen output and hence disturbances during the logging period.

The screen output very occasionally halts due to noise pickup on the PC data link. Should this occur, de-levitate the vehicle using the vehicle switch and re-load the controller program.